

Single-chip Type with Built-in FET Switching Regulator Series

High-efficiency Step-up/down Switching Regulator with Built-in Power MOSFET



BD8301MUV No.09027ECT07

General Description

ROHM's highly-efficient step-up/down switching regulator BD8301MUV produces step-up/down output including 3.3 V from 1 cell of lithium battery with just one coil.

This IC adopts an original step-up/down drive system and creates a higher efficient power supply than conventional Sepic-system or H-bridge system switching regulators.

Features

1) Highly-efficient step-up/down DC/DC converter to be constructed just with one inductor.

2) Input voltage
3) Output current
2.5 V - 5.5 V
1 A at 3.3 V

800 mA at 5.0 V

4) Incorporates soft-start function.

5) Incorporates timer latch system short protecting function.

6) High heat radiation surface mounted package VQFN020V4040

Application

General portable equipment like portable audio or DSC/DVC

Absolute Maximum Ratings

Parameter	Symbol	Ratings	Unit
Maximum applied power voltage	Vcc,PVcc	7.0	V
Maximum input current	linmax	2.0	Α
Maximum input valtage	Lx1	7.0	V
Maximum input voltage	Lx2	7.0	V
Power dissipation	Pd	700	mW
Operating temperature range	Topr	-25 to +85	°C
Storage temperature range	Tstg	-55 to +150	°C
Junction temperature	Tjmax	150	°C

^{*1} When installed on a 70.0 mm × 70.0 mm × 1.6 mm glass epoxy board. The rating is reduced by 5.6 mW/°C at Ta = 25°C or more.

Operating Conditions (Ta = 25°C)

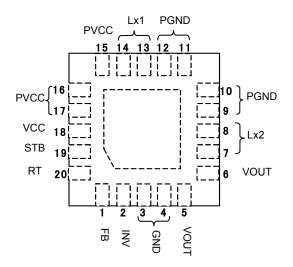
Parameter	Symbol	Voltage range	Unit
Power supply voltage	Vcc	2.5 to 5.5	V
Output voltage	OUT	2.8 to 5.2	V

Electrical Characteristics

(Unless otherwise specified, Ta = 25 °C, Vcc = 3.7 V)

Parameter		Symbol	Target Value		e	Unit	Conditions
			Min	Тур	Max	Unit	Conditions
[Low voltage input malf	unction preventir	ng circuit]					
Detection threshold voltage		VUV	-	2.25	2.45	V	Vcc monitor
Hysteresis range		ΔVUVhy	50	100	150	mV	
[Oscillator]							
Oscillation frequency		fosc	0.8	1.0	1.2	MHz	RT=47kΩ
[Error AMP]							
INV threshold voltage		VINV	0.790	0.800	0.810	V	
Input bias current		IINV	-50	0	50	nA	Vcc=7.0V , VINV=3.5V
Soft-start time		Tss	0.6	1.00	1.4	msec	RT=47kΩ
Output source current		IEO	10	20	30	μA	VINV=0.5V , VFB =1.5V
Output sink current		IEI	0.7	1.5	3.0	mA	VINV=1.1V , VFB =1.5V
[PWM comparator]							
LX1 Max Duty		Dmax1	-	-	100	%	
LX2 Max Duty		Dmax2	77	85	93	%	
[Output]							
LX1 PMOS ON resistance		RON1p	-	120	200	mΩ	VGS=3.0V
LX1 NMOS ON resistance		RON1n	ı	100	160	mΩ	VGS=3.0V
LX2 PMOS ON resista	ance	RON2p	ı	120	200	mΩ	VGS=3.0V
LX2 NMOS ON resistance		RON2n	1	100	160	mΩ	VGS=3.0V
LX1 leak current		l leak1	-1	0	1	μA	
LX2 leak current		I leak2	-1	0	1	μA	
[STB]							
STB pin ontrol voltage	Operation	VSTBH	1.5	ı	5.5	V	
STB pill official voltage	No-operation	VSTBL	-0.3	ı	0.3	V	
STB pin pull-down resistance		RSTB	250	400	700	kΩ	
[Circuit current]							
Standby current	VCC pin	ISTB1	-	-	1	μA	
	PVCC pin	ISTB2	-	-	1	μA	
	VOUT pin	ISTB3	-	-	1	μA	
Circuit current at operation VCC		lcc1	-	500	750	μA	VINV=1.2V
Circuit current at operation PVCC		lcc2	-	10	20	μA	VINV=1.2V

Description of Pins



Pin No.	Pin Name	Function
1	FB	Error AMP output terminal
2	INV	Error AMP input terminal
3~4	GND	Ground terminal
5~6	Vout	Output voltage terminal
7~8	Lx2	Output side coil connecting terminal
9~12	PGND	Power transistor ground terminal
13~14	Lx1	Input side coil connecting terminal
15~17	PVCC	DC/DC converter input terminal
18	VCC	Control part power supply input
		terminal
19	STB	ON/OFF terminal
20	RT	Oscillation frequency set terminal

Fig.1 Pin layout

Block Diagram

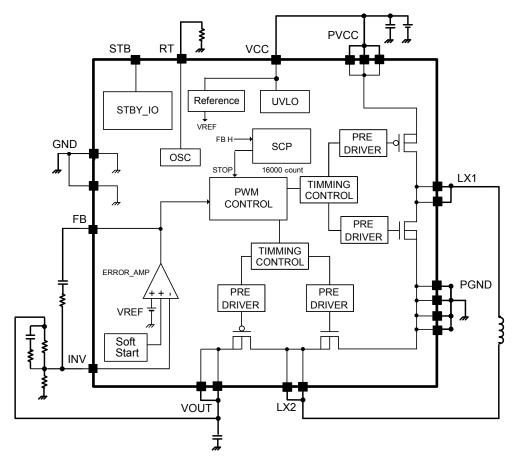


Fig.2 Block diagram

BD8301MUV Technical Note

Description of Blocks

1.VREF

This block generates ERROR AMP reference voltage.

The reference voltage is 0.8 V.

2.UVLO

Circuit for preventing low voltage malfunction

Prevents malfunction of the internal circuit at activation of the power supply voltage or at low power supply voltage. Monitors VCC pin voltage to turn off all output FET and DC/DC converter output when VCC voltage is lower than 2.2 V, and reset the timer latch of the internal SCP circuit and soft-start circuit.

3.SCP

Timer latch system short-circuit protection circuit

When the INV pin is the set 0.8 V or lower voltage, the internal SCP circuit starts counting.

The internal counter is in synch with OSC; the latch circuit activates after the counter counts about 16000 oscillations to turn off DC/DC converter output (about 16 msec when RT = $47k\Omega$).

To reset the latch circuit, turn off the STB pin once. Then, turn it on again or turn on the power supply voltage again.

4.OSC

Oscillation circuit to change frequency by external resistance of the RT pin (20 pin).

When RT = 47 k Ω , operation frequency is set at 1 MHz.

5.FRROR AMP

Error amplifier for detecting output signals and output PWM control signals

The internal reference voltage is set at 0.8 V.

6.PWM COMP

Voltage-pulse width converter for controlling output voltage corresponding to input voltage

Comparing the internal SLOPE waveform with the ERROR AMP output voltage, PWM COMP controls the pulse width and outputs to the driver.

Max Duty and Min Duty are set at the primary side and the secondary side of the inductor respectively, which are as follows:

Primary side (Lx1) Max Duty: 100 %,

Min Duty : 0 %

Secondary side (Lx2) Max Duty: 100 %,

Min Duty : About 15 %

7.SOFT START

Circuit for preventing in-rush current at startup by bringing the output voltage of the DC/DC converter into a soft-start Soft-start time is in synch with the internal OSC, and the output voltage of the DC/DC converter reaches the set voltage after about 1000 oscillations (About 1 msec when RT = 47 k Ω).

8.PRE DRIVER

CMOS inverter circuit for driving the built-in Pch/Nch FET

Dead time is provided for preventing feedthrough during switching.

The dead time is set at about 15 nsec for each individual SWs.

9. STBY IO

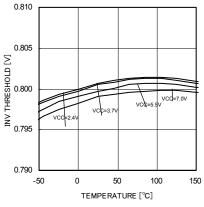
Voltage applied on STB pin (19 pin) to control ON/OFF of IC

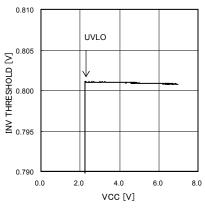
Turned ON when a voltage of 1.5 V or higher is applied and turned OFF when the terminal is open or 0 V is applied. Incorporates approximately 400 $k\Omega$ pull-down resistance.

10. Pch/Nch FET SW

Built-in SW for switching the coil current of the DC/DC converter. Pch FET is about 120 m Ω and Nch is 100 m Ω . Since the current rating of this FET is 2 A, it should be used within 2 A in total including the DC current and ripple current of the coil.

●Reference Data (Unless otherwise specified, Ta = 25°C, VCC = 3.7 V)





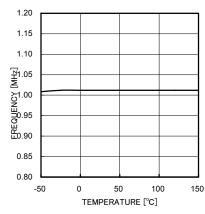
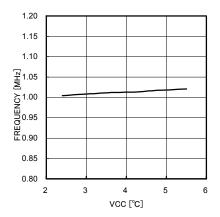
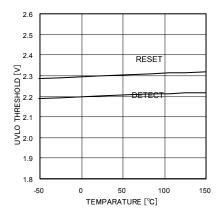


Fig.3 INV threshold

Fig.4. INV threshold (power supply property)

Fig.5 Oscillation frequency





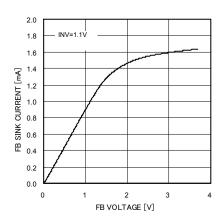
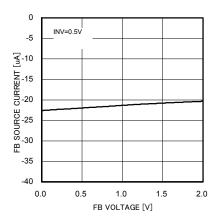
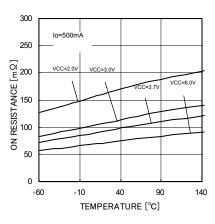


Fig.6 Oscillation frequency (power supply property)

Fig.7 UVLO threshold

Fig.8 FB sink current





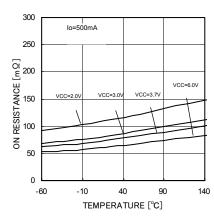


Fig.9 FB source current

Fig.10 Lx1 Pch FET ON resistance

Fig.11 Lx1 Nch FET ON resistance

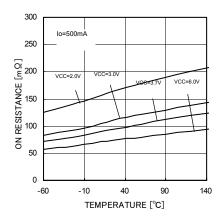


Fig.12 Lx2 Pch FET ON resistance

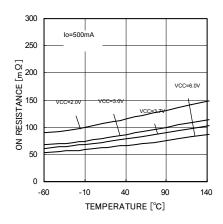


Fig.13 Lx2 Nch FET ON resistance

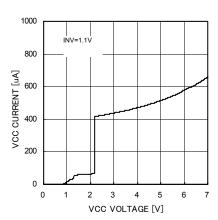


Fig.14 VCC input current

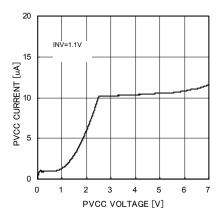


Fig.15 PVCC input current

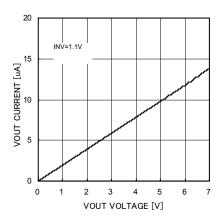
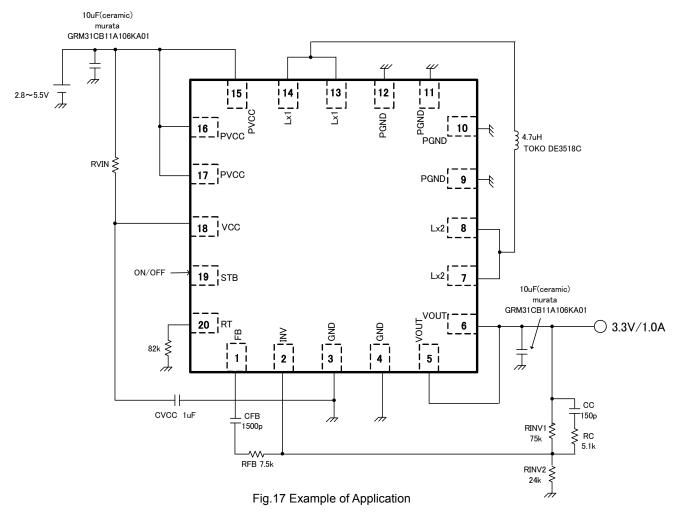


Fig.16 VOUT input current

●Example of Application Input: 2.8 to 5.5 V, output: 3.3 V / 1.0 A, frequency 600 kHz



●Example of Board Layout

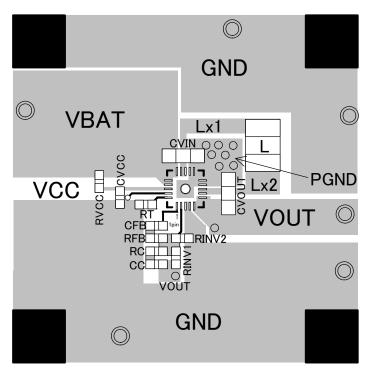
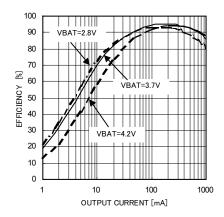
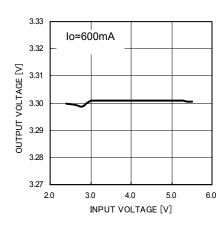


Fig.18 Example of Board Layout

Technical Note **BD8301MUV**

Reference Application Data





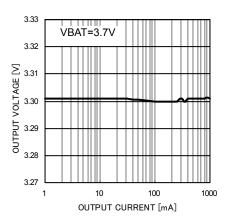


Fig.19 Power conversion efficiency

Fig.20 Line regulation

Fig.21 Load regulation

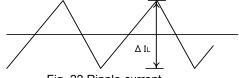
Selection of Parts for Applications

(1) Output inductor

A shielded inductor that satisfies the current rating (current value, Ipeak as shown in the drawing below) and has a low DCR (direct current resistance component) is recommended.

Inductor values affect output ripple current greatly.

Ripple current can be reduced as the coil L value becomes larger and the switching frequency becomes higher as the equations shown below.



Ipeak =lout ×(Vout/VIN) /
$$\eta$$
+ Δ IL/2 [A]

Fig. 22 Ripple current

$$\triangle$$
IL= $\frac{\text{(Vin-Vout)}}{L} \times \frac{\text{Vout}}{\text{Vin}} \times \frac{1}{f}$ [A] (in step-down mode) (2)

$$\triangle IL = \frac{|(Vin-Vout)|}{L} \times \frac{Vout \times 2 \times 0.85}{(Vin+Vout)} \times \frac{1}{f}$$
 [A] (in step-up/down mode) (3)

$$\triangle IL = \frac{\text{(Vout-Vin)}}{L} \times \frac{\text{Vin}}{\text{Vout}} \times \frac{1}{f}$$
 [A] (in step-up mode) (4)

(η: Efficiency, ΔIL: Output ripple current, f: Switching frequency)

As a guide, output ripple current should be set at about 20 to 50% of the maximum output current.

* Current over the coil rating flowing in the coil brings the coil into magnetic saturation, which may lead to lower efficiency or output oscillation. Select an inductor with an adequate margin so that the peak current does not exceed the rated current of the coil.

(2) Output capacitor

A ceramic capacitor with low ESR is recommended for output in order to reduce output ripple.

There must be an adequate margin between the maximum rating and output voltage of the capacitor, taking the DC bias property into consideration.

Output ripple voltage when ceramic capacitor is used is obtained by the following equation.

$$Vpp = \triangle IL \times \frac{1}{2\pi \times f \times Co} + \triangle IL \times R_{ESR} \quad [V] \quad \cdot \cdot \cdot \quad (5)$$

Setting must be performed so that output ripple is within the allowable ripple voltage.

(3) Setting of oscillation frequency

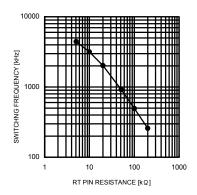
Oscillation frequency can be set using a resistance value connected to the RT pin (1 pin).

Oscillation frequency is set at 1 MHz when RT = 47 k Ω , and frequency is inversely proportional to RT value.

See Fig. 23 for the relationship between RT and frequency.

Soft-start time changes along with oscillation frequency.

See Fig. 24 for the relationship between RT and soft-start time.



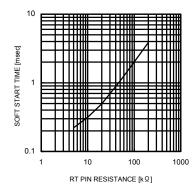


Fig. 23 Oscillation frequency – RT pin resistance

Fig. 24 Soft-start time – RT pin resistance

(4) Output voltage setting

The internal reference voltage of the ERROR AMP is 0.8 V. Output voltage should be obtained by referring to Equation (8) of Fig. 25.

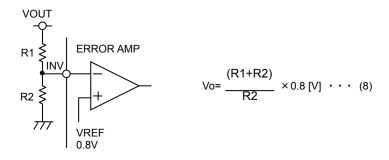


Fig. 25 Setting of feedback resistance

^{*} Note that the above example of frequency setting is just a design target value, and may differ from the actual equipment.

(5) Determination of phase compensation

Condition for stable application

The condition for feedback system stability under negative feedback is as follows:

- Phase delay is 135 °or less when gain is 1 (0 dB) (Phase margin is 45° or higher)

Since DC/DC converter application is sampled according to the switching frequency, the GBW of the whole system (frequency at which gain is 0 dB) must be set to be equal to or lower than 1/5 of the switching frequency. In summary, target property of applications is as follows:

- Phase delay must be 135° or lower when gain is 1 (0 dB) (Phase margin is 45° or higher).
- The GBW at that time (frequency when gain is 0 dB) must be equal to or lower than 1/5 of the switching frequency.

For this reason, switching frequency must be increased to improve responsiveness.

One of the points to secure stability by phase compensation is to cancel secondary phase delay (-180°) generated by LC resonance by the secondary phase lead (i.e. put two phase leads).

Since GBW is determined by the phase compensation capacitor attached to the error amplifier, when it is necessary to reduce GBW, the capacitor should be made larger.

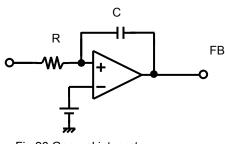


Fig.26 General integrator

Error AMP is a low-pass filter because phase compensation such as (1) and (2) is performed. For DC/DC converter application, R is a parallel feedback resistance.

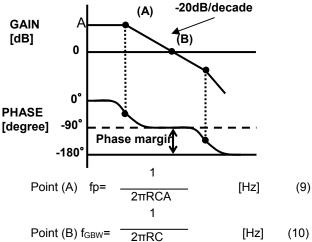


Fig.27 Frequency property of integrator

Phase compensation when output capacitor with low ESR such as ceramic capacitor is used is as follows:

When output capacitor with low ESR (several tens of $m\Omega$) is used for output, secondary phase lead (two phase leads) must be put to cancel secondary phase lead caused by LC.

One of the examples of phase compensation methods is as follows:

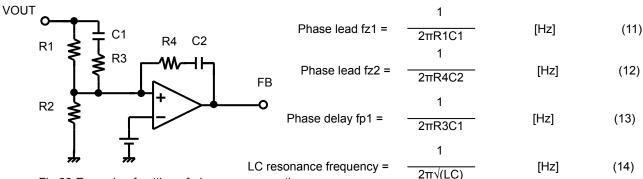


Fig.28 Example of setting of phase compensation

For setting of phase-lead frequency, both of them should be put near LC resonance frequency. When GBW frequency becomes too high due to the secondary phase lead, it may get stabilized by setting the primary phase delay to a frequency slightly higher than the LC resonance frequency by R3 to compensate it.

●I/O Equivalence Circuit

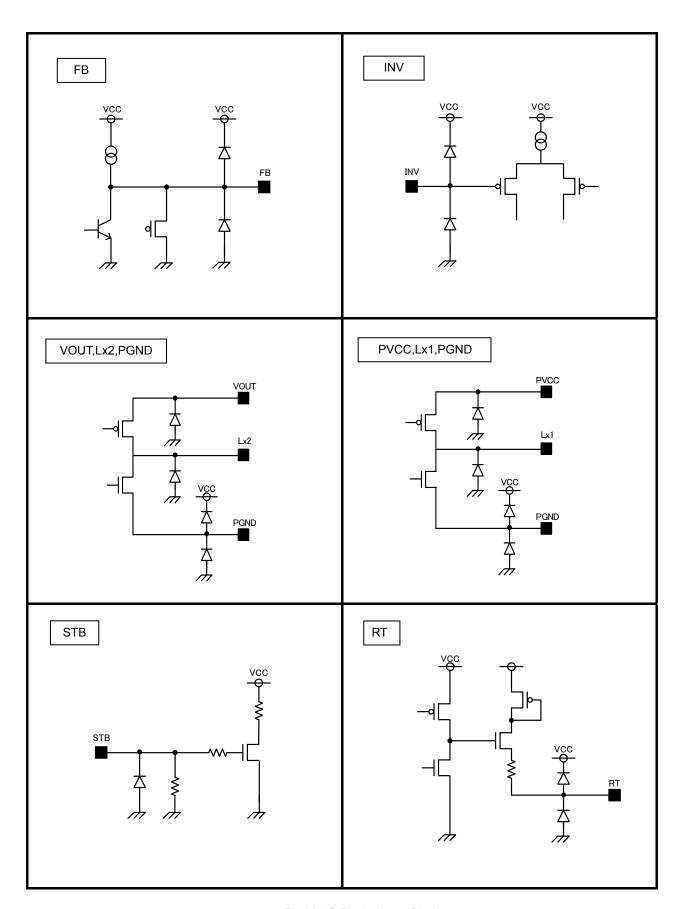


Fig.29 I/O Equivalence Circuit

Precautions for Use

1) Absolute Maximum Rating

We dedicate much attention to the quality control of these products, however the possibility of deterioration or destruction exists if the impressed voltage, operating temperature range, etc., exceed the absolute maximum ratings. In addition, it is impossible to predict all destructive situations such as short-circuit modes, open circuit modes, etc. If a special mode exceeding the absolute maximum rating is expected, please review matters and provide physical safety means such as fuses, etc.

2) GND Potential

Keep the potential of the GND pin below the minimum potential at all times.

3) Thermal Design

Work out the thermal design with sufficient margin taking power dissipation (Pd) in the actual operation condition into account.

4) Short Circuit between Pins and Incorrect Mounting

Attention to IC direction or displacement is required when installing the IC on a PCB. If the IC is installed in the wrong way, it may break. Also, the threat of destruction from short-circuits exists if foreign matter invades between outputs or the output and GND of the power supply.

5) Operation under Strong Electromagnetic Field

Be careful of possible malfunctions under strong electromagnetic fields.

6) Common Impedance

When providing a power supply and GND wirings, show sufficient consideration for lowering common impedance and reducing ripple (i.e., using thick short wiring, cutting ripple down by LC, etc.) as much as you can.

7) Thermal Protection Circuit (TSD Circuit)

This IC contains a thermal protection circuit (TSD circuit). The TSD circuit serves to shut off the IC from thermal runaway and does not aim to protect or assure operation of the IC itself. Therefore, do not use the TSD circuit for continuous use or operation after the circuit has tripped.

8) Rush Current at the Time of Power Activation

Be careful of the power supply coupling capacity and the width of the power supply and GND pattern wiring and routing since rush current flows instantaneously at the time of power activation in the case of CMOS IC or ICs with multiple power supplies.

9) IC Terminal Input

This is a monolithic IC and has P+ isolation and a P substrate for element isolation between each element. P-N junctions are formed and various parasitic elements are configured using these P layers and N layers of the individual elements. For example, if a resistor and transistor are connected to a terminal as shown on Fig.30:

- OThe P-N junction operates as a parasitic diode when GND > (Terminal A) in the case of a resistor or when GND > (Pin B) in the case of a transistor (NPN)
- OAlso, a parasitic NPN transistor operates using the N layer of another element adjacent to the previous diode in the case of a transistor (NPN) when GND > (Pin B).

The parasitic element consequently rises under the potential relationship because of the IC's structure. The parasitic element pulls interference that could cause malfunctions or destruction out of the circuit. Therefore, use caution to avoid the operation of parasitic elements caused by applying voltage to an input terminal lower than the GND (P board), etc.

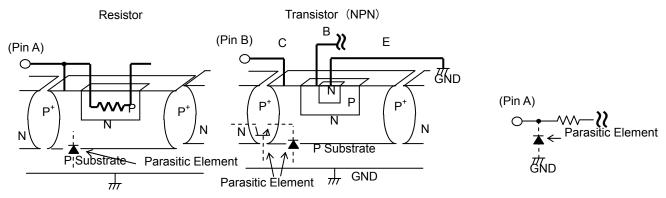
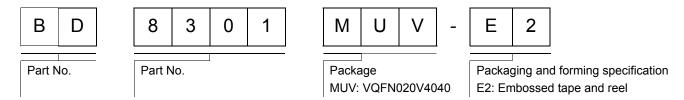
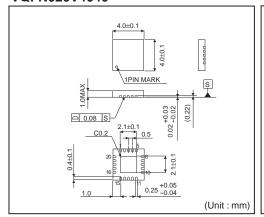


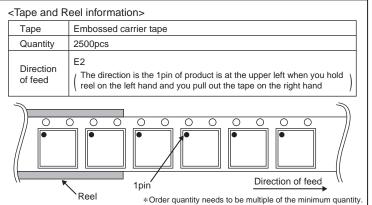
Fig.30 Example of simple structure of Bipolar IC

Ordering part number



VQFN020V4040





Notes

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