

# 2N6370 (SILICON)

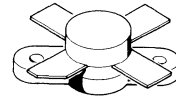
## The RF Line

### NPN SILICON RF POWER TRANSISTOR

... designed primarily as a driver for high-power linear amplifier stages operating from 2.0 to 30 MHz with a 28-Volt supply.

- Power Output @ 28 Vdc, 30 MHz – 10 W (PEP)
- Intermodulation Distortion at Rated Power Output – IMD = -30 dB (Max)

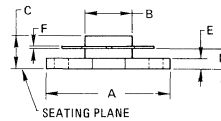
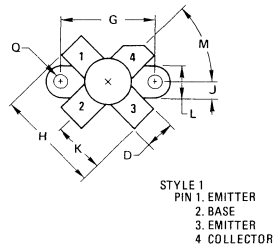
10 W (PEP) – 30 MHz  
RF POWER TRANSISTOR  
NPN SILICON



#### \*MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	$V_{CEO}$	35	Vdc
Collector-Base Voltage	$V_{CBO}$	65	Vdc
Emitter-Base Voltage	$V_{EBO}$	4.0	Vdc
Collector Current – Continuous	$I_C$	1.5	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above $25^\circ\text{C}$	$P_D$	20 0.114	Watts W/ $^\circ\text{C}$
Storage Temperature Range	$T_{stg}$	-65 to +200	$^\circ\text{C}$

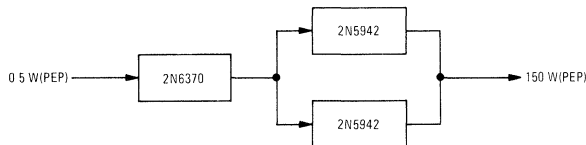
\*Indicates JEDEC Registered Data



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	24.54	24.89	0.970	0.980
B	3.47	9.73	0.373	0.383
C	6.07	7.14	0.239	0.281
D	5.59	5.84	0.220	0.230
E	2.16	2.67	0.085	0.105
F	0.10	0.15	0.004	0.006
G	18.29	18.54	0.720	0.730
H	21.59	22.10	0.850	0.870
J	3.12	3.23	0.123	0.127
K	10.80	11.05	0.425	0.435
L	6.22	6.48	0.245	0.255
M	40°	50°	40°	50°
N	3.81	4.57	0.150	0.180
Q	2.97	3.12	0.117	0.123

CASE 211-01

#### TYPICAL DRIVER APPLICATION

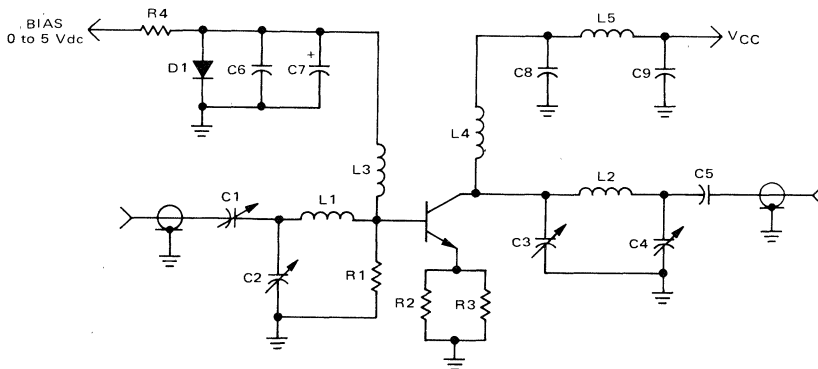


**\*ELECTRICAL CHARACTERISTICS** ( $T_C = 25^\circ\text{C}$  unless otherwise noted)

Characteristics	Symbol	Min	Max	Unit
<b>OFF CHARACTERISTICS</b>				
Collector-Emitter Breakdown Voltage ( $I_C = 50 \text{ mA dc}, I_B = 0$ )	$BV_{CEO}$	35	—	Vdc
Collector-Emitter Breakdown Voltage ( $I_C = 50 \text{ mA dc}, V_{BE} = 0$ )	$BV_{CES}$	65	—	Vdc
Emitter-Base Breakdown Voltage ( $I_E = 5.0 \text{ mA dc}, I_C = 0$ )	$BV_{EBO}$	4.0	—	Vdc
Collector Cutoff Current ( $V_{CE} = 28 \text{ Vdc}, V_{BE} = 0, T_C = +55^\circ\text{C}$ )	$I_{CES}$	—	10	mA dc
<b>ON CHARACTERISTICS</b>				
DC Current Gain ( $I_C = 0.5 \text{ A dc}, V_{CE} = 5.0 \text{ Vdc}$ )	$h_{FE}$	5.0	50	—
<b>DYNAMIC CHARACTERISTICS</b>				
Current-Gain – Bandwidth Product ( $I_C = 0.5 \text{ A dc}, V_{CE} = 15 \text{ Vdc}, f = 50 \text{ MHz}$ )	$f_T$	50	—	MHz
Output Capacitance ( $V_{CB} = 28 \text{ Vdc}, I_E = 0, f = 1.0 \text{ MHz}$ )	$C_{ob}$	—	40	pF
<b>FUNCTIONAL TEST</b>				
Common-Emitter Amplifier Power Gain (Figure 1) ( $P_{out} = 10 \text{ W(PEP)}, I_C = 470 \text{ mA dc Max}, V_{CC} = 28 \text{ Vdc}, f_1 = 30 \text{ MHz}, f_2 = 30.001 \text{ MHz}$ )	$G_{pE}$	12	—	dB
Intermodulation Distortion Ratio (Figure 1) ( $P_{out} = 10 \text{ W(PEP)}, I_C = 470 \text{ mA dc Max}, V_{CC} = 28 \text{ Vdc}, f_1 = 30 \text{ MHz}, f_2 = 30.001 \text{ MHz}$ )	IMD	—	-30	dB
Collector Efficiency ( $P_{out} = 10 \text{ W(PEP)}, I_C = 470 \text{ mA dc Max}, V_{CC} = 28 \text{ Vdc}, f_1 = 30 \text{ MHz}, f_2 = 30.001 \text{ MHz}$ )	$\eta$	38	—	%

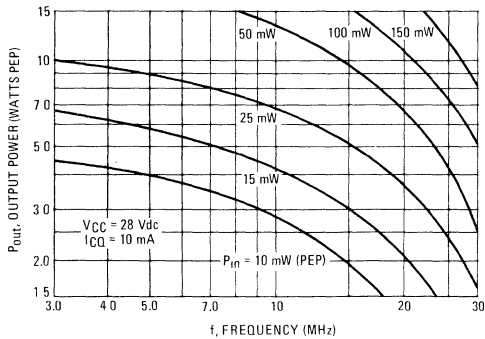
\* Indicates JEDEC Registered Data.

FIGURE 1 – 30 MHz TEST CIRCUIT

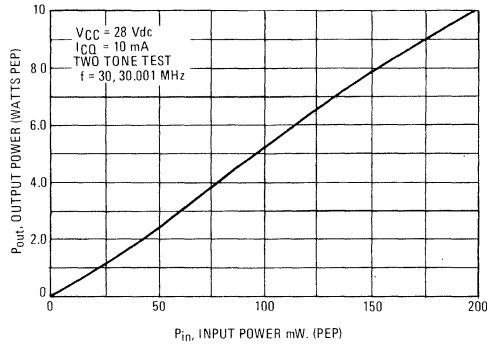


- |            |   |                        |        |   |
|------------|---|------------------------|--------|---|
| C1         | 80 – 480 pF   | ARCO 466 or equivalent | L2     | 5 Turns, #18 AWG, 1/4" I.D., 5/16" Long (0.13 $\mu\text{H}$ ) |
| C2, C3, C4 | 170 – 780 pF  | ARCO 469 or equivalent | L3     | 10 $\mu\text{H}$  |
| C5         | 0.1 $\mu\text{F}$   |                        | L4     | 1.0 $\mu\text{H}$   |
| C6, C9     | 0.01 $\mu\text{F}$  |                        | L5     | RFC VK200 FERROXCUBE  |
| C7         | 500 $\mu\text{F}$   | TANTALUM or equivalent | R1     | 10 OHMS 1/2 W ALLEN BRADLEY or equivalent                     |
| C8         | 2000 pF   | UNELCO or equivalent   | R2, R3 | 1.5 OHMS 1/2 W ALLEN BRADLEY or equivalent                    |
| D1         | 1N4001  |                        | R4     | 50 OHMS 1/2 W ALLEN BRADLEY or equivalent                     |
| L1         | 4 Turns, #18 AWG, 1/2" I.D., 1/4" Long (0.1 $\mu\text{H}$ ) |                        |        | ADJUST BIAS FOR $I_{CQ} = 10 \text{ mA}$                      |

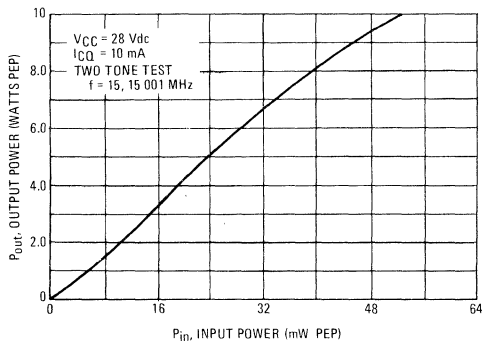
**FIGURE 2 – LINEAR OUTPUT POWER  
versus FREQUENCY**



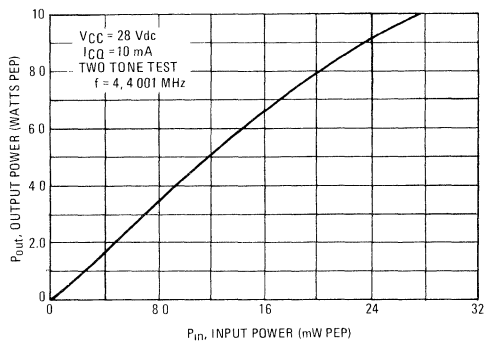
**FIGURE 3 – OUTPUT POWER  
versus INPUT POWER**



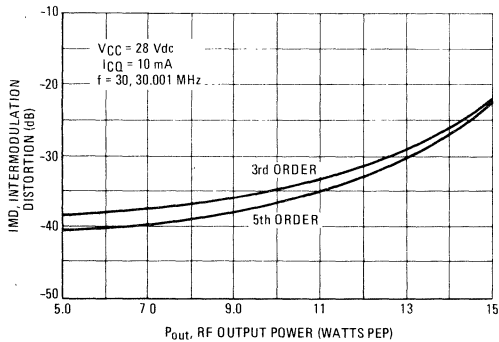
**FIGURE 4 – OUTPUT POWER  
versus INPUT POWER**



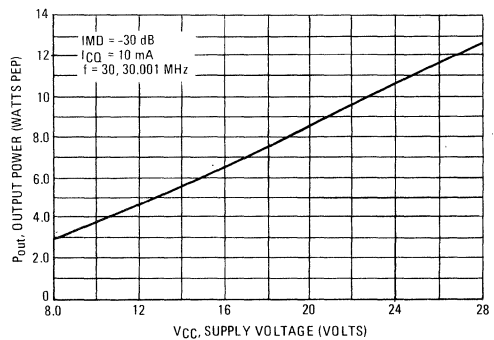
**FIGURE 5 – OUTPUT POWER  
versus INPUT POWER**



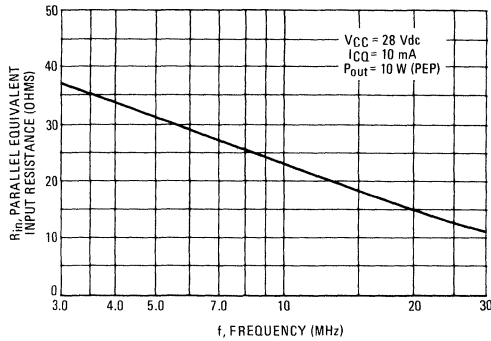
**FIGURE 6 – INTERMODULATION DISTORTION  
versus OUTPUT POWER**



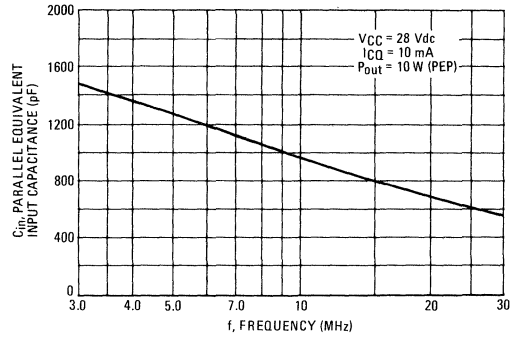
**FIGURE 7 – LINEAR OUTPUT POWER  
versus SUPPLY VOLTAGE**



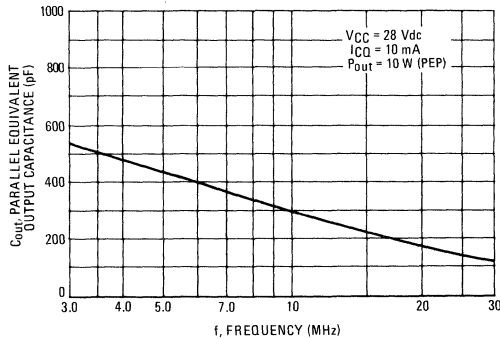
**FIGURE 8 – PARALLEL EQUIVALENT INPUT RESISTANCE versus FREQUENCY**



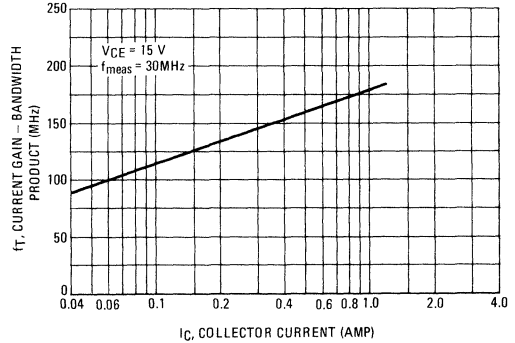
**FIGURE 9 – PARALLEL EQUIVALENT INPUT CAPACITANCE versus FREQUENCY**



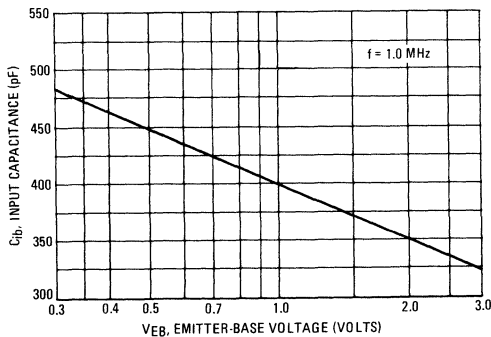
**FIGURE 10 – PARALLEL EQUIVALENT OUTPUT CAPACITANCE versus FREQUENCY**



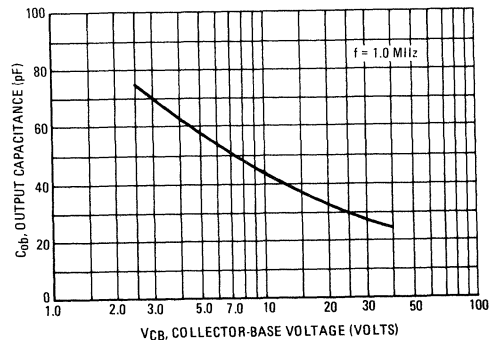
**FIGURE 11 – CURRENT GAIN – BANDWIDTH PRODUCT**



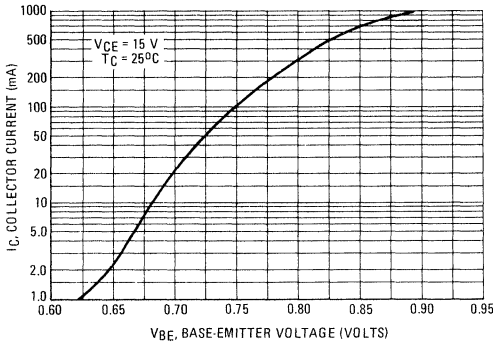
**FIGURE 12 – INPUT CAPACITANCE versus EMITTER-BASE VOLTAGE**



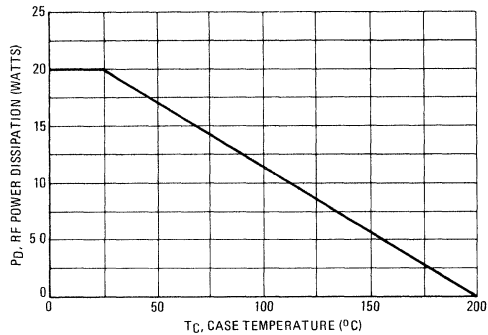
**FIGURE 13 – OUTPUT CAPACITANCE versus COLLECTOR-BASE VOLTAGE**



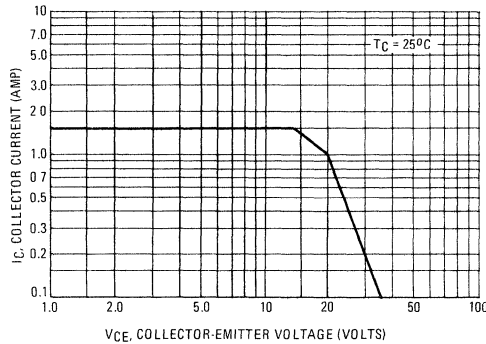
**FIGURE 14 – COLLECTOR CURRENT versus BASE-EMITTER VOLTAGE**



**FIGURE 15 – RF POWER DERATING**



**FIGURE 16 – DC SAFE OPERATING AREA**



**APPLICATIONS INFORMATION**

The 2N6370 transistor is designed for linear power amplifier service in the driver or lower level stages of HF (2-30 MHz) single sideband (SSB) transmitters. It may also be used in amplitude modulated (AM) transmitters employing low level modulation in the exciter, or in any application requiring a linear amplifier. The device also has adequate gain for many VHF applications below 100 MHz.

Designed primarily for lower level stages and not the output stage of SSB transmitters, the 2N6370 does not employ internal emitter resistors. Therefore, for linear power amplifier applications which normally require forward bias for improved linearity, it is suggested that external emitter resistance be employed for improved DC operating point stability over the full temperature range. Typical resistor values for HF operation are illustrated in the test

amplifier shown in Figure 1. The 2N6370 has more than adequate gain at HF, so the designer may wish to utilize unbypassed emitter resistance as shown in the circuit of Figure 1. Of course, bypassing may be included if more gain is desired.

The linear amplifier characterization data in Figures 2 through 10 were measured with the unbypassed emitter resistor configuration shown in Figure 1. For a more detailed discussion of linear power amplifier specifications and design, see Reference 1.

**REFERENCES**

1. "Solid-State Linear Power Amplifier Design", Motorola Semiconductor Products, Inc. Application Note AN-546
2. Pappenfus, Bruene, and Schoenike, "Single Sideband Principles and Circuits", McGraw – Hill.