

GR581 DATA SHEET

FEATURES

- unity gain 12 dB/oct. highpass Butterworth filter
- adaptive frequency range from 200 Hz to 2 kHz
- rectifier threshold set to 82 dBSPL (adjustable)
- low noise, typically 2.6 μV
- 300 µA typical current drain
- operates from 1.1 to 3 VDC
- preamplifier with 56 dB open loop gain

PACKAGING

- 10 pin MICROpac
- 10 pin PLID[®]
- Chip (73 x 59 mils)

DESCRIPTION

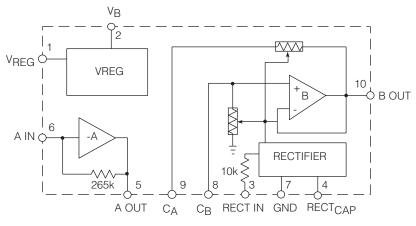
The GR581 is a level-sensitive, adaptive highpass filter comprised of a current controlled highpass filter, a half- wave rectifier, a voltage regulator for microphone bias and a separate preamplifier.

The internal rectifier senses the long term average signal level and controls the filter response by setting the control current of the filter. The rectifier sensitivity, with respect to the input signal, can be increased by placing the internal preamplifier (A) before the filter section of the GR581. The preamplifier has an internal 265 k Ω feedback resistor from its input to output, to facilitate in setting the gain.

An increase of 20 dB above the rectifier threshold will automatically increase the corner frequency one decade above the initial corner frequency. The filter will only allow an increase in corner frequency of one decade, regardless of further increases in the input signal level.

It is recommended that the attack and release times be set to 30 ms and 90 ms respectively. The average time period of a speech frame is about 15 ms which is not long enough to activate the filter, however long term average noise, which can have time periods greater than 30 ms, will activate the filter (providing that the amplitude is above the rectifier threshold).

The GR581 is an improved version of the LS581adaptive high pass filter and has an identical pinout.



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All resistors in ohms, all capacitors in farads unless otherwise stated.

FUNCTIONAL BLOCK DIAGRAM

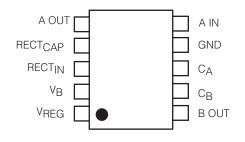
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ABSOLUTE MAXIMUM RATINGS

PARAMETER	VALUE			
Supply Voltage	3 VDC			
Power Dissipation	25 mW			
Operating Temperature Range	-10°C to 40°C			
Storage Temperature Range	-20°C to 70°C			
CAUTION CLASS 1 ESD SENSITIVITY	6			

PIN CONNECTIONS



ELECTRICAL CHARACTERISTICS Conditions: Supply Voltage V_{CC} = 1.3 V, Temperature 25°C

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
Total Current	IT			165	300	450	μA
Voltage Regulator (Pin 1)	V _{REG}			0.87	0.93	0.99	V _{DC}
Input Referred Noise	IRN	NFB 0.2 - 10kHz	Filter f _C set to 0.2kHz	-	2.6	-	μVRMS
		at 12dB/oct	Filter f _c set to 2kHz	-	5.6	-	
Attack Time	t _{ATT}		1	-	30	-	ms
Release Time	t _{REL}			-	90	-	ms
STAGE A							
Quiescent Voltage on pin 5	V _{Q5}			0.49	-	0.67	V _{DC}
Open Loop Gain	A _{OL}			45	56	-	dB
Feedback Resistor	R _F			175	265	355	kΩ
Current Sourcing Capacity	ISOURCE			15	30	-	μA
Current Sinking Capacity	I _{SINK}			15	30	-	μA
FILTER SECTION	•	•				1	•
Quiescent Voltage on pin 3	V _{Q3}			0.49	0.58	0.67	V _{DC}
Quiescent Voltage on pin 4	V _{Q4}			0.49	0.58	0.67	V _{DC}
Quiescent Voltage on pin 8	V _{Q8}			0.55	-	0.78	V _{DC}
Quiescent Voltage on pin 9	V _{Q9}			0.55	-	0.78	V _{DC}
Filter Insertion Loss	FIL	V _{OUT} = 850mVRM	-0.5	0.1	1.3	dB	
Distortion	THD	V _{OUT} = 850mV _{RMS} f=1kHz (S1 closed)		-	2	3	%
Rectifier Gain		V _{AC 2} = 2.5n	nVRMS (S2 closed)	5	7	9	
	A _{REC}	f = 100Hz (Note 1)					
Rectifier Bandwidth	B _R	$V_{AC2} = 20m$	-	4	-	kHz	
Pin 9 Nominal Current	I _{P9}	VP9 = 0V		0.70	1.00	1.30	μA
Current Range	I _{RANGE}	(Note 2, 3)		8	10	12	
Slope		(Note 2, 4)		0.75	1	1.25	
Rectifier Threshold	V _{TH}	f = 100H	1.7	2.5	2.8	mV _{DC}	
Corner Frequency	f _c	(No	140	200	260	Hz	

All Conditions and Parameters remain as show in Test Circuit unless otherwise specified in CONDITIONS Column.

WWW VQX- guiescent (unbias) voltage measured on the pin, (nothing connected to the pin). VPX - actual voltage measured on the pin at given condition (X is pin number).

NOTES:

1. $A_{REC} = 1.9375 \times (V_{P4} / V_{P3}) [V_{IN} = 10mV_{RMS}] - 0.9375 \times (V_{P4} / V_{P3}) [V_{IN} = 18mV_{RMS}]$ **2.** $I_{D0} = I_{P9} [V_{P9} = 0];$ $= I_{PQ} [V_{P4} = V_{Q4} + 35mV; V_{PQ} =$

$$I_{P9} [V_{P9} = 0];$$
 $I_{D1} = I_{P9} [V_{P4} = V_{Q4} + 35mV; V_{P9} = 0]$

$$I_{D2} = I_{P9} [V_{P4} = V_{Q4} + 85mV; V_{P9} = 0];$$
 $I_{D3} = I_{P9} [V_{P4} = V_{Q4} + 180mV; V_{P9} = 0]$

- **3.** $I_{RANGE} = I_{D3} / I_{D0}$
- 4. SLOPE = ((I_{D2} I_{D1}) / 50mV) x 14k Ω
- $\textbf{5.} \quad \text{V}_{AL} = 85 \text{mV} ((\text{I}_{D2} \text{I}_{D0}) \ / \ \text{SLOPE}) \ \times \ 14 \text{k} \Omega; \quad \text{V}_{AH} = 85 \text{mV} + (\ 50 \text{mV} \ \times (\ \text{I}_{D3} \text{I}_{D2} \) \ / \ (\ \text{I}_{D2} \text{I}_{D1} \));$ $V_{P4} \leq V_{AL} \left[V_{IN} = 1.7 m V_{RMS} \right]$ and $V_{P4} \geq V_{AL} \left[V_{IN} = 2.8 m V_{RMS} \right]$

6. $f_{c} = 1 / (2 \times \pi \times 1.41 \times 10 \text{ F x R});$ $R = 26 \text{ mV } \times ((1 / I_{D0}) + (1 / (12 - I_{D0})))$

 $I2 = ((3 \times (I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (4 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV]) / (I_{D0} + I_{P9}[V_{P9} = V_{Q9} - 18mV])) / (4 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV]) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV]))) / (1 - ((I_{D0} + I_{P9}[V_{P9} = V_{Q9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV]))) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV]))) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV])) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV]))) / (1 - ((I_{D0} + I_{P9}[V_{P9} + 18mV]))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV)))) / (1 - ((I_{D0} + 18mV))) / (1 -$

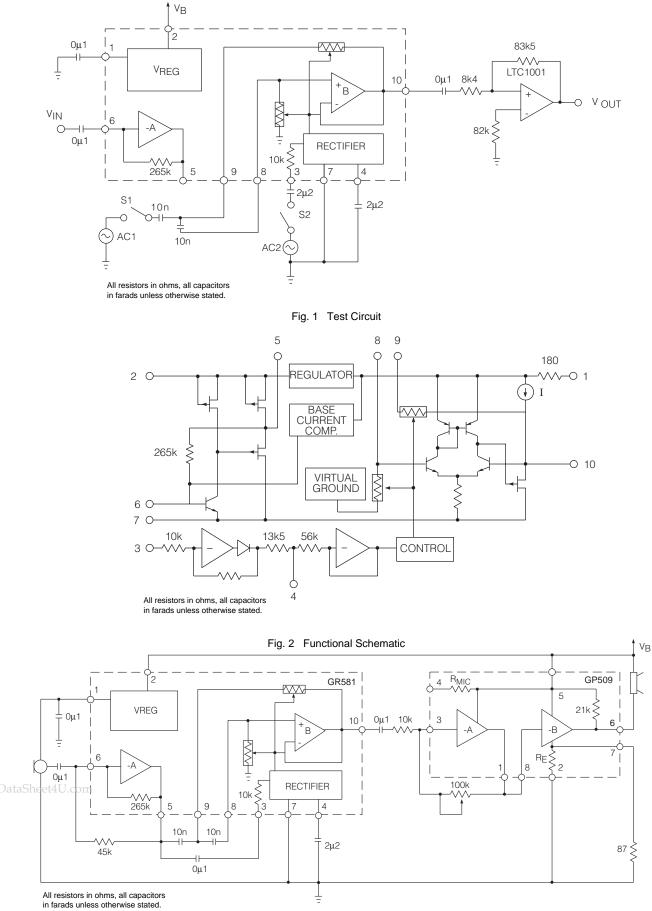


Fig. 3 Typical Hearing Instrument Application

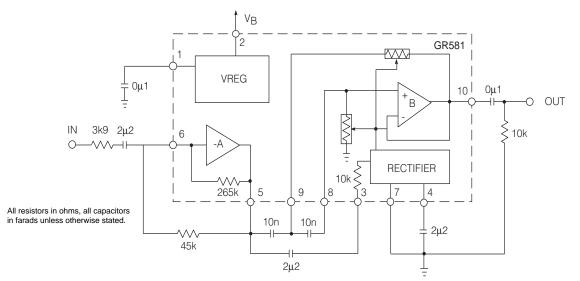
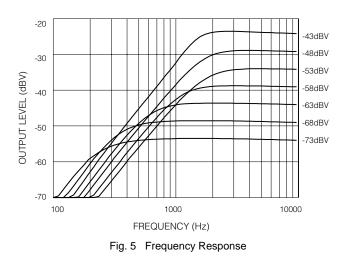


Fig. 4 Characterisation Circuit (used to generate typical curves)



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REVISION NOTES

Changes to standard