

### Smart Highside High Current Power Switch

#### Features

- Overload protection
- Current limitation
- Short circuit protection
- Overtemperature protection
- Overvoltage protection (including load dump)
- Clamp of negative voltage at output
- Fast deenergizing of inductive loads <sup>1)</sup>
- Low ohmic inverse current operation
- Reverse battery protection
- Diagnostic feedback with load current sense
- Open load detection via current sense
- Loss of  $V_{bb}$  protection<sup>2)</sup>
- **Electrostatic discharge (ESD)** protection

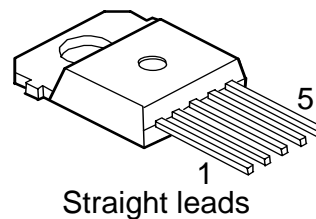
#### Product Summary

|                                  |              |            |            |
|----------------------------------|--------------|------------|------------|
| Overvoltage protection           | $V_{bb(AZ)}$ | 63         | V          |
| Output clamp                     | $V_{ON(CL)}$ | 42         | V          |
| Operating voltage                | $V_{bb(on)}$ | 5.0 ... 34 | V          |
| On-state resistance              | $R_{ON}$     | 2.9        | m $\Omega$ |
| Load current (ISO)               | $I_L(ISO)$   | 132        | A          |
| Short circuit current limitation | $I_L(SCp)$   | 400        | A          |
| Current sense ratio              | $I_L : I_S$  | 25 000     |            |

#### Application

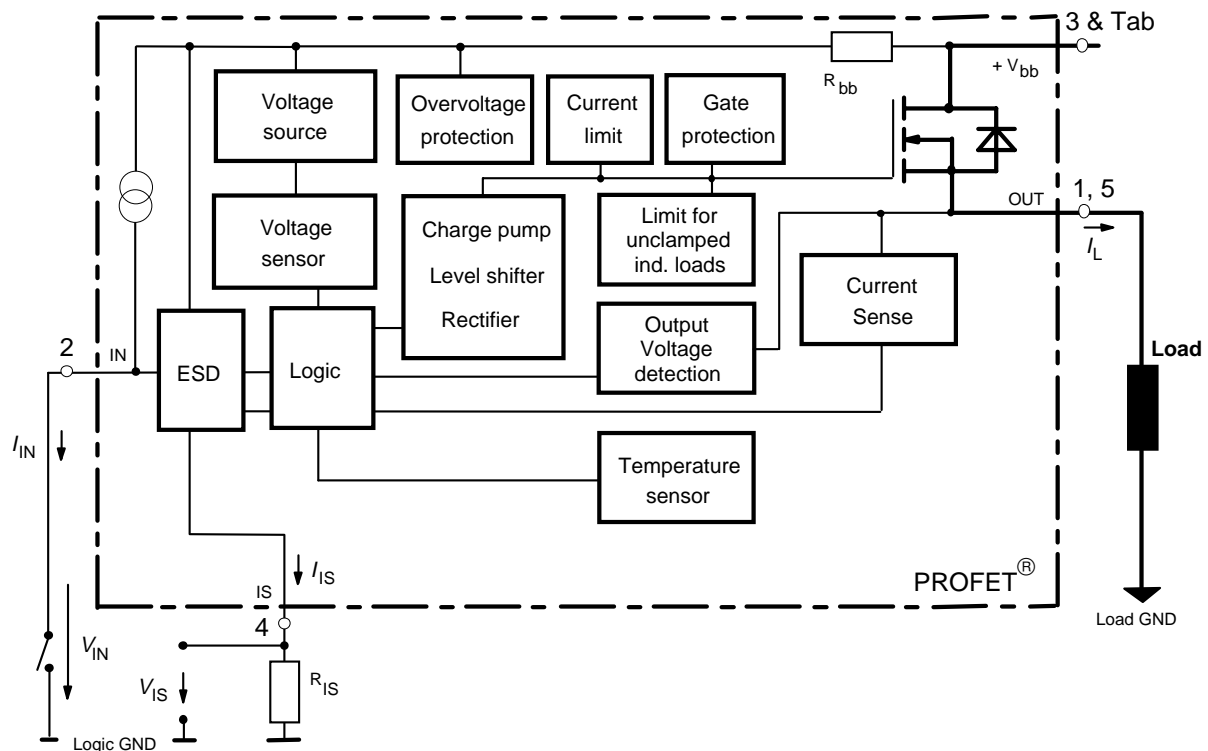
- Power switch with current sense diagnostic feedback for 12V and 24V DC grounded loads
- Most suitable for loads with high inrush current like lamps and motors; all types of resistive and inductive loads
- Replaces electromechanical relays, fuses and discrete circuits

TO-218AB/5



#### General Description

N channel vertical power FET with charge pump, current controlled input and diagnostic feedback with load current sense, integrated in Smart SiPMOS<sup>®</sup> chip on chip technology. Fully protected by embedded protection functions.



1) With additional external diode.

2) Additional external diode required for energized inductive loads (see page9).

| Pin | Symbol            | Function   |
|-----|-------------------|--|
| 1   | OUT O             | Output to the load. The pins 1 and 5 must be shorted with each other especially in high current applications <sup>3)</sup>   |
| 2   | IN I              | Input, activates the power switch in case of short to ground   |
| 3   | V <sub>bb</sub> + | Positive power supply voltage, the tab is electrically connected to this pin. In high current applications the tab should be used for the V <sub>bb</sub> connection instead of this pin <sup>4)</sup> . |
| 4   | IS S              | Diagnostic feedback providing a sense current proportional to the load current; zero current on failure (see Truth Table on page 7)  |
| 5   | OUT O             | Output to the load. The pins 1 and 5 must be shorted with each other especially in high current applications <sup>3)</sup>   |

### Maximum Ratings at $T_j = 25\text{ °C}$ unless otherwise specified

| Parameter  | Symbol                | Values       | Unit |
|--|-----------------------|--------------|------|
| Supply voltage (overvoltage protection see page 4)   | $V_{bb}$              | 42           | V    |
| Supply voltage for full short circuit protection, resistive load or $L < t_{bd}\ \mu\text{H}$ $T_{j,start} = -40 \dots +150\text{ °C}$ :   | $V_{bb}$              | 34           | V    |
| Load current (short circuit current, see page 5)   | $I_L$                 | self-limited | A    |
| Load dump protection $V_{LoadDump} = U_A + V_S$ , $U_A = 13.5\text{ V}$<br>$R_l^{5)} = 2\ \Omega$ , $R_L = 0.1\ \Omega$ , $t_d = 200\text{ ms}$ ,<br>IN, IS = open or grounded   | $V_{Load\ dump}^{6)}$ | 80           | V    |
| Operating temperature range  | $T_j$                 | -40 ... +150 | °C   |
| Storage temperature range  | $T_{stg}$             | -55 ... +150 |      |
| Power dissipation (DC), $T_C \leq 25\text{ °C}$  | $P_{tot}$             | 310          | W    |
| Inductive load switch-off energy dissipation, single pulse<br>$V_{bb} = 12\text{ V}$ , $T_{j,start} = 150\text{ °C}$ , $T_C = 150\text{ °C const.}$ ,<br>$I_L = t_{bd} (>=20)\text{ A}$ , $Z_L = t_{bd}\text{ mH}$ , $0\ \Omega$ , see diagrams on page 10 | $E_{AS}$              | tbd          | J    |
| Electrostatic discharge capability (ESD)<br>Human Body Model acc. MIL-STD883D, method 3015.7 and ESD assn. std. S5.1-1993, $C = 100\text{ pF}$ , $R = 1.5\text{ k}\Omega$  | $V_{ESD}$             | 2.0          | kV   |
| Current through input pin (DC)   | $I_{IN}$              | +15, -250    | mA   |
| Current through current sense status pin (DC)<br>see internal circuit diagrams on page 8   | $I_{IS}$              | +15, -250    |      |

3) Not shorting all outputs will considerably increase the on-state resistance, reduce the peak current capability and decrease the current sense accuracy

4) Otherwise add up to  $0.5\text{ m}\Omega$  (depending on used length of the pin) to the  $R_{ON}$  if the pin is used instead of the tab.

5)  $R_l$  = internal resistance of the load dump test pulse generator.

6)  $V_{Load\ dump}$  is setup without the DUT connected to the generator per ISO 7637-1 and DIN 40839.



### Thermal Characteristics

| Parameter and Conditions   | Symbol          | Values |     |      | Unit |
|--|-----------------|--------|-----|------|------|
|  |                 | min    | typ | max  |      |
| Thermal resistance<br>chip - case:<br>junction - ambient (free air): | $R_{thJC}^{7)}$ | --     | --  | 0.40 | K/W  |
|  | $R_{thJA}$      | --     | 30  | --   |      |

### Electrical Characteristics

| Parameter and Conditions   | Symbol | Values |     |     | Unit |
|--|--------|--------|-----|-----|------|
|  |        | min    | typ | max |      |
| at $T_j = -40 \dots +150^\circ\text{C}$ , $V_{bb} = 12\text{V}$ unless otherwise specified |        |        |     |     |      |

### Load Switching Capabilities and Characteristics

|  |  |            |                          |                          |                        |
|--|--|------------|--------------------------|--------------------------|------------------------|
| On-state resistance (Tab to pins 1,5, see measurement circuit page 8)<br>$I_L = \text{tbd} (>=20)\text{A}$ , $T_j = 25^\circ\text{C}$ :<br>$V_{IN} = 0$ , $I_L = \text{tbd} (>=20)\text{A}$ , $T_j = 150^\circ\text{C}$ :<br>$I_L = \text{tbd A}$ , $T_j = 150^\circ\text{C}$ :<br>$V_{bb} = \text{tbd V}^8)$ , $I_L = \text{tbd A}$ , $T_j = 150^\circ\text{C}$ : | $R_{ON}$<br><br><br><br>$R_{ON(Static)}$ | --         | 2.4<br>4.6<br>tbd<br>tbd | 2.9<br>5.7<br>tbd<br>tbd | $m\Omega$              |
| Nominal load current <sup>9)</sup> (Tab to pins 1,5)<br>ISO 10483-1/6.7: $V_{ON} = 0.5\text{V}$ , $T_C = 85^\circ\text{C}$ <sup>10)</sup>  | $I_{L(ISO)}$                             | 111        | 132                      | --                       |                        |
| Maximum load current in resistive range<br>(Tab to pins 1,5) $V_{ON} = 1.8\text{V}$ , $T_C = 25^\circ\text{C}$ :<br>see diagram on page 13 $V_{ON} = 1.8\text{V}$ , $T_C = 150^\circ\text{C}$ :  | $I_{L(Max)}$                             | tbd<br>tbd | --<br>--                 | --<br>--                 | A                      |
| Turn-on time <sup>11)</sup> $I_{IN}$  to 90% $V_{OUT}$ :  | $t_{on}$                                 | 130        | --                       | 550                      | $\mu\text{s}$          |
| Turn-off time $I_{IN}$  to 10% $V_{OUT}$ :<br>$R_L = 1\Omega$ , $T_j = -40\dots+150^\circ\text{C}$  | $t_{off}$                                | 60         | --                       | 240                      |                        |
| Slew rate on <sup>11)</sup> (10 to 30% $V_{OUT}$ )<br>$R_L = 1\Omega$  | $dV/dt_{on}$                             | --         | 0.8                      | --                       | $\text{V}/\mu\text{s}$ |
| Slew rate off <sup>11)</sup> (70 to 40% $V_{OUT}$ )<br>$R_L = 1\Omega$   | $-dV/dt_{off}$                           | --         | 0.8                      | --                       | $\text{V}/\mu\text{s}$ |

### Inverse Load Current Operation

|   |  |     |            |            |           |
|---|--|-----|------------|------------|-----------|
| On-state resistance (Pins 1,5 to pin 3)<br>$V_{bIN} = 12\text{V}$ , $I_L = -\text{tbd} (>=20)\text{A}$<br>see diagram on page 10    | $T_j = 25^\circ\text{C}$ :<br>$T_j = 150^\circ\text{C}$ :<br>$R_{ON(inv)}$ | --  | 2.4<br>4.6 | 2.9<br>5.7 | $m\Omega$ |
| Nominal inverse load current (Pins 1,5 to Tab)<br>$V_{ON} = -0.5\text{V}$ , $T_C = 85^\circ\text{C}$ <sup>10)</sup>                 | $I_{L(inv)}$   | 111 | 132        | --         |           |
| Drain-source diode voltage ( $V_{out} > V_{bb}$ )<br>$I_L = -\text{tbd} (>=20)\text{A}$ , $I_{IN} = 0$ , $T_j = +150^\circ\text{C}$ | $-V_{ON}$  | --  | tbd        | --         | mV        |

7) Thermal resistance  $R_{thCH}$  case to heatsink (about 0.25 K/W with silicone paste) not included!

8) Decrease of  $V_{bb}$  below 10 V causes slowly a dynamic increase of  $R_{ON}$  to a higher value of  $R_{ON(Static)}$ . As long as  $V_{bIN} > V_{bIN(u) \text{ max}}$ ,  $R_{ON}$  increase is less than 10 % per second for  $T_j < 85^\circ\text{C}$ .

9) Not tested, specified by design.

10)  $T_j$  is about  $105^\circ\text{C}$  under these conditions.

11) See timing diagram on page 14.

| Parameter and Conditions<br>at $T_j = -40 \dots +150^\circ\text{C}$ , $V_{bb} = 12\text{V}$ unless otherwise specified | Symbol | Values |     |     | Unit |
|--|--------|--------|-----|-----|------|
|  |        | min    | typ | max |      |

### Operating Parameters

|  |                |  |          |          |          |               |
|--|----------------|--|----------|----------|----------|---------------|
| Operating voltage ( $V_{IN} = 0$ ) Fehler! Textmarke nicht definiert,<br>12) | $V_{bb(on)}$   | 5.0  | --       | 34       | V        |               |
| Undervoltage shutdown 13)  | $V_{bIN(u)}$   | --   | 3.5      | 4.5      | V        |               |
| Undervoltage start of charge pump<br>see diagram page 15                     | $V_{bIN(ucp)}$ | --   | 5        | 6.5      | V        |               |
| Overvoltage protection <sup>14)</sup><br>$I_{bb} = 15\text{ mA}$             | $V_{bIN(z)}$   | $T_j = -40^\circ\text{C}$ :<br>$T_j = 25\dots+150^\circ\text{C}$ : | 60<br>62 | --<br>66 | --<br>-- | V             |
| Standby current<br>$I_{IN} = 0$  | $I_{bb(off)}$  | $T_j = -40\dots+25^\circ\text{C}$ :<br>$T_j = 150^\circ\text{C}$ : | --<br>-- | 15<br>25 | 25<br>60 | $\mu\text{A}$ |

### Protection Functions

|   |                |   |                  |                   |                  |               |
|---|----------------|---|------------------|-------------------|------------------|---------------|
| Short circuit current limit (Tab to pins 1,5)<br>$V_{ON} = 12\text{V}$ , time until shutdown max. $300\mu\text{s}$  | $I_L(SCp)$     | $T_c = -40^\circ\text{C}$ :<br>$T_c = 25^\circ\text{C}$ :<br>$T_c = +150^\circ\text{C}$ : | --<br>tbd<br>tbd | 460<br>400<br>280 | --<br>tbd<br>tbd | A             |
| Short circuit shutdown delay after input current<br>positive slope, $V_{ON} > V_{ON(SC)}$<br>min. value valid only if input "off-signal" time exceeds $30\mu\text{s}$ | $t_d(SC)$      |   | 80               | --                | 300              | $\mu\text{s}$ |
| Output clamp <sup>15)</sup><br>(inductive load switch off)  | $-V_{OUT(CL)}$ | $I_L = 40\text{ mA}$ :<br>$I_L = 20\text{ A}$ :   | --<br>--         | 15<br>17          | --<br>--         | V             |
| Output clamp (inductive load switch off)<br>at $V_{OUT} = V_{bb} - V_{ON(CL)}$ (e.g. overvoltage)<br>$I_L = 40\text{ mA}$   | $V_{ON(CL)}$   |   | 39               | 42                | 46               | V             |
| Short circuit shutdown detection voltage<br>(pin 3 to pins 1,5)   | $V_{ON(SC)}$   |   | --               | 6                 | --               | V             |

12) For all voltages  $0 \dots 34\text{V}$  the device is fully protected against overtemperature and short circuit.

13)  $V_{bIN} = V_{bb} - V_{IN}$  see diagram on page 8. When  $V_{bIN}$  increases from less than  $V_{bIN(u)}$  up to  $V_{bIN(ucp)} = 5\text{V}$  (typ.) the charge pump is not active and  $V_{OUT} \approx V_{bb} - 3\text{V}$ .

14) See also  $V_{ON(CL)}$  in circuit diagram on page 9.

15) This output clamp can be "switched off" by using an additional diode at the IS-Pin (see page 8). If the diode is used,  $V_{OUT}$  is clamped to  $V_{bb} - V_{ON(CL)}$  at inductive load switch off.

| Parameter and Conditions<br>at $T_j = -40 \dots +150 \text{ }^\circ\text{C}$ , $V_{bb} = 12 \text{ V}$ unless otherwise specified | Symbol          | Values |     |     | Unit             |
|---|-----------------|--------|-----|-----|------------------|
|   |                 | min    | typ | max |                  |
| Thermal overload trip temperature   | $T_{jt}$        | 150    | --  | --  | $^\circ\text{C}$ |
| Thermal hysteresis  | $\Delta T_{jt}$ | --     | 10  | --  | K                |

### Reverse Battery

|   |                      |    |          |          |                  |
|---|----------------------|----|----------|----------|------------------|
| Reverse battery voltage <sup>16)</sup>  | $-V_{bb}$            | -- | --       | 16       | V                |
| On-state resistance (Pins 1,5 to pin 3) $T_j = 25 \text{ }^\circ\text{C}$ :<br>$V_{bb} = -12 \text{ V}$ , $V_{IN} = 0$ , $I_L = -\text{tbd}$ ( $\geq 20$ ) A, $R_{IS} = 1 \text{ k}\Omega$ $T_j = 150 \text{ }^\circ\text{C}$ : | $R_{ON(\text{rev})}$ | -- | 2.8<br>0 | tbd<br>0 | $\text{m}\Omega$ |
| Integrated resistor in $V_{bb}$ line  | $R_{bb}$             | -- | 120      | --       | $\Omega$         |

### Diagnostic Characteristics

|  |                              |  |                |   |                |
|--|------------------------------|--|----------------|---|----------------|
| Current sense ratio, static on-condition,<br>$k_{ILIS} = I_L : I_{IS}$ , $V_{ON} < 1.5 \text{ V}^{17)}$ ,<br>$V_{IS} < V_{OUT} - 5 \text{ V}$ , $V_{bIN} > 4.5 \text{ V}$                      | $k_{ILIS}$                   | -40 $^\circ\text{C}$ :<br>25 $^\circ\text{C}$ :<br>150 $^\circ\text{C}$ :              | --<br>--<br>-- | 26 530<br>25 430<br>23 520  | --<br>--<br>-- |
| see diagram on page 12<br>$I_L = 180 \text{ A}$ :<br>$I_L = 50 \text{ A}$ :<br>$I_L = 25 \text{ A}$ :<br>$I_L = 10 \text{ A}$ :<br>$I_{IN} = 0$ (e.g. during deenergizing of inductive loads): |                              |  |                | -40 $^\circ\text{C}$ :<br>+25 $^\circ\text{C}$ :<br>150 $^\circ\text{C}$ :<br>$\pm 4.5\%$<br>$\pm 4.2\%$<br>$\pm 4.0\%$<br>$\pm 8.9\%$<br>$\pm 7.5\%$<br>$\pm 6.1\%$<br>$\pm 15\%$<br>$\pm 12\%$<br>$\pm 9.0\%$<br>$\pm 46\%$<br>$\pm 36\%$<br>$\pm 24\%$ |                |
| Sense current saturation   | $I_{IS,lim}$                 |  | 6.5            | --  | --             |
| Current sense leakage current<br>$I_{IN} = 0$ , $V_{IS} = 0$ :<br>$V_{IN} = 0$ , $V_{IS} = 0$ , $I_L \leq 0$ :   | $I_{IS(LL)}$<br>$I_{IS(LH)}$ |  | --             | --  | 0.5<br>--      |
| Current sense settling time <sup>18)</sup> after positive input slope (90% of $I_{IS}$ static) $I_L = 0 / \text{tbd}$ ( $\geq 20$ ) A:   | $t_{son(IS)}$                |  | --             | tbd   | 500            |
| Current sense settling time <sup>18)</sup> after negative input slope (10% of $I_{IS}$ static) $I_L = \text{tbd}$ ( $\geq 20$ ) / 0 A:   | $t_{soff(IS)}$               |  | --             | tbd   | 500            |
| Current sense settling time <sup>18)</sup> after change of load current (60% to 90%) $I_L = 15 / \text{tbd}$ ( $\geq 20$ ) A:  | $t_{slc(IS)}$                |  | --             | tbd   | 500            |
| Overvoltage protection<br>$I_{bb} = 15 \text{ mA}$   | $V_{bIS(Z)}$                 | $T_j = -40 \text{ }^\circ\text{C}$ :<br>$T_j = 25 \dots +150 \text{ }^\circ\text{C}$ : | 60<br>62       | --<br>66  | --<br>--       |

<sup>16)</sup> The reverse load current through the intrinsic drain-source diode has to be limited by the connected load (as it is done with all polarity symmetric loads). Note that under off-conditions ( $I_{IN} = I_{IS} = 0$ ) the power transistor is not activated. This results in raised power dissipation due to the higher voltage drop across the intrinsic drain-source diode. The temperature protection is not active during reverse current operation! Increasing reverse battery voltage capability is simply possible as described on page 9.

<sup>17)</sup> If  $V_{ON}$  is higher, the sense current is no longer proportional to the load current due to sense current saturation, see  $I_{IS,lim}$ .

<sup>18)</sup> Not tested, specified by design.

| Parameter and Conditions<br>at $T_j = -40 \dots +150 \text{ }^\circ\text{C}$ , $V_{bb} = 12 \text{ V}$ unless otherwise specified | Symbol | Values |     |     | Unit |
|---|--------|--------|-----|-----|------|
|   |        | min    | typ | max |      |

### Input

|   |               |    |    |    |               |
|---|---------------|----|----|----|---------------|
| Input and operating current (see diagram page 13)<br>IN grounded ( $V_{IN} = 0$ ) | $I_{IN(on)}$  | -- | 1  | 2  | mA            |
| Input current for turn-off <sup>19)</sup>   | $I_{IN(off)}$ | -- | -- | 80 | $\mu\text{A}$ |

### Truth Table

|                               | Input current level | Output level     | Current Sense $I_{IS}$  | Remark  |
|-------------------------------|---------------------|------------------|-------------------------|---|
| Normal operation              | L<br>H              | L<br>H           | 0<br>nominal            | $=I_L / k_{IIS}$ , up to $I_{IS}=I_{IS,lim}$                                    |
| Very high load current        | H                   | H                | $I_{IS,lim}$            | up to $V_{ON}=V_{ON(Fold\ back)}$<br>$I_{IS}$ no longer proportional to $I_L$   |
| Current-limitation            | H                   | H                | 0                       | $V_{ON} > V_{ON(Fold\ back)}$<br>if $V_{ON} > V_{ON(SC)}$ , shutdown will occur |
| Short circuit to GND          | L                   | L                | 0                       |   |
|                               | H                   | L                | 0                       |   |
| Over-temperature              | L                   | L                | 0                       |   |
|                               | H                   | L                | 0                       |   |
| Short circuit to $V_{bb}$     | L                   | H                | 0                       |   |
|                               | H                   | H                | <nominal <sup>20)</sup> |   |
| Open load                     | L                   | Z <sup>21)</sup> | 0                       |   |
|                               | H                   | H                | 0                       |   |
| Negative output voltage clamp | L                   | L                | 0                       |   |
| Inverse load current          | L                   | H                | 0                       |   |
|                               | H                   | H                | 0                       |   |

L = "Low" Level

H = "High" Level

Overtemperature reset via input:  $I_{IN}=\text{low}$  and  $T_j < T_{jt}$  (see diagram on page Fehler! Textmarke nicht definiert.)

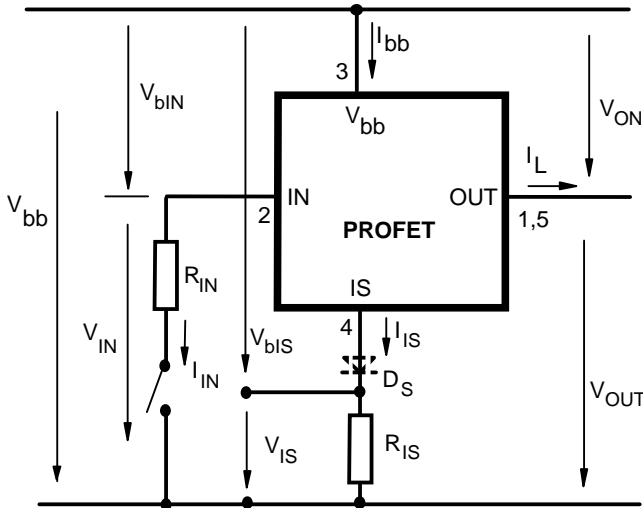
Short circuit to GND: Shutdown remains latched until next reset via input (see diagram on page 14)

<sup>19)</sup> We recommend the resistance between IN and GND to be less than  $0.5 \text{ k}\Omega$  for turn-on and more than  $500 \text{ k}\Omega$  for turn-off. Consider that when the device is switched off ( $I_{IN} = 0$ ) the voltage between IN and GND reaches almost  $V_{bb}$ .

<sup>20)</sup> Low ohmic short to  $V_{bb}$  may reduce the output current  $I_L$  and can thus be detected via the sense current  $I_{IS}$ .

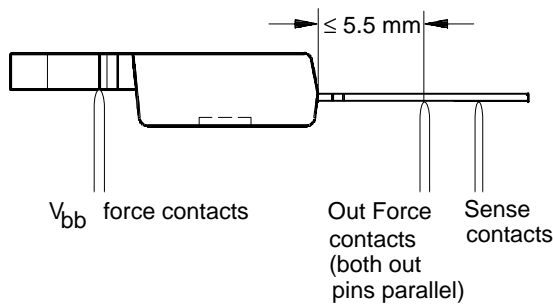
<sup>21)</sup> Power Transistor "OFF", potential defined by external impedance.

### Terms

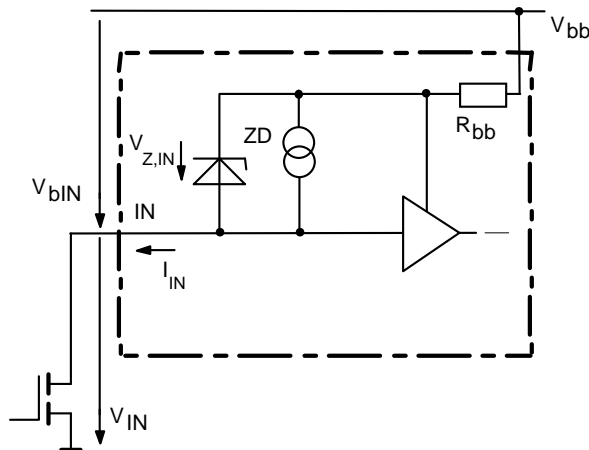


Two or more devices can easily be connected in parallel to increase load current capability.

### R<sub>ON</sub> measurement layout

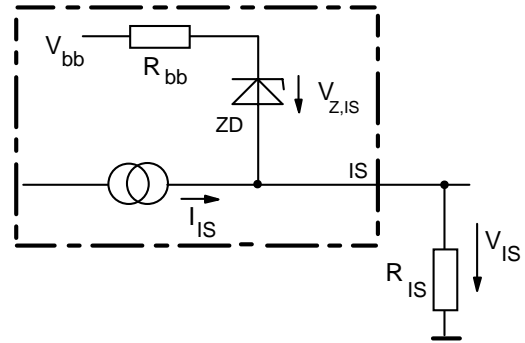


### Input circuit (ESD protection)



When the device is switched off ( $I_{IN} = 0$ ) the voltage between IN and GND reaches almost  $V_{bb}$ . Use a mechanical switch, a bipolar or MOS transistor with appropriate breakdown voltage as driver.  
 $V_{Z,IN} = 66\text{ V (typ.)}$ .

### Current sense status output

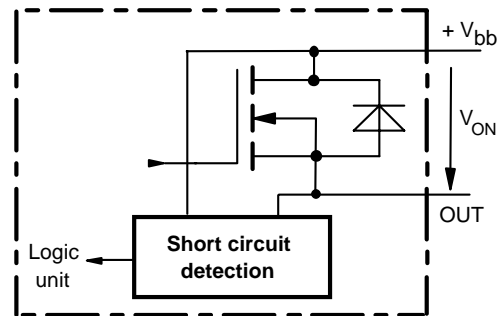


$V_{Z,IS} = 66\text{ V (typ.)}$ ,  $R_{IS} = 1\text{ k}\Omega$  nominal (or  $1\text{ k}\Omega/n$ , if  $n$  devices are connected in parallel).  $I_S = I_L/k_{IIS}$  can be only driven by the internal circuit as long as  $V_{out} - V_{IS} > 5\text{ V}$ . If you want to measure load currents up to  $I_{L(M)}$ ,  $R_{IS}$  should be less than  $\frac{V_{bb} - 5\text{ V}}{I_{L(M)} / k_{IIS}}$ .

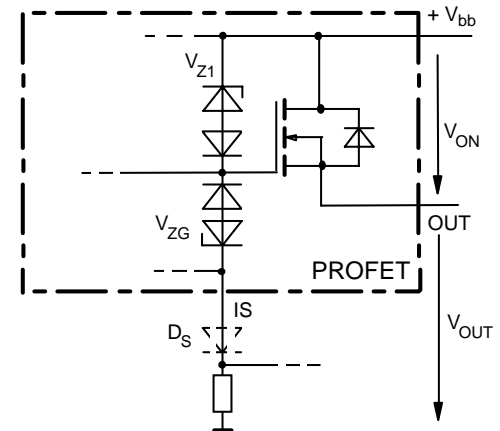
Note: For large values of  $R_{IS}$  the voltage  $V_{IS}$  can reach almost  $V_{bb}$ . See also overvoltage protection. If you don't use the current sense output in your application, you can leave it open.

### Short circuit detection

Fault Condition:  $V_{ON} > V_{ON(SC)}$  (6 V typ.) and  $t > t_{d(SC)}$  (80 ...300  $\mu\text{s}$ ).



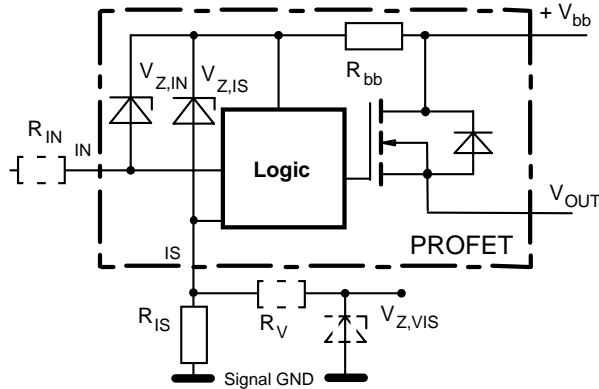
### Inductive and overvoltage output clamp



$V_{ON}$  is clamped to  $V_{ON(CL)} = 42\text{ V typ.}$  At inductive load switch-off without  $D_S$ ,  $V_{OUT}$  is clamped to  $V_{OUT(CL)} = -15\text{ V typ.}$  via  $V_{ZG}$ . With  $D_S$ ,  $V_{OUT}$  is clamped to  $V_{bb} - V_{ON(CL)}$  via  $V_{Z1}$ . Using  $D_S$  gives faster deenergizing of

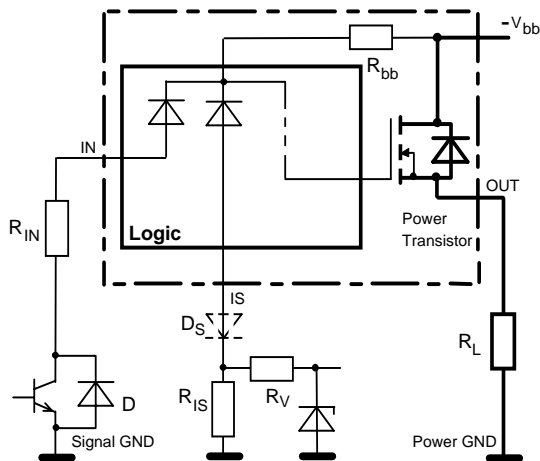
the inductive load, but higher peak power dissipation in the PROFET.

### Overvoltage protection of logic part



$R_{bb} = 120\Omega$  typ.,  $V_{Z,IN} = V_{Z,IS} = 66V$  typ.,  $R_{IS} = 1k\Omega$  nominal. Note that when overvoltage exceeds  $71V$  typ. a voltage above  $5V$  can occur between  $IS$  and  $GND$ , if  $R_V, V_{Z,VIS}$  are not used.

### Reverse battery protection



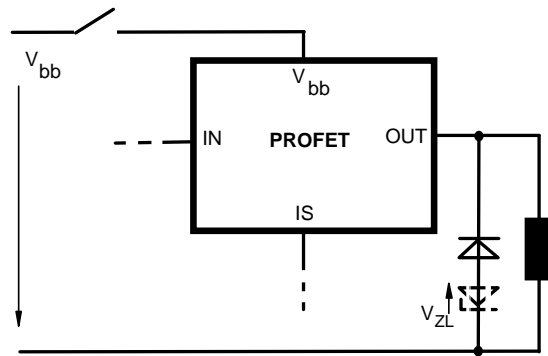
$R_V \geq 1k\Omega$ ,  $R_{IS} = 1k\Omega$  nominal. Add  $R_{IN}$  for reverse battery protection in applications with  $V_{bb}$  above  $16V^{(16)}$ ; recommended value:  $\frac{1}{R_{IN}} + \frac{1}{R_{IS}} + \frac{1}{R_V} = \frac{0.1A}{|V_{bb}| - 12V}$  if  $D_S$  is not used (or  $\frac{1}{R_{IN}} = \frac{0.1A}{|V_{bb}| - 12V}$  if  $D_S$  is used).

To minimize power dissipation at reverse battery operation, the summarized current into the  $IN$  and  $IS$  pin should be about  $120mA$ . The current can be provided by using a small signal diode  $D$  in parallel to the input switch, by using a MOSFET input switch or by proper adjusting the current through  $R_{IS}$  and  $R_V$ .

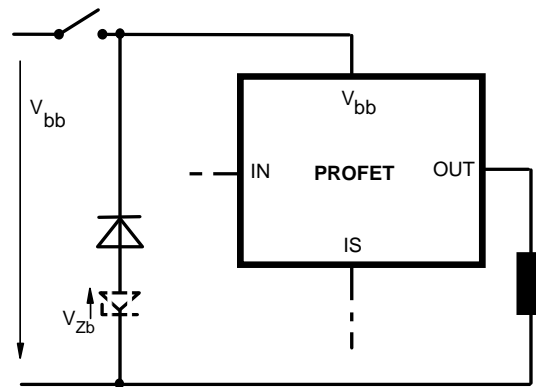
### $V_{bb}$ disconnect with energized inductive load

Provide a current path with load current capability by using a diode, a Z-diode, or a varistor. ( $V_{ZL} < 72V$  or  $V_{Zb} < 30V$  if  $R_{IN}=0$ ). For higher clamp voltages currents at  $IN$  and  $IS$  have to be limited to  $250mA$ .

Version a:

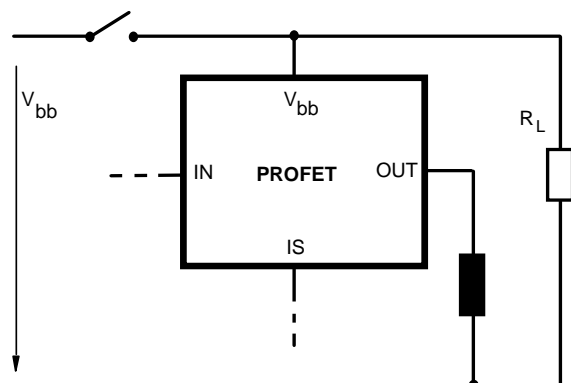


Version b:



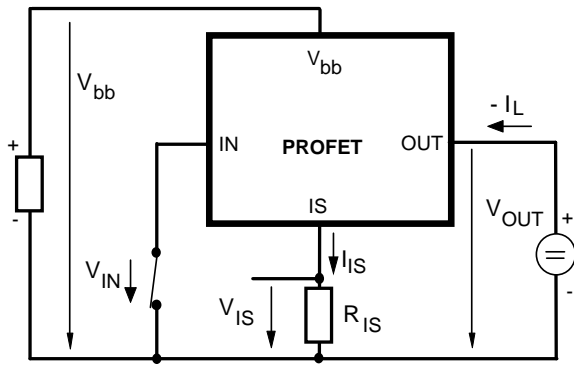
Note that there is no reverse battery protection when using a diode without additional Z-diode  $V_{ZL}, V_{Zb}$ .

Version c: Sometimes a necessary voltage clamp is given by non inductive loads  $R_L$  connected to the same switch and eliminates the need of clamping circuit:



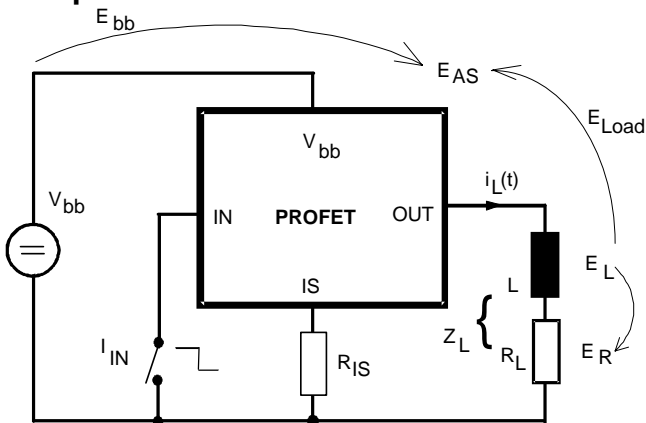


### Inverse load current operation



The device is specified for inverse load current operation ( $V_{OUT} > V_{bb} > 0V$ ). The current sense feature is not available during this kind of operation ( $I_{IS} = 0$ ). With  $I_{IN} = 0$  (e.g. input open) only the intrinsic drain source diode is conducting resulting in considerably increased power dissipation. If the device is switched on ( $V_{IN} = 0$ ), this power dissipation is decreased to the much lower value  $R_{ON(INV)} \cdot I^2$  (specifications see page 4).  
 Note: *Temperature protection during inverse load current operation is not possible!*

### Inductive load switch-off energy dissipation



Energy stored in load inductance:

$$E_L = \frac{1}{2} \cdot L \cdot I_L^2$$

While demagnetizing load inductance, the energy dissipated in PROFET is

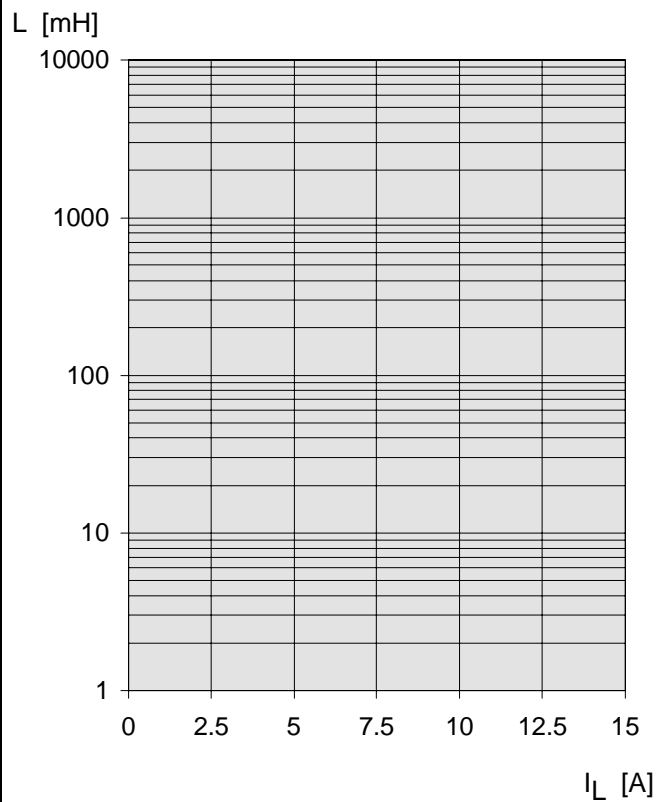
$$E_{AS} = E_{bb} + E_L - E_R = \int V_{ON(CL)} \cdot i_L(t) dt,$$

with an approximate solution for  $R_L > 0 \Omega$ :

$$E_{AS} = \frac{I_L \cdot L}{2 \cdot R_L} (V_{bb} + |V_{OUT(CL)}|) \ln \left( 1 + \frac{I_L \cdot R_L}{|V_{OUT(CL)}|} \right)$$

### Maximum allowable load inductance for a single switch off

$L = f(I_L)$ ;  $T_{j,start} = 150^\circ C$ ,  $V_{bb} = 12V$ ,  $R_L = 0 \Omega$



### Options Overview

| Type  | BTS | 550P<br>650P          | 555                   |
|---|-----|-----------------------|-----------------------|
| Overtemperature protection with hysteresis<br>$T_j > 150\text{ °C}$ , latch function <sup>22)</sup>   |     | X                     | X                     |
| $T_j > 150\text{ °C}$ , with auto-restart on cooling  |     | X                     |                       |
| Short circuit to GND protection<br>switches off when $V_{ON} > 6\text{ V}$ typ.<br>(when first turned on after approx. $180\text{ }\mu\text{s}$ ) |     | X                     | X                     |
| Overvoltage shutdown  |     | -                     | -                     |
| Output negative voltage transient limit<br>to $V_{bb} - V_{ON(CL)}$<br>to $V_{OUT} = -15\text{ V}$ typ  |     | X<br>X <sup>23)</sup> | X<br>X <sup>23)</sup> |

<sup>22)</sup> Latch except when  $V_{bb} - V_{OUT} < V_{ON(SC)}$  after shutdown. In most cases  $V_{OUT} = 0\text{ V}$  after shutdown ( $V_{OUT} \neq 0\text{ V}$  only if forced externally). So the device remains latched unless  $V_{bb} < V_{ON(SC)}$  (see page 5). No latch between turn on and  $t_{d(SC)}$ .

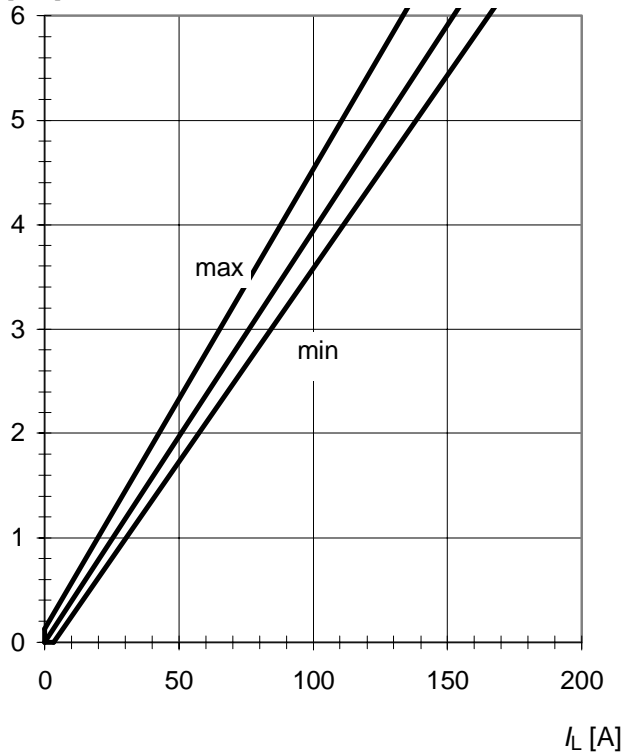
<sup>23)</sup> Can be "switched off" by using a diode  $D_S$  (see page 8) or leaving open the current sense output.

### Characteristics

**Current sense versus load current:**

$$I_{IS} = f(I_L)$$

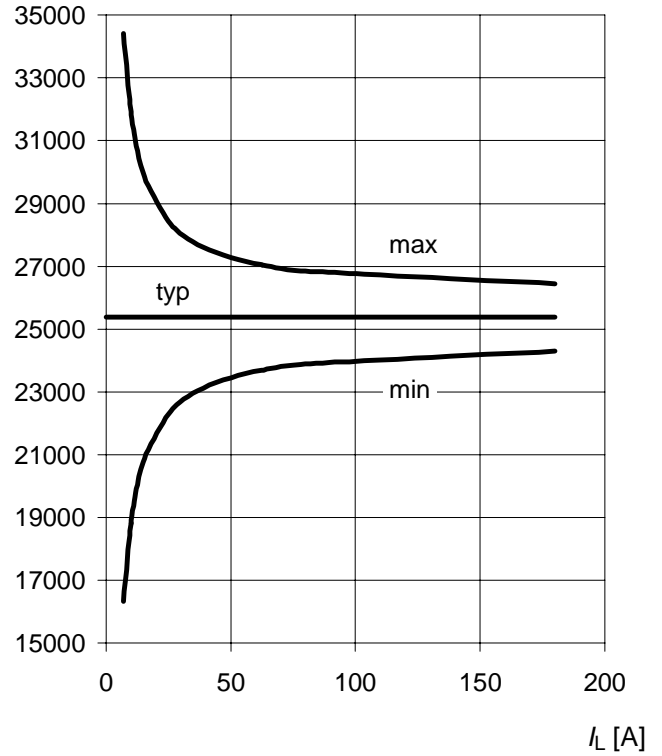
$I_{IS}$  [mA]



**Current sense ratio:**

$$K_{ILIS} = f(I_L), T_J = 25\text{ °C}$$

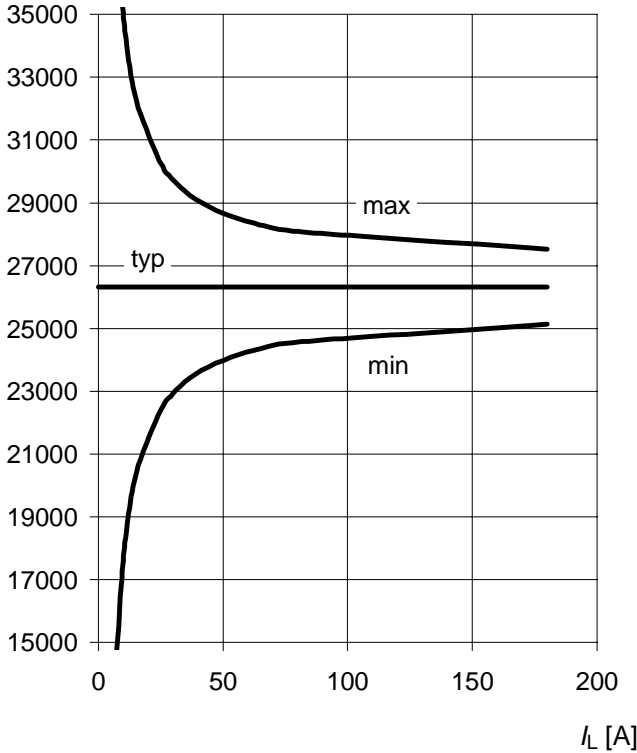
$K_{ILIS}$



**Current sense ratio:**

$$K_{ILIS} = f(I_L), T_J = -40\text{ °C}$$

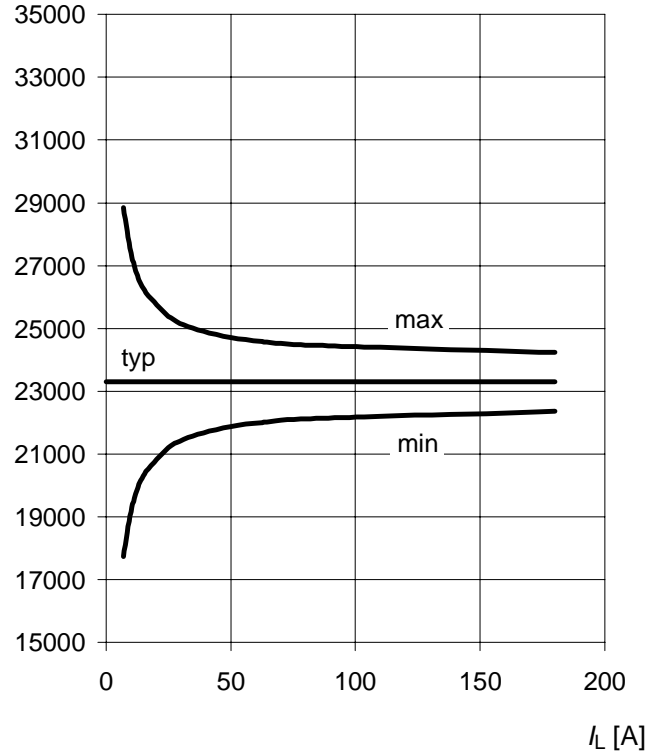
$K_{ILIS}$



**Current sense ratio:**

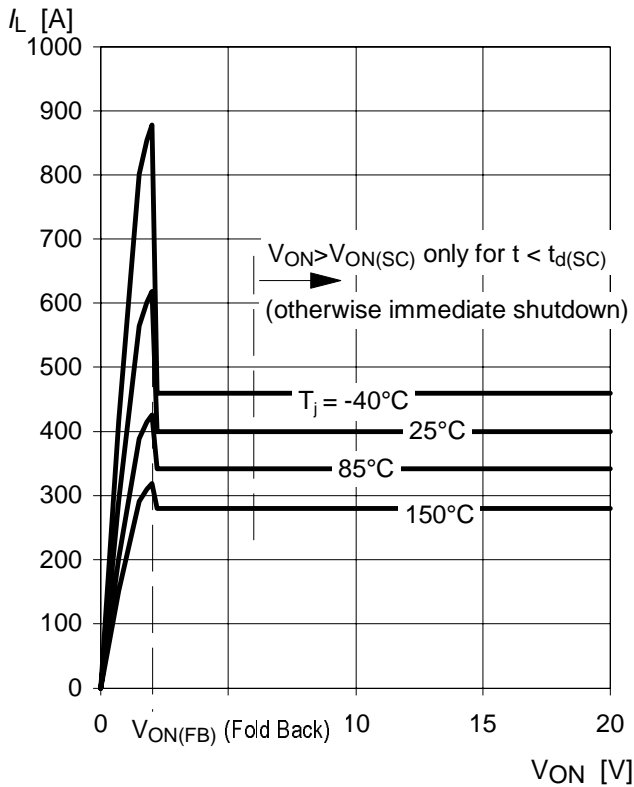
$$K_{ILIS} = f(I_L), T_J = 150\text{ °C}$$

$K_{ILIS}$



### Typ. current limitation characteristic

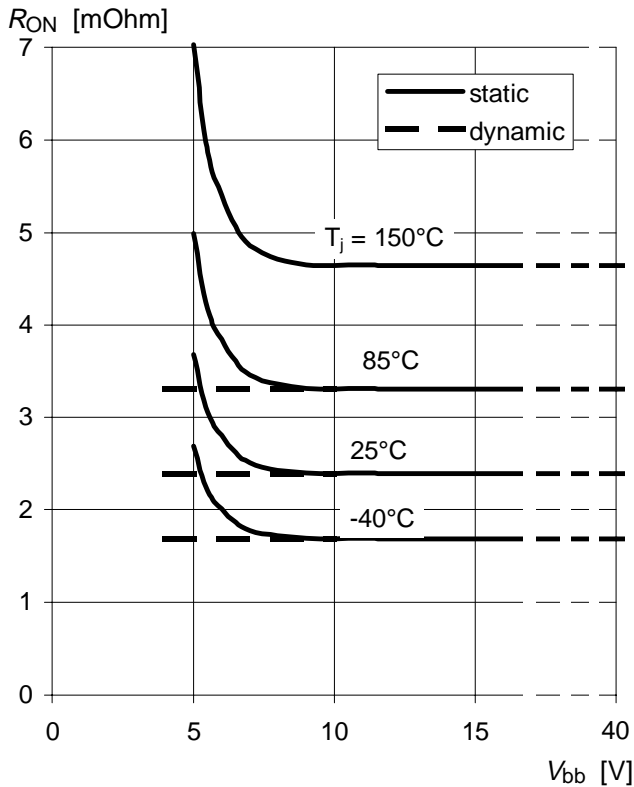
$$I_L = f(V_{ON}, T_j)$$



In case of  $V_{ON} > V_{ON(SC)}$  (typ. 6 V) the device will be switched off by internal short circuit detection.

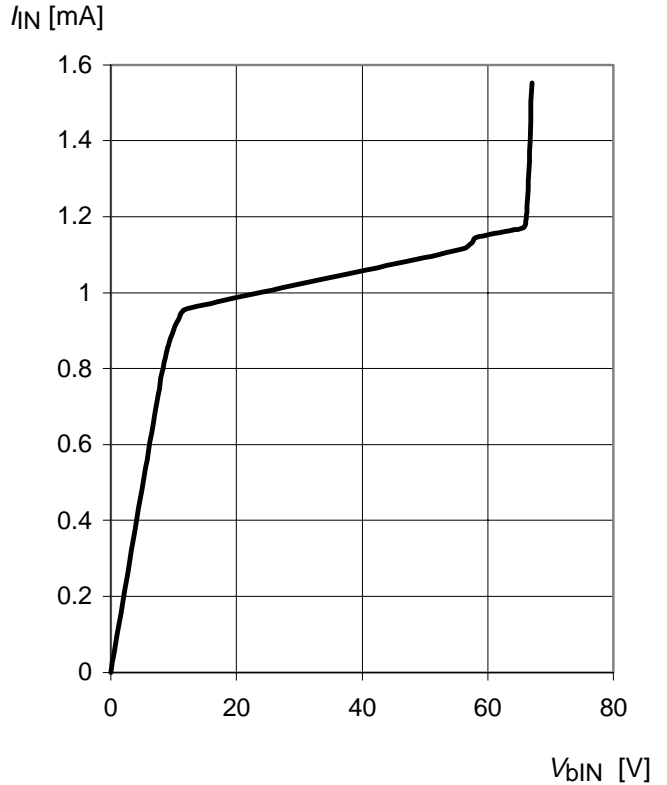
### Typ. on-state resistance

$$R_{ON} = f(V_{bb}, T_j); I_L = tbd (>=20) \text{ A}; V_{IN} = 0$$



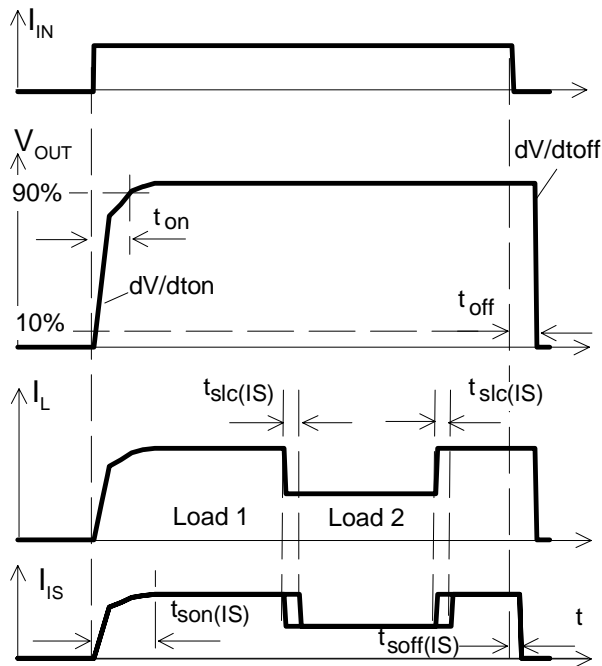
### Typ. input current

$$I_{IN} = f(V_{bIN}), V_{bIN} = V_{bb} - V_{IN}$$



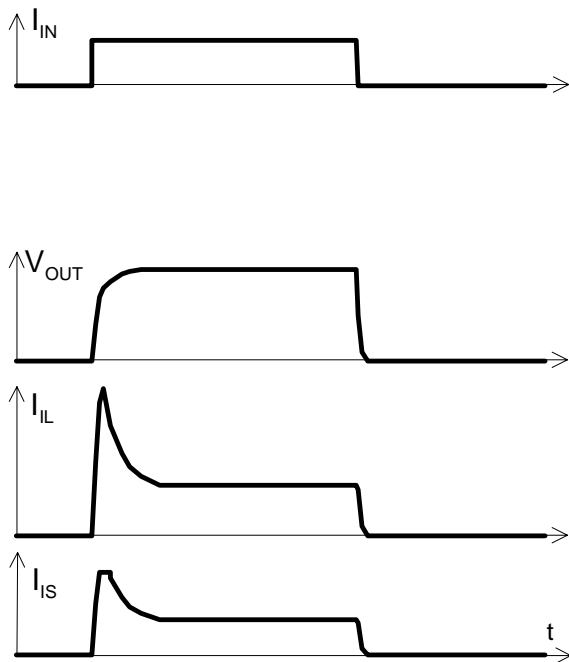
### Timing diagrams

**Figure 1a:** Switching a resistive load, change of load current in on-condition:



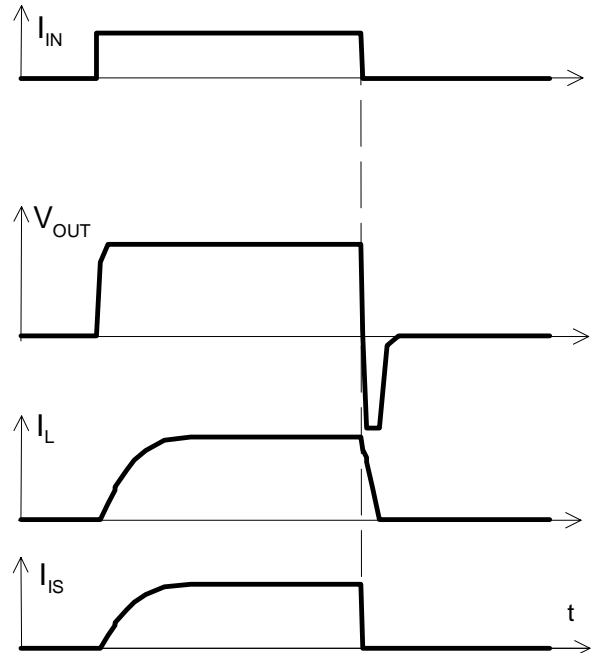
The sense signal is not valid during a settling time after turn-on/off and after change of load current.

**Figure 2a:** Switching motors and lamps:



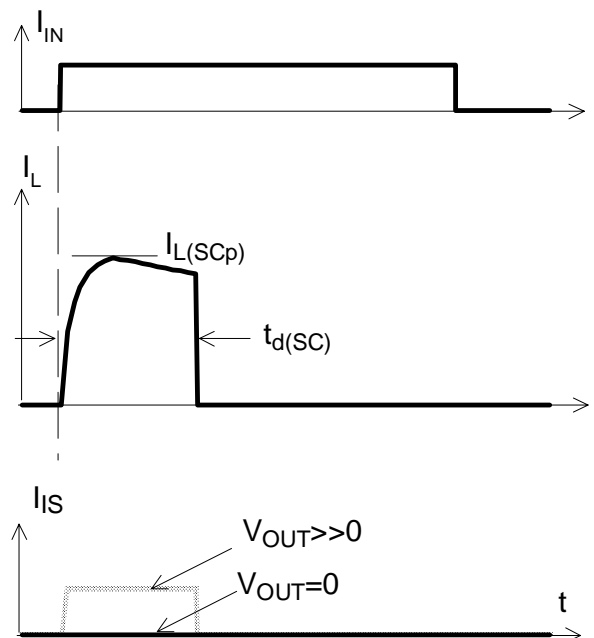
Sense current saturation can occur at very high inrush currents (see  $I_{IS,lim}$  on page 6).

**Figure 2b:** Switching an inductive load:



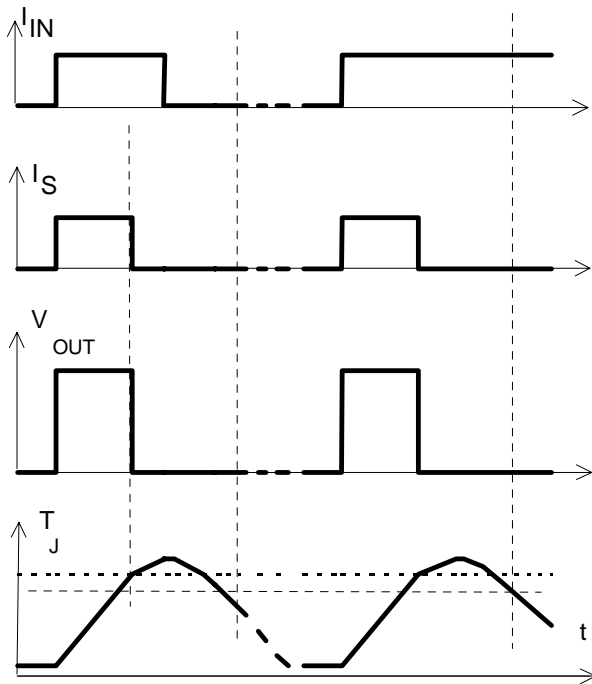
**Figure 3a:** Short circuit:

shut down by short circuit detection, reset by  $I_{IN} = 0$ .

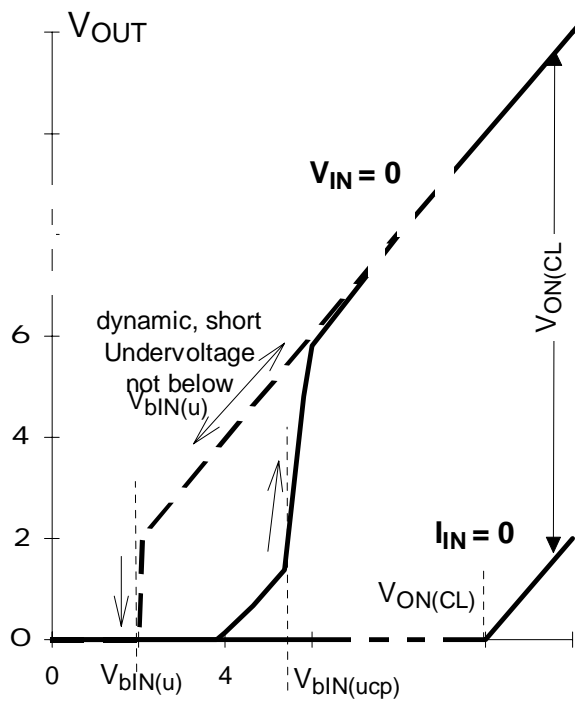


Shut down remains latched until next reset via input.

**Figure 4a:** Overtemperature, Reset if ( $I_{IN}$ =low) and ( $T_j < T_{jt}$ )



**Figure 6a:** Undervoltage restart of charge pump, overvoltage clamp



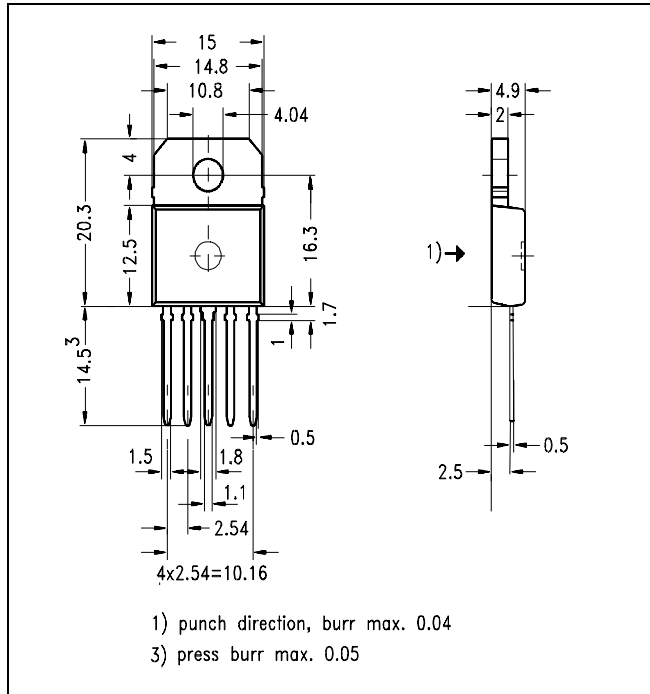
### Package and Ordering Code

All dimensions in mm

**TO-218AB/5 Option E3146** Ordering code

BTS555 E3146

Q67060-S6953A3



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