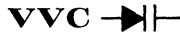


# 1N5461A,B,C (SILICON) thru 1N5476A,B,C



## SILICON EPICAP DIODES

... a PREMIUM line of epitaxial, passivated, abrupt-junction tuning diodes for critical and sophisticated frequency control applications through the UHF range.

- High Q at High Frequencies
- Guaranteed High Capacitance Tuning Range
- Excellent Unit-to-Unit Uniformity
- Guaranteed Temperature Coefficient
- Capacitance Tolerances – 10%, 5.0%, and 2.0%
- Complete Typical Design Curves

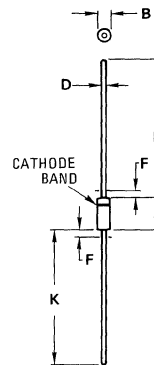
## VOLTAGE-VARIABLE CAPACITANCE DIODES

6.8 – 100 pF  
30 VOLTS



### \*\* MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Reverse Voltage	$V_R$	30	Volts
Device Dissipation @ $T_A = 25^\circ\text{C}$ Derate above $25^\circ\text{C}$	$P_D$	400 2.67	mW mW/ $^\circ\text{C}$
Operating Junction Temperature Range	$T_J$	+175	$^\circ\text{C}$
Storage Temperature Range	$T_{stg}$	-65 to +200	$^\circ\text{C}$



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	5.84	7.62	0.230	0.300
B	2.16	2.72	0.085	0.107
D	0.46	0.56	0.018	0.022
F	—	1.27	—	0.050
K	25.40	—	1.000	—

All JEDEC dimensions and notes apply

CASE 51-02  
DO-7

\*\* Indicates JEDEC Registered Data.

**\*\* ELECTRICAL CHARACTERISTICS** ( $T_A = 25^\circ\text{C}$  unless otherwise noted)

Characteristic--All Types	Test Conditions	Symbol	Min	Typ	Max	Unit
Reverse Breakdown Voltage	$I_R = 10 \mu\text{Adc}$	$BV_R$	30	—	—	Vdc
Reverse Voltage Leakage Current	$V_R = 25 \text{ Vdc}, T_A = 25^\circ\text{C}$ $V_R = 25 \text{ Vdc}, T_A = 150^\circ\text{C}$	$I_R$	—	—	0.02 20	$\mu\text{Adc}$
Series Inductance	$f = 250 \text{ MHz}, \text{lead length} \approx 1/16''$	$L_S$	—	4.0	10	nH
Case Capacitance	$f = 1.0 \text{ MHz}, \text{lead length} \approx 1/16''$	$C_C$	0.1	0.17	0.25	pF
Diode Capacitance Temperature Coefficient (Note 6)	$V_R = 4.0 \text{ Vdc}, f = 1.0 \text{ MHz}$	$TC_C$	—	300	400	ppm/ $^\circ\text{C}$

Device	$C_T$ , Diode Capacitance* $V_R = 4.0 \text{ Vdc}, f = 1.0 \text{ MHz}$ pF			TR, Tuning Ratio $C_2/C_{30}$ $f = 1.0 \text{ MHz}$		Q, Figure of Merit $V_R = 4.0 \text{ Vdc}$ $f = 50 \text{ MHz}$
	Min (Nom -10%)	Nom	Max (Nom +10%)	Min	Max	Min
1N5461A	6.1	6.8	7.5	2.7	3.1	600
1N5462A	7.4	8.2	9.0	2.8	3.1	600
1N5463A	9.0	10.0	11.0	2.8	3.1	550
1N5464A	10.8	12.0	13.2	2.8	3.1	550
1N5465A	13.5	15.0	16.5	2.8	3.1	550
1N5466A	16.2	18.0	19.8	2.9	3.1	500
1N5467A	18.0	20.0	22.0	2.9	3.1	500
1N5468A	19.8	22.0	24.2	2.9	3.2	500
1N5469A	24.3	27.0	29.7	2.9	3.2	500
1N5470A	29.7	33.0	36.3	2.9	3.2	500
1N5471A	35.1	39.0	42.9	2.9	3.2	450
1N5472A	42.3	47.0	51.7	2.9	3.2	400
1N5473A	50.4	56.0	61.6	2.9	3.3	300
1N5474A	61.2	68.0	74.8	2.9	3.3	250
1N5475A	73.8	82.0	90.2	2.9	3.3	225
1N5476A	90.0	100.0	110.0	2.9	3.3	200

\*To order devices with  $C_T$  Nom  $\pm 5.0\%$  or  $\pm 2.0\%$  add Suffix B or C respectively.

\*\*Indicates JEDEC Registered Data.

**PARAMETER TEST METHODS**

**1.  $L_S$ , Series Inductance**

$L_S$  is measured on a shorted package at 250 MHz using an impedance bridge (Boonton Radio Model 250A RX Meter or equivalent).

**2.  $C_C$ , Case Capacitance**

$C_C$  is measured on an open package at 1.0 MHz using a capacitance bridge (Boonton Electronics Model 75A or equivalent).

**3.  $C_T$ , Diode Capacitance**

( $C_T = C_C + C_j$ ).  $C_T$  is measured at 1.0 MHz using a capacitance bridge (Boonton Electronics Model 75A or equivalent).

**4. TR, Tuning Ratio**

TR is the ratio of  $C_T$  measured at 2.0 Vdc divided by  $C_T$  measured at 30 Vdc.

**5. Q, Figure of Merit**

Q is calculated by taking the G and C readings of an admittance bridge at the specified frequency and substituting in the following equations:

$$Q = \frac{2\pi fC}{G}$$

(Boonton Electronics Model 33AS8 or equivalent).

**6.  $TC_C$ , Diode Capacitance Temperature Coefficient**

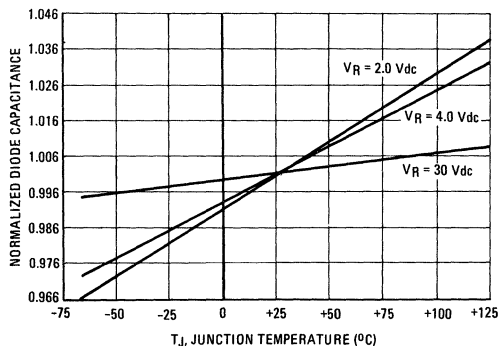
$TC_C$  is guaranteed by comparing  $C_T$  at  $V_R = 4.0 \text{ Vdc}, f = 1.0 \text{ MHz}, T_A = -65^\circ\text{C}$  with  $C_T$  at  $V_R = 4.0 \text{ Vdc}, f = 1.0 \text{ MHz}, T_A = +85^\circ\text{C}$

in the following equation, which defines  $TC_C$ :

$$TC_C = \left[ \frac{C_T(+85^\circ\text{C}) - C_T(-65^\circ\text{C})}{85 + 65} \right] \frac{10^6}{C_T(25^\circ\text{C})}$$

Accuracy limited by  $C_T$  measurement to  $\pm 0.1 \text{ pF}$ .

**FIGURE 1 — NORMALIZED DIODE CAPACITANCE versus JUNCTION TEMPERATURE**



TYPICAL DEVICE PERFORMANCE

FIGURE 2 – DIODE CAPACITANCE versus REVERSE VOLTAGE

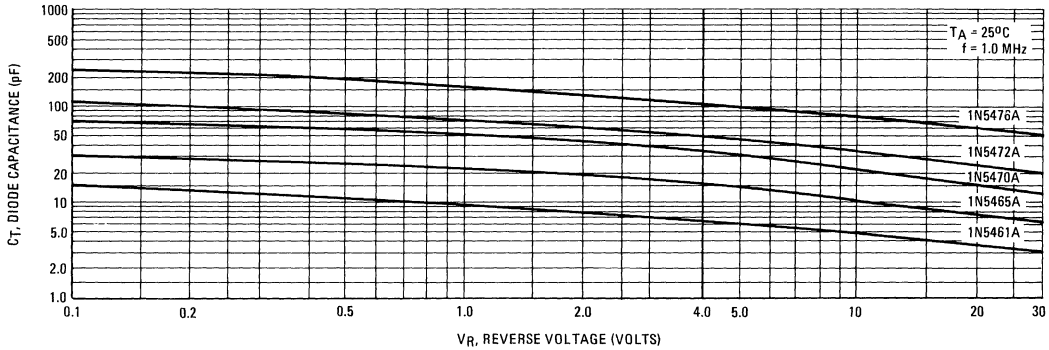


FIGURE 3 – FIGURE OF MERIT versus REVERSE VOLTAGE

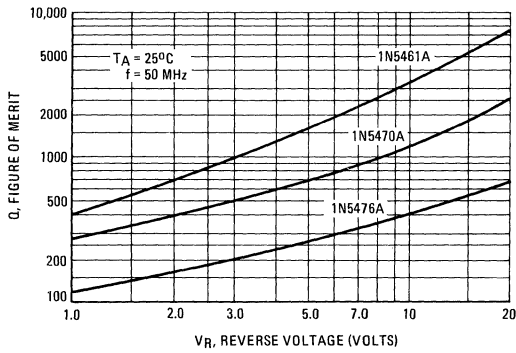


FIGURE 4 – FIGURE OF MERIT versus FREQUENCY

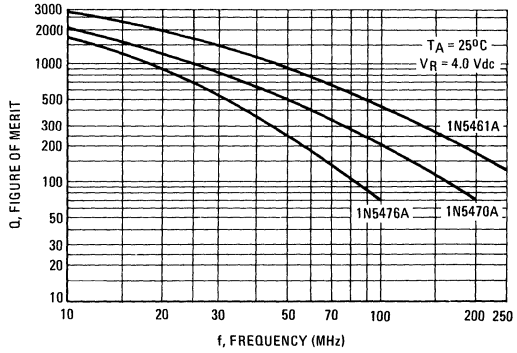


FIGURE 5 – REVERSE CURRENT versus REVERSE BIAS VOLTAGE

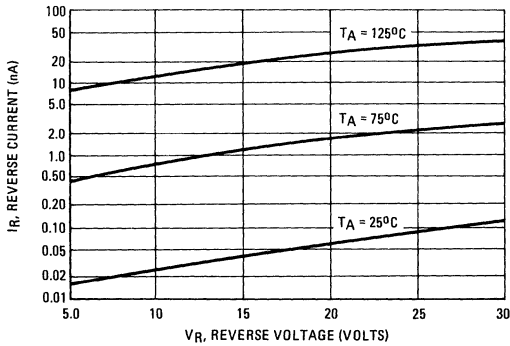
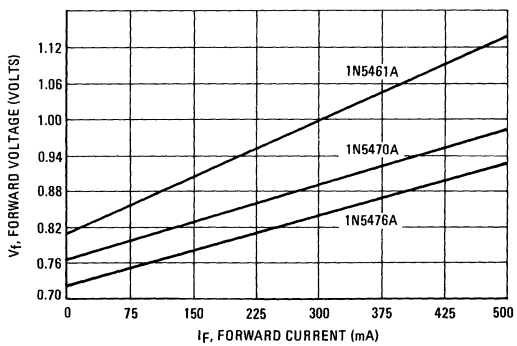


FIGURE 6 – FORWARD VOLTAGE versus FORWARD CURRENT



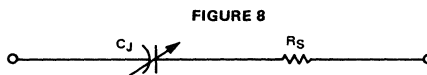
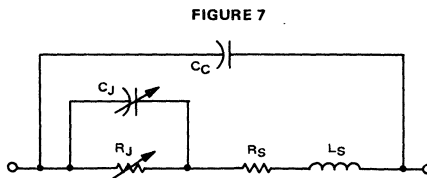
**EPICAP VOLTAGE-VARIABLE CAPACITANCE DIODE DEVICE CONSIDERATIONS**

**A. Epicap Network Presentation**

The equivalent circuit in Figure 7 shows the voltage capacitance and parasitic elements of an EPICAP diode. For design purposes at all but very high and very low frequencies,  $L_S$ ,  $R_J$ , and  $C_C$  can be neglected. The simplified equivalent circuit of Figure 8 represents the diode under these conditions.

**Definitions:**

- $C_J$  - Voltage-Variable Junction Capacitance
- $R_S$  - Series Resistance (semiconductor bulk, contact, and lead resistance)
- $C_C$  - Case Capacitance
- $L_S$  - Series Inductance
- $R_J$  - Voltage-Variable Junction Resistance (negligible above 100 kHz)



**B. Epicap Capacitance versus Reverse Bias Voltage**

The most important design characteristic of an EPICAP diode is the  $C_T$  versus  $V_R$  variation as shown in equations 1 and 2. Tuning Ratio, TR, between any two voltage points on curve of equation (2) is determined from equations (3) and (4).

$$C_T = C_C + C_J \tag{1}$$

$$C_T = C_C + \frac{C_0}{\left(1 + \frac{V_R}{\phi}\right)^\gamma} \tag{2}$$

$$TR \text{ Junction} = \frac{C_{J1}}{C_{J2}} = \left(\frac{V_{R2} + \phi}{V_{R1} + \phi}\right)^\gamma \tag{3}$$

$$TR \text{ Diode} = \frac{C_{T1}}{C_{T2}} = \frac{C_{J1} + C_C}{C_{J2} + C_C} \tag{4}$$

**C. Epicap Capacitance versus Frequency**

Variations in EPICAP effective capacitance, as a function of operating frequency, can be derived from a simplified equivalent circuit similar to that of Figure 7, but neglecting  $R_S$  and  $R_J$ . The admittance expression for such a circuit is given in equation 5. Examination of equation 5 yields the following information:

At low frequencies,  $C_{eq} \approx C_J$ ; at very high frequencies ( $f \approx \infty$ )  $C_{eq} \approx C_C$ .

As frequency is increased from 1.0 MHz,  $C_{eq}$  increases until it is maximum at  $\omega^2 = 1/L_S C_J$ ; and as  $\omega^2$  is increased from  $1/L_S C_J$  toward infinity,  $C_{eq}$  increases from a very negative capacitance (inductance) toward  $C_{eq} = C_C$ , a positive capacitance.

Very simple calculations for  $C_{eq}$  at higher frequencies indicate the problems encountered when capacity measurements are made above 1.0 MHz. As  $\omega$  approaches  $\omega_0 = 1/\sqrt{L_S C_J}$ , small variations in  $L_S$  cause extreme variations in measured diode capacitance.

- $C_0 = C_J$  at  $V_R = 0$
- $V_R =$  Reverse Bias (Volts) \*
- $\gamma$ , Diode Power Law,  $\approx 0.44$
- $\phi$ , Contact Potential,  $\approx 0.6$  Volt
- $C_C \approx 0.17$  pF

$$Y = j\omega C_{eq} = j\omega C_C + \frac{j\omega C_J}{1 - \omega^2 L_S C_J} \tag{5}$$

**D. EPICAP Figure of Merit (Q) and Cutoff Frequency ( $f_{co}$ )**

The efficiency of EPICAP response to an input frequency is related to the Figure of Merit of the device as defined in equation 6. For very low frequencies, equation 7 applies whereas at high frequencies, where  $R_J$  can be neglected, equation 8 may be rewritten into the familiar form of equation 9.

Another useful parameter for EPICAP devices is the cutoff frequency ( $f_{co}$ ), and is the frequency point where Q is equal to 1. Equation 9 gives this relationship.

$$Q = \frac{X_{Seq}}{R_{Seq}} \tag{6}$$

$$Q_L f = \frac{\omega C_J R_J^2}{R_J + R_S(1 + \omega^2 C_J^2 R_J^2)} \tag{7}$$

$$Q_{hf} = \frac{1}{\omega R_S C_{eq}} \tag{8}$$

$$f_{co} = Q_{fmax} \frac{1}{2\pi R_S C_{BVR}} \tag{9}$$

**E. Harmonic Generation Using EPICAPS**

Efficient harmonic generation is possible with EPICAPS because of their high cutoff frequency and breakdown voltage. Since EPICAP junction capacitance varies inversely with the square root of the breakdown voltage, harmonic generator performance can be accurately predicted from various idealized models. Equation 10 gives the level of maximum input power for the EPICAP and equation 11 gives the relationships governing EPICAP circuit efficiency. In these equations, adequate heat sinking has been assumed.

$$P_{in(max)} = \frac{M(BV_R + \phi)^2}{R_S} \frac{f_{in}}{f_{co}} \tag{10}$$

$$M(x2) = 0.0285; M(x3) = 0.0241; M(x4) = 0.196$$

$$Eff = 1 - N \frac{f_{out}}{f_{co}} \tag{11}$$

$$N(x2) = 20.8; N(x3) = 34.8; N(x4) = 62.5$$

M and N are Constants