## Features

- 10V~36V Input Voltage Range
- Fixed 5.1V Output Voltage
- Programmable Operation Frequency from 50KHz~300KHz
- Dual Channel Accurate OCP
- ±1.5% Voltage Reference Accuracy
- COT Control with Internal ripple injection
- Programmable Protection Auto-restart Time
- Build-in Wire Drop Compensation
- Selectable CCM/DEM Operation
- Output Short-Circuit Protection
- Output Over-Voltage Protection
- Output Under-Voltage Protection
- Over Temperature Protection
- TQFN20-5x5 Package
- Green Product (RoHS, Lead-Free, Halogen-Free Compliant)

## Applications

- Car Charger
- Portable Charger Devices
- Automotive Power Application
- General-Purposed DC-DC Converters

## **General Description**

The GS92D3 is a synchronous Buck converter. Features include wide input voltage range, dual channel accurate OCP, build-in wire drop compensation and auto-restart after protections.

The GS92D3 has fast dynamic transient response with COT control scheme and also has good line and load regulation with internal ripple injection.

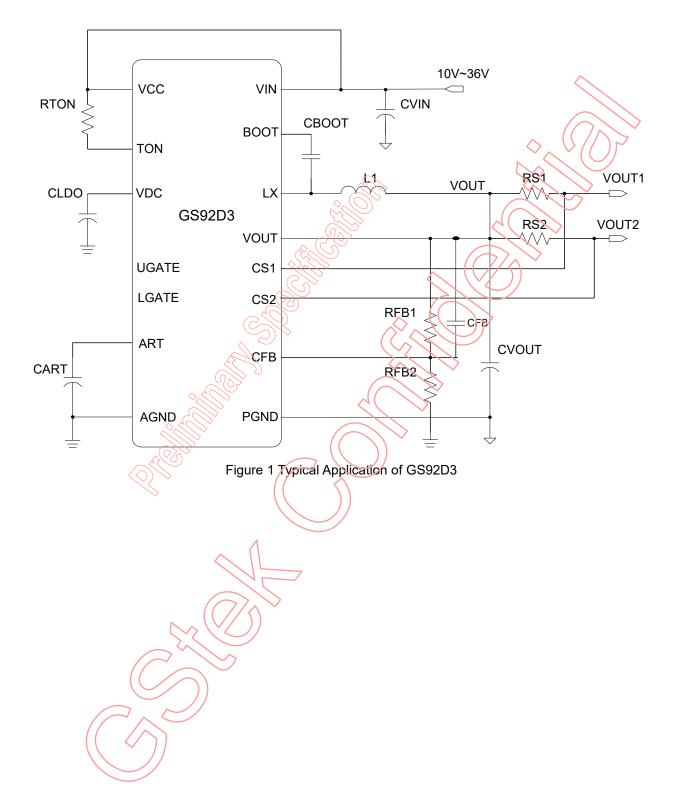
The GS92D3 provide dual channel accurate OCP. When OCP is detected in channel, the output is disabled until ART timing is over, and then the chip will restart automatically, which make sure the safety of whele system. Wire drop compensation is also provided to compensate the voltage loss in cable transmission.

Other protections include over-voltage protection, under-voltage protection, short-circuit protection and over-temperature protection.

The GS92D3 is available in TQFN20-5x5 package.

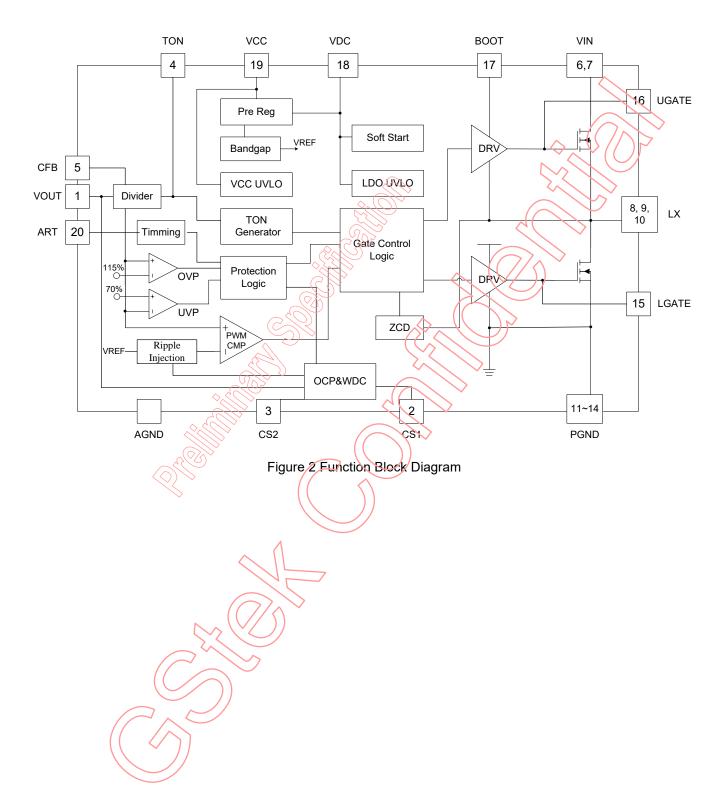
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# **Typical Application**

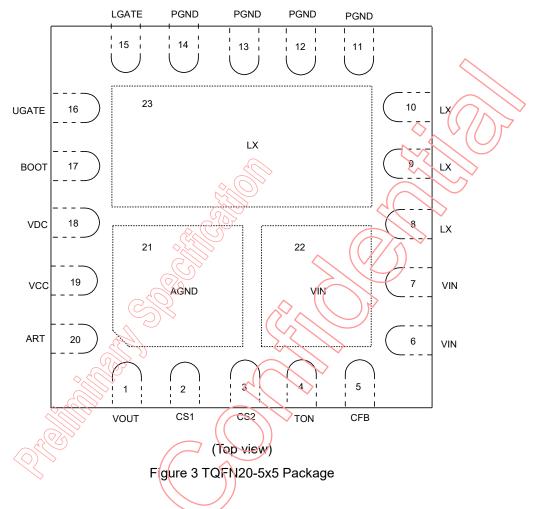


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# **Function Block Diagram**



# **Pin Configuration**



# **Pin Descriptions**

Pin Dese	criptions	5	Λ
No.	Name	I/O	Description
1	VOUT	I	Output voltage feedback pin. Connect to output capacitor.
2	CS1		Channel 1 current sense.
3	CS2		Charinel 2 current sense.
4	TON	$\sum$	On time setting. Connect a resistor to VCC.
5	CFB	$\langle \rangle \rangle$	Feedback Pin.
6,7,22	VIN		Power Supply pin for internal MOSFET
8~10,23	LX		Upper driver floating ground and used to sense the current of inductor.
11~14	PGND	Ι	Power ground for Internal MOSFET
15	LGATE	0	Low-side power MOS gate drive output.
16	UGATE	0	High-side power MOS gate driver output.

17 BOOT		BOOT I/O	Power supply for high-side driver.		
17	BOOT	1/0	Connect a 0.1uF capacitor between BOOT and LX.		
18	VDC	I/O	Internal Output regulator, Connect a capacitor to AGND		
19	VCC	I	Power Supply pin for internal Circuits.		
20	ART	I	Setting auto-restart time. Connect a capacitor to AGND		
21	AGND	I	Power Ground pin for internal Circuits.		

# Ordering Information GS92D3<u>PP-R</u>

1. Package	-	→ 2. Shipping	1

		A P	
No	ltem		Contents
1	Package	TQ: TQFN20-5x5	
2	Shipping	R: Tape & Reet	

Example: GS92D3 TQFN20-5x5 Tape & Reel ordering information is "GS92D3TQ-R"

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## Absolute Maximum Rating (Note 1)

Parameter	Symbol	Limits	Units
VCC to GND	$V_{CC,} V_{IN}$	-0.3 ~ 40	V
TON to GND	V <sub>TON</sub>	-0.3 ~ 40	V
CSX to GND	V <sub>CSX</sub>	-0.3 ~ 6	V
VDC to GND	V <sub>DC</sub>	-0.3 ~ 6	V
ART to GND	V <sub>ART</sub>	-0.3~6	V
VOUT/VFB to GND	VOUT VCFB	-0.3~6	V
BOOT Voltage	VBOOT-GND	-0.3~46	V
BOOT to LX Voltage	VBOOT-LX	-0,3 ~ 6	V
LG to GND	V <sub>LG</sub>	-0.3~6	V
LX to GND	V <sub>LX</sub>	- 0.7V~40V (DC) -8V~40V(<200nS)	V
Package Power Dissipation at $T_A \leq 25$ °C	PD_TQFN205x5	4228	mW
Junction Temperature	T	- 45 ~ 150	°C
Storage Temperature	T <sub>STG</sub>	- 55 ~ 150	°C
Lead Temperature (Soldering) 10S	TIEAD	260	°C
ESD (Human Body Mode) (Note 2)		2K	V
ESD (Machine Mode) (Note 2)		200	V
Thermal Information (Note 3)			

# Thermal Information (Note 3)

Parameter	Symbol	Limits	Units
Thermal Resistance Junction to Amplent	$\theta_{JA_TQFN20-5x5}$	23.65	°C/W

# Recommend Operating Condition (Note 4)

Symbol	Limits	Units
$V_{CC},V_{IN}$	10~36	V
$V_{\text{DC}}$	4.5~5.5	V
TJ	-40 ~125	°C
T <sub>A</sub>	-40 ~ 85	°C
	V <sub>CC</sub> V <sub>IN</sub> V <sub>DC</sub> T <sub>J</sub>	V <sub>CC</sub> ·V <sub>IN</sub> 10~36   V <sub>DC</sub> 4.5~5.5   T <sub>J</sub> -40 ~125

## **Electrical Characteristics**

( $R_{TON}$ =1000KOhm,  $V_{CC}$ = $V_{IN}$ =12V,  $T_A$  =25°C, unless otherwise specified)

Parameter	Symbol	Conditions	Min	Тур	Мах	Units		
Supply Voltage (Vcc)								
Under voltage lock out (Rising)	V <sub>CC_UVLO</sub>			9		>		
UVLO Hysteresis	$V_{CC\_UVLOHYS}$			0.7	(//)	V V		
5V Pre-regulator (VDC)				$\sim$		/		
Output Voltage	$V_{DC}$			5.15	$\sum$	V		
Under voltage lock out (Rising)	V <sub>VDC_UVLO</sub>		<	4.3		V		
UVLO Hysteresis	$V_{\text{VDC}\_\text{UVLOHYS}}$			0.3		V		
Vout Section				ノ				
Vout Reference Voltage	V <sub>OUT_R</sub>		5	5.1		V		
Vout Operation Current	IOUT_OR			70		uA		
Vout Discharge Current	LOUT DIS			10		mA		
Accurate OCP(CS1/CS2)								
OCP Threshold	VOCP			108		mV		
OCP Delay	Тоср			5		us		
Current Parameters(V <sub>cc</sub> )								
Quiescent Current	Ι <sub>Q</sub>	V <sub>OUT</sub> =5.5V, VIN=12V		760		uA		
System Time	Δ							
On-Time	TON	V <sub>IN</sub> =V <sub>CC</sub> =12V,V <sub>OUT</sub> =4.8V		3.9		us		
TON Current	ITON-ON	V <sub>IN</sub> =V <sub>CC</sub> =12V		11.3		uA		
Minimum Off-Time		$V_{IN}=V_{CC}=12V, V_{OUT}=4.8V$		450		ns		
Softstart Time								
Internal Softstart Time	T <sub>SS</sub>			2.6		ms		
Auto Restart Section	<u></u>							
Auto-restart Threshold Voltage	V <sub>ART</sub>			2		V		
ART charging Current	I <sub>ART_CHG</sub>			2		uA		
ART discharging Current	I <sub>ART_DIS</sub>	V <sub>ART</sub> =1.8V		1.5		mA		
Driver Section								
High Side MOS RDSON	R <sub>DSH</sub>	BOOT-LX=5V		13		mohms		

High Side Leakage	I <sub>LEAKH</sub>			10		uA	
Low Side MOS RDSON	R <sub>DSL</sub>	VDC-GND=5V		6		mohms	
Low Side Leakage	I <sub>LEAKL</sub>			10		uA	
Dead Time	T <sub>DH</sub>			44	$\wedge$	ns	
Dead Time	$T_DL$			34		ns	
LX Current Sensing						$\langle \rangle$	
Current Limit Threshold	V <sub>CL</sub>	GND-LX		108	$\lor(O)$	mV	
Zero Crossing Threshold	V <sub>ZCD</sub>	GND-LX	-10	$\sum$	10	mV	
Voltage Fault Protection		S.O.		$\sim$	$\mathcal{S}$		
UV Threshold	$V_{\text{UV}\_\text{TH}}$		<	70		%	
UV Fault Delay	T <sub>UV_D</sub>		$(\mathcal{O})$	20		us	
OVP Threshold	V <sub>OV_TH</sub>			115		%	
OVP Delay	T <sub>ov_p</sub>		)r	20		us	
Over Temperature Shutd	own						
Thermal Shutdown			>	150		°C	
Threshold	TTSPN			150		C	
Thermal Shutdown	T <sub>HYS_TSDN</sub>			20		°C	
Hysteresis	THYS_ISDN			20		0	
Bootstrap Diode		$\bigcirc$					
Internal Boost Charging	R <sub>bt_d</sub>	VCC to BOOT, 10mA		80	110	ohms	
Switch On-Resistance	U_18			00	110	onnio	
Wire Drop Compensation							
Wire Drop Compensation	R <sub>WDC</sub>	V <sub>ART</sub> =1V		200		mv	
Rate	$\square \bigcirc \land$	(VOUT-VCS=100mV)		200			
Short Protection When Start Up							
Short Protection Delay	TSP	V <sub>OUT</sub> =0.4V		1		ms	
Time		001 000		-			

Note 1. Stresses listed as the above "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.

**Note 2.**Devices are ESD sensitive. Handling precaution recommended.

**Note 3.** $\theta_{JA}$  is measured in the natural convection at  $T_A=25^{\circ}C$  on a high effective thermal conductivity test board (4 Layers, 2S2P) of JEDEC 51-7 thermal measurement standard.

**Note 4.** The device is not guaranteed to function outside its operating conditions.

**Note 5** Recommend the Pulse time<100ns when VIN over than 40V.

Note 6 If V(BOOT)-V(LX)<4V, a boot diode is recommended.

## **Application Information**

The GS92D3 is a synchronous Buck Converter with COT control scheme. Features include wide input voltage range, dual channel accurate OCP, wire drop compensation and programmable timing of auto-restart after protections.

#### System Clock Generator and PWM Control

The on-time of GS92D3 can be set by an external setting resistor from VCC to TON, thus the GS92D3 based Buck converter has a relative constant operation frequency over wide input voltage range. At the beginning of each switching cycle, upper power MOSFET is turned on, after typical fixed on-time, the upper MOSFET is turned off, and then lower power MOSFET is turned on after internal dead time. The upper MOSFET will not be turned on at the beginning of next cycle until output voltage falls down below the preset voltage.

To avoid the surge inductor current during large load transient, a minimum Off-time is added. Typical minimum off-time is around 450ns.

#### High Side Switch On-Time Count

The on-time is decided by the external setting resistor, and the input voltage. Looking at the TON pin, the input voltage is converted to current which is inversely proportional to itself by dividing the external setting resistor. The TON current is used to charge an internal capacitor and when the voltage of the capacitor reaches the internal voltage which is proportional to output voltage on-time one-shot pulse is generated, and then upper power MOSFET is turned off and lower power MOSFET is turned on. We can count the on-time and switching frequency according to the equations below:

 $T_{ON} = (V_{OUT} \times R_{TON} \times 8.93p) / (V_{IN} - 0.8)$ 

Then, the switching frequency is:

 $F_{sw}=V_{OUT}/(V_{IN} \times T_{ON})$ 

R<sub>TON</sub> is a resistor connected from input voltage (VCC)

Green Solution Technology Co., LTD. Rev.:0.0(*Preliminary Specification*) to TON pin.

For heavy load application, due to ground bounced and the high impedance of  $R_{TON}$ , the TON pin should always be bypassed to AGND using a several nF-order ceramic capacitor for reliable system operation.

#### DEM

When the load turns light, the GS92D3 maintains the on-time and extend the off-time, which decrease the system clock frequency to skip PWM pulses for better efficiency. The GS92D3 zero crossing detector will sense the inductor current from LX pin and judge its value by comparing the LX pin voltage to ground. Once the LX node voltage is equal to the PGND node voltage, the converter will turn off the low side power MOSFET and enter DEM. As the load current decrease, it takes longer time to discharge the output capacitor to the level that required to start the next switching cycle. The on-time is kept the same as in the heavy-load operation.

#### Accurate Over Current Protection

The accurate OCP is implemented by the CS1 and CS2 pins. OCP is triggered and shuts down UG and LG if (VOUT-VCS1) or (VOUT-VCS2) is higher than 108mv (Typical), thus the OCP threshold can be set by the following equation:

#### $I_{OCP}$ =108mv/R<sub>S</sub>

 $\mathsf{R}_\mathsf{S}$  is the sense resistor connected between VOUT pin and CS pin. The OCP has 5us de-bounce time.

When OCP is triggered, the GS92D3 will enter a auto-restart procedure: delay a time period and rebuild the output from soft start. The delay time can be set by ART pin.

#### Auto-restart Setting

The GS92D3 will auto-restart when protections occurred. Before restart, a delay time period can be set by connecting a capacitor from ART pin to AGND pin. A current will charge the capacitor from ground level to a

preset level. The delay time is calculated by the following equation:

#### $T_{ART}$ =1E6\* $C_{ART}$

#### Wire Drop Compensation

The GS92D3 will compensate the cable voltage drop due to the output current. The output current is sensed by CS1 pin and CS2 pin as mentioned before. The GS92D3 will choose the larger output current to compensate if the current of two channels are different.

#### **Current Limit**

The GS92D3 uses the on-state resistance of the low-side power MOSFET as a current-sense resistor to sense the inductor current. In this case, the GS92D3 build in a cycle-by-cycle current limit. The current limit circuit regulates the inductor valley current that means if the valley value of the inductor current exceeded a preset level the PWM is not allowed to initiate a new switching cycle.

During soft-start, the GS92D3 will linearly release the current limit according to the internal soft-start ramp. The current limit will be fully released about 1ms after soft start begun.

#### **Output Over-Voltage Protection**

When the VOUT voltage rises up to 115% of the normal operating voltage, the internal fault-logic module delays about 20us and turns on the low-side Power MOSFET. The state is maintained until the ART timing is over, and the GS92D3 will restart.

#### Output Under-Voltage Protection

When the VOUT voltage falls down to 70% of the normal operating voltage, the internal fault-logic module will delay about 20us and turns on the low-side Power MOSFETs. The state is maintained until the ART timing is over, and the GS92D3 will restart. UVP is disabled during soft start.

#### VDC and VCC UVLO

An internal under voltage lockout (UVLO) module is

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used to sense the VDC power supply. The PWM converter is forbidden by the under voltage lockout module. When VDC rises above 4.3V, the GS92D3 will initial the control logic circuitries and soft-start ramping generator, and then allows switching to occur. When VDC falls below 4.0V, the PWM converter is forbidden. When VCC rises above 9V, the LDO output voltage (VDC) of GS92D3 enables and regulates a 5.15V voltage. After VCC falls below 8.3V the LDO (VDC) will turn off.

#### Short Circuit Protection

During soft start, if short circuit occurs, the output current will increase rapidly to current limit and the state maintained until soft start finished, which makes the external components endure a big stress. The GS92D3 offers rapid protections when short circuit occurred during soft start.

#### VOUT Rin

The VOUT pin offers feedback information of output voltage, which makes the Ton more accurate, so the switching frequency variation is very small even when the GS92D3 operates in a very wide input voltage range. When any fault condition occurs, the VOUT pin provides a discharge path from output to ground.

#### **Choose Inductor**

Set the ripple current approximately 1/4 to 1/2 of the maximum output current. 1/3 is recommended.

$$L_{IND} = \frac{1}{I_{IND(ripple)} \times f} \times \frac{(V_{IN(max)} - V_{OUT}) \times V_{OUT}}{V_{IN(max)}}$$
$$L_{IND} = \frac{3}{I_{IOUT(max)} \times f} \times \frac{(V_{IN(max)} - V_{OUT}) \times V_{OUT}}{V_{IN(max)}}$$

For applications that require fast transient response with minimum VOUT overshoot, consider a smaller inductance than above. The cost of a small inductance value is higher steady state ripple, larger line regulation, and higher switching loss.

The inductor also needs to have low DCR to achieve good efficiency, as well as enough room above peak

inductor current before saturation. The peak inductor current can be estimate as follows.

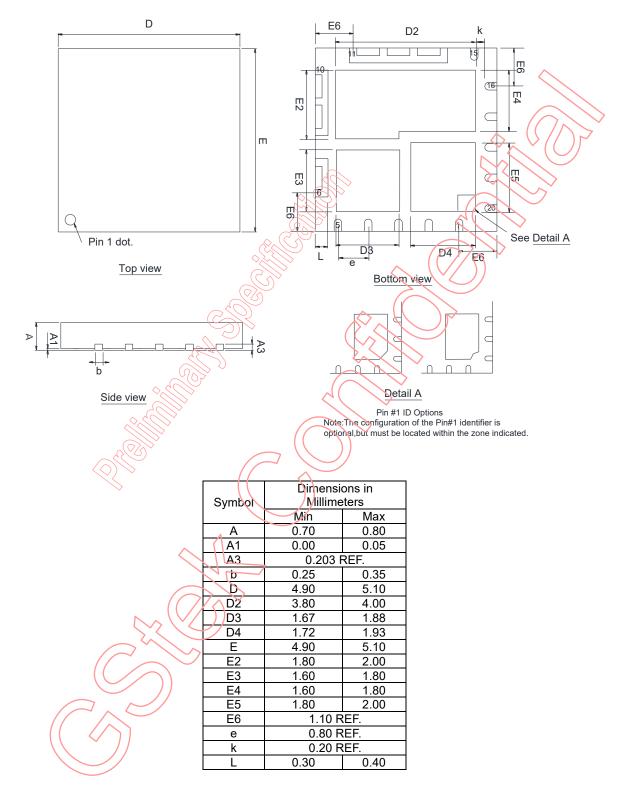
 $L_{IND(peak)} = \frac{1}{L \times f} \times \frac{(V_{IN(\max)} - V_{OUT}) \times V_{OUT}}{V_{IN(\max)}} + \frac{V_{CL}}{R_{DS(on)}}$ 

#### **Choose Output Capacitors**

$$RESR = \frac{1}{I_{ripple}} \times 0.038$$
$$\approx \frac{3}{I_{OUT(max)}} \times 0.038$$
$$RESR \approx \frac{V_{OUT}}{I_{OUT(max)}} \times 114(mohm)$$

Organic semiconductor capacitors or specialty polymer capacitors are recommended.

## Package Dimensions, TQFN20-5x5



#### Note

- 1. Min.: Minimum dimension specified.
- 2. Max.: Maximum dimension specified.
- 3. REF.: Reference. Normal/Regular dimension specified for referenc

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