

NOT RECOMMENDED FOR NEW DESIGNS
PLEASE REFER TO ISL59837
FOR A PIN COMPATIBLE UPGRADE

ISL59830A

True Single Supply Video Driver With Power Down

FN6233 Rev.3.00 Sep 26, 2006

The ISL59830A is a revolutionary device that allows true single-supply operation of video amplifiers. The device runs off a single 3.3V supply and generates the required negative voltage internally. This allows for DC-accurate coupling of video onto a 75Ω double-terminated line. Since the buffers have an integrated 6dB gain, the only external components required are the 75Ω termination resistors and a small capacitor. An input reference voltage can be supplied to shift the analog video level down by an amount equal to the reference (typically 0.6V).

Ordering Information

PART NUMBER	PART MARKING	TAPE & REEL	PACKAGE	PKG. DWG.#
ISL59830AIAZ (See Note)	59830AIAZ	-	16 Ld QSOP (Pb-free)	M16.15A
ISL59830AIAZ-T7 (See Note)	59830AIAZ	13"	16 Ld QSOP (Pb-free)	M16.15A

NOTE: Intersil Pb-free plus anneal products employ special Pb-free material sets; molding compounds/die attach materials and 100% matte tin plate termination finish, which are RoHS compliant and compatible with both SnPb and Pb-free soldering operations. Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.

Features

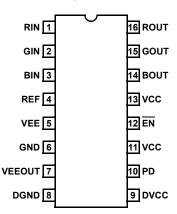
- · Triple single-supply buffer
- · Operates from single +3.3V supply
- · No output DC blocking capacitor needed
- · Fixed gain of 2 output buffer
- · Output three-statable
- · Enable/disable function
- · Charge pump power down function
- · 50MHz 0.1dB bandwidth
- · 200MHz -3dB bandwidth
- · Pb-free plus anneal available (RoHS compliant)

Applications

· Driving video

Pinout

ISL59830A (16 LD QSOP) TOP VIEW



Absolute Maximum Ratings (T_A = +25°C)

V _{CC} , Supply Voltage between V _S and GND5V	Operating Temperature
V _{IN} , V _{REF}	Maximum Die Temperature
Voltage between V _{IN} and V _{REF} ±2V	Storage Temperature65°C to +150°C
Maximum Continuous Output Current	Lead Temperature
	Power Dissipation See Curves

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore: $T_J = T_C = T_A$

AC Electrical Specifications V_{CC} = DV $_{CC}$ = +3.3V, REF = GND, T_A = +25°C, R_L = 150 Ω , unless otherwise specified.

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
BW -3dB	3dB Bandwidth	V _{OUT} = 200mV _{PP}		200		MHz
		V _{OUT} = 2V _{PP}		100		MHz
BW 0.1dB	0.1dB Bandwidth	V _{OUT} = 2V _{PP}		50		MHz
S _R	Slew Rate	V _{OUT} = 2V _{PP}	500			V/µs
d _G	Differential Gain			.06		%
d _P	Differential Phase			0.1		۰
X _T	Hostile Crosstalk	6MHz		-90		dB
I	Input to Output Isolation	6MHz		-70		dB
V _N	Input Noise Voltage			20		nV/√Hz
CSW Freq	Charge Pump Switch Frequency			168		MHz
Load Reg		I _{EE} = 0mA to 10mA		12	60	mV
V _{RIPPLE}	Ripple Voltage			30		mV

DC Electrical Specifications $V_{CC} = D_{VCC} = +3.3V$, REF = GND, $T_A = +25^{\circ}C$, $R_L = 150\Omega$, unless otherwise specified.

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
V+	Supply Range		3.0		3.6	V
V _G %	Gain Error	$R_L = 150\Omega$, $V_{IN} = +2.5V$ to -1V			1.5	%
GM	Gain Matching	$R_L = 150\Omega$		0.5		%
R _{IN}	Input Resistance	V _{IN} = 0V to 1.5V	1.0	1.7	15	МΩ
Vos	Output Offset Voltage	V _{REF} = 0	-25	7	+25	mV
I _{OUT +}	Output Current	$R_L = 10\Omega, V_{IN} = 1.2V$	50			mA
I _{OUT} -	Output Current	$R_L = 10\Omega, V_{IN} = -0.3V$			-18	mA
Z _{OUT}	Output Impedance	Enabled		1		Ω
		Three-stated		10		МΩ
PSRR	Power Supply Rejection Ratio		60	90		dB
IS	Supply Current	Enabled			150	mA
I _{S_PD}	Power Down Supply Current	EN = PD = 3.3V		0.9		mA
R _{REF}	Input Reference Resistor		4	5	6	kΩ



Pin Descriptions

PIN NUMBER	PIN NAME	PIN FUNCTION	EQUIVALENT CIRCUIT
1	RIN	Analog input	V _{CC} V _{CC} V _{CE} V _{EE} CIRCUIT 1
2	GIN	Analog input	Reference Circuit 1
3	BIN	Analog input	Reference Circuit 1
4	REF	Reference input	REF D Sout CIRCUIT 2
5	VEE	Chip substrate	D _{VCC} CHARGE PUMP D _{GND} CIRCUIT 3
6	GND	Analog ground	
7	VEE OUT	Charge pump output	Reference Circuit 3
8	DGND	Charge pump ground	Reference Circuit 3
9	DVCC	Charge pump supply voltage	Reference Circuit 3
10	PD	Charge pump enable	Reference Circuit 4
11, 13	VCC	Positive power supply	
12	ĒN	Chip enable	V _{CC} V _{CC} CIRCUIT 4

Pin Descriptions (Continued)

PIN NUMBER	PIN NAME	PIN FUNCTION	EQUIVALENT CIRCUIT
14	BOUT	Analog output	V _{CC} V _{EE} CIRCUIT 5
15	GOUT	Analog output	Reference Circuit 5
16	ROUT	Analog output	Reference Circuit 5

Typical Performance Curves

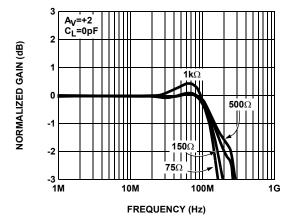


FIGURE 1. GAIN vs FREQUENCY FOR VARIOUS RLOAD

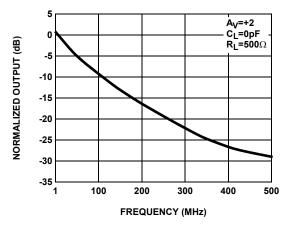


FIGURE 3. $V_{\mbox{\scriptsize REF}}$ PIN OUTPUT FREQUENCY RESPONSE

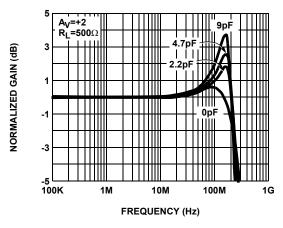


FIGURE 2. GAIN vs FREQUENCY FOR VARIOUS CLOAD

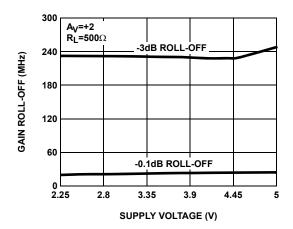


FIGURE 4. GAIN ROLL-OFF vs FREQUENCY

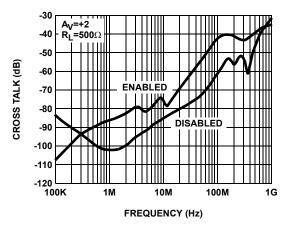


FIGURE 5. CROSS TALK CHANNEL TO CHANNEL (TYPICAL)

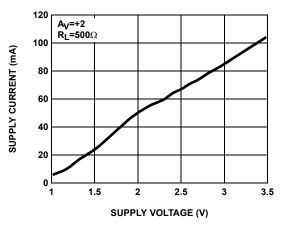


FIGURE 7. SUPPLY CURRENT vs SUPPLY VOLTAGE

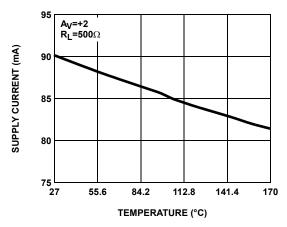


FIGURE 9. SUPPLY CURRENT vs TEMPERATURE

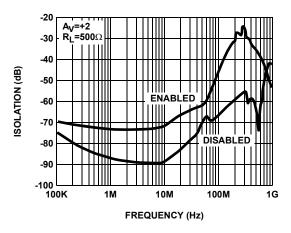


FIGURE 6. INPUT TO OUTPUT ISOLATION vs FREQUENCY

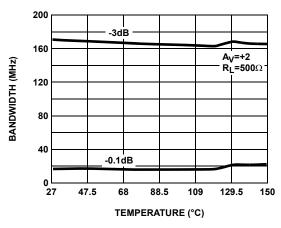


FIGURE 8. BANDWIDTH vs TEMPERATURE

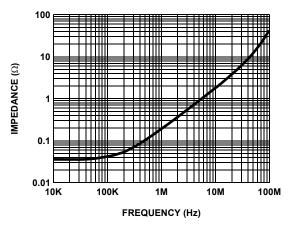


FIGURE 10. OUTPUT IMPEDANCE vs FREQUENCY

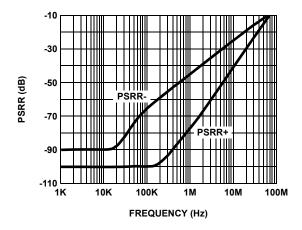


FIGURE 11. POWER SUPPLY REJECTION RATIO vs FREQUENCY

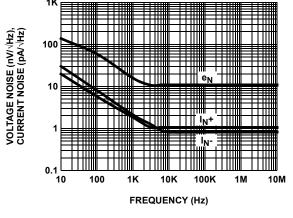


FIGURE 12. VOLTAGE AND CURRENT NOISE vs FREQUENCY

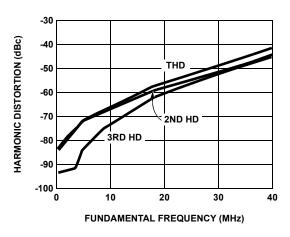
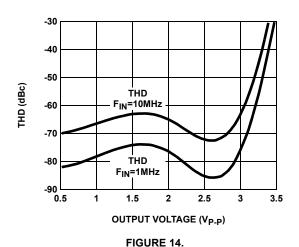


FIGURE 13. HARMONIC DISTORTION vs FREQUENCY



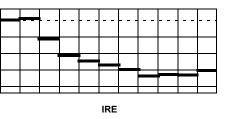


FIGURE 15. DIFFERENTIAL GAIN

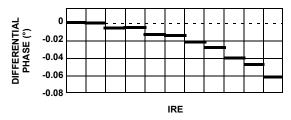


FIGURE 16. DIFFERENTIAL PHASE

DIFFERENTIAL GAIN (%)

-0.04

-0.06

-0.08

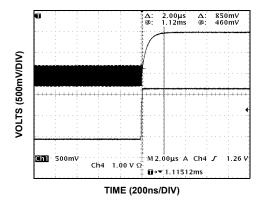


FIGURE 17. DISABLE TIME

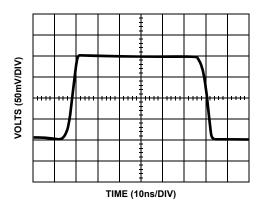


FIGURE 19. SMALL SIGNAL RISE & FALL TIME

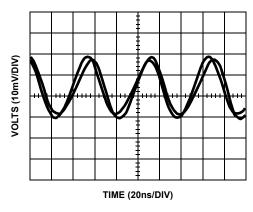


FIGURE 21. CHARGE PUMP OSCILLATION

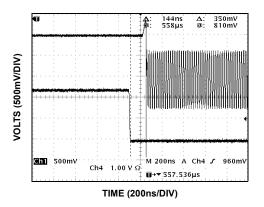


FIGURE 18. ENABLE TIME

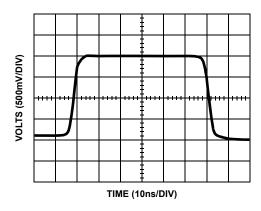


FIGURE 20. LARGE SIGNAL RISE & FALL TIMES

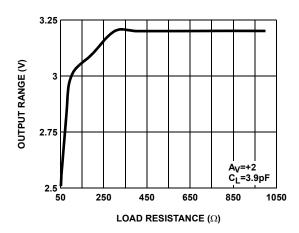


FIGURE 22. MAXIMUM OUTPUT MAGNITUDE vs LOAD RESISTANCE

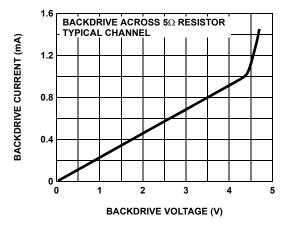


FIGURE 23. BACKDRIVE VOLTAGE vs CURRENT

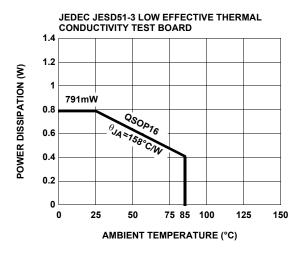


FIGURE 25. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

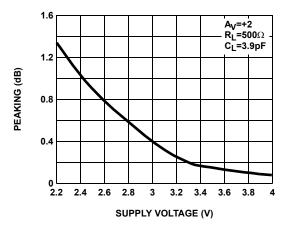


FIGURE 24. PEAKING vs SUPPLY VOLTAGE

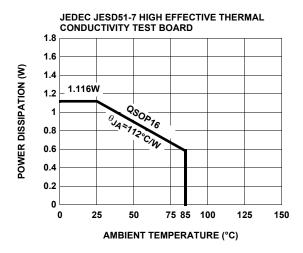
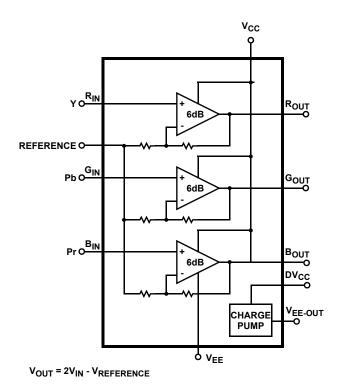
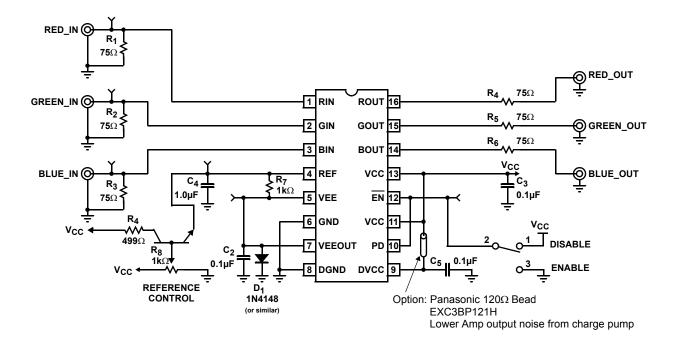


FIGURE 26. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

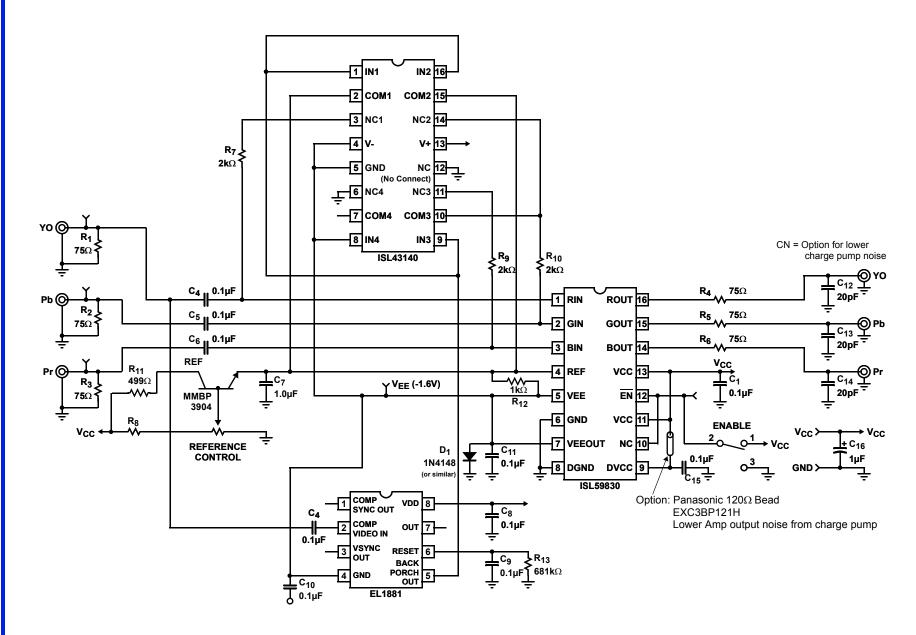
Block Diagram



Demo Board Schematic



ISL59830A + DC-Restore Solution



Description of Operation and Application Information

Theory Of Operation

The ISL59830A is a highly practical and robust marriage of three high bandwidth, high speed, low power, rail-to-rail voltage feedback amplifiers with a charge pump, to provide a negative rail without an additional power supply. Designed to operate with a single supply voltage range of from 0V to 3.3V, the ISL59830A eliminates the need for a split supply with the incorporation of a charge pump capable of generating a bottom rail as much as 1.6V below ground; for a 4.9V range on a single 3.3V supply. This performance is ideal for NTSC video with its negative-going sync pulses.

The Amplifier

The ISL59830A fabricated on a dielectrically isolated high speed 5V Bi-CMOS process with 4GHz PNPs and NPN transistor exceeding 20GHz - perfect for low distortion, low power demand and high frequency circuits. While the ISL59830A utilizes somewhat standard voltage mode feedback topologies, there are many non-standard analog features providing its outstanding bandwidth, rail-to-rail operation, and output drive capabilities. The input signal initially passes through a folded cascode, a topology providing enhanced frequency response essentially by fixing the base collector voltage at the junction of the input and gain stage. The collector of each input device looks directly into an emitter that is tied closely to ground through a resistor and biased with a very stable DC source. Since the voltage of this collector is "locked stable" the effective bandwidth limiting of the Miller capacitance is greatly reduced. The signal is then passed through a second fully-realized differential gain stage and finally through a proprietary common emitter output stage for improved rail-to-rail output performance. The result is a highlystable, low distortion, low power, and high frequency amplifier

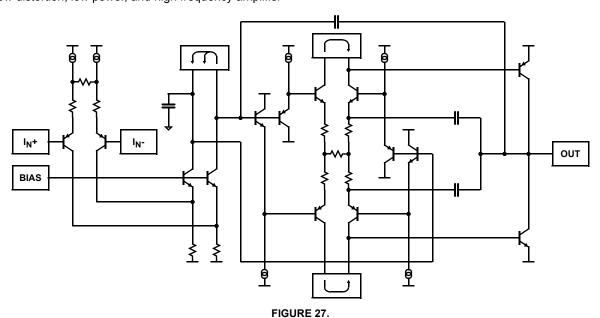
capable of driving moderately capacitive loads with near rail-torail performance.

Input Output Range

The three amplifier channels have an input common mode voltage range from 0.15V below the bottom rail to within 100mV of the positive supply, V_S+ pin (Note: bottom rail is established by the charge pump at negative one half the positive supply). As the input signal moves outside the specified range, the output signal will exhibit increasingly higher levels of harmonic distortion. And of course, as load resistance becomes lower, the current drive capability of the device will be challenged and its ability to drive close to each rail is reduced. For instance, with a load resistance of 1×100 the output swing is within 100×100 mV of the rails, while a load resistance of 1×100 limits the output swing to within around 1×100 mV of the rails.

Amplifier Output Impedance

To achieve near rail-to-rail performance, the output stage of the ISL59830A uses transistors in the common emitter configuration, typically producing higher output impedance than the standard emitter follower output stage. The exceptionally high open loop gain of the ISL59830A and local feedback reduces output impedance to less than 2Ω at low frequency. However, since output impedance of the device is exponentially modulated by the magnitude of the open loop gain, output impedance increases with frequency as the open loop gain decreases with frequency. This inductive-like effect of the output impedance is countered in the ISL59830A with proprietary output stage topology, keeping the output impedance low over a wide frequency range and making it possible to easily and effectively drive relatively heavy capacitive loads (See Figure 10).



The Charge Pump

The ISL59830A charge pump provides a bottom rail up to 1.65V below ground while operating on a 0V to 3.3V power supply. The charge pump is internally regulated to one-half the potential of the positive supply. This internal multi-phase charge pump is driven by a 160MHz differential ring oscillator driving a series of inverters and charge storage circuitry. Each series inverter charges and places parallel adjoining charge circuitry slightly out of phase with the immediately preceding block. The overall effect is sequential discharge and generation of a very low ripple of about 10mV that is applied to the amplifiers providing a negative rail of up to -1.65V.

There are two options to reduce the output supply noise.

- Add a 120Ω bead in series between V_{CC} and DV_{CC} to further reduce ripple.
- Add a 20pF capacitor between the back load 75Ω resistor and ground (see the ISL59830A + DC-Restore Solution schematic on page 10).

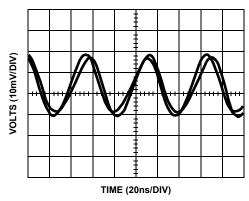


FIGURE 28. CHARGE PUMP OSCILLATION

The system operates at sufficiently high frequencies that any related charge pump noise is far beyond standard video bandwidth requirements. Still, appropriate bypassing discipline must be observed, and all pins related to either the power supply or the charge pump must be properly bypassed. See "Power Supply Bypassing and Printed Circuit Board Layout" in this section.

The V_{REF} Pin

Applying a voltage to the VREF pin simply places that voltage on what would usually be the ground side of the gain resistor of the amplifier, resulting in a DC-level shift of the output signal. Applying 100mV to the Vref pin would apply a 100mV DC level shift to the outgoing signal. The charge pump provides sufficient bottom room to accommodate the shifted signal.

Note: The VREF input is the common point of the 3 amps minus input resistors. Any common resistance on VREF input will share the voltage induced on it with all the other amps, so using a resistor source to get offset will cause cross talk and gain change for the offset for all amps and amp +input gain change. Offset on the VREF pin must be low impedance to prevent gain error and cross talk. A transistor emitter follower

should work like an NPN MMBT3904 with the emitter connected to the VREF pin and 1k pull down to V- with $1\mu F$ cap bypass to ground and the collector to V+ and base to V offset source. If better tempco is needed then a diode may be used in series with the pot to ground. A 499W resistor may be added in series with the collector to prevent damage when testing.

See the Block Diagram on page 9.

The V_{EE} Pin

The V_{EE} pin is the output pin for the charge pump. A voltmeter applied to this pin will display the output of the charge pump. This pin does not affect the functionality of the part. One may use this pin as an additional voltage source. Keep in mind that the output of this pin is generated by the internal charge pump and a fully regulated supply that must be properly bypassed. We recommend a $0.1\mu\text{F}$ ceramic capacitor placed as close to the pin and connected to the ground plane of the board.

Input, Output, and Supply Voltage Range

The ISL59830A is designed to operate with a single supply voltage range of from 0V to 3.3V. The need for a split supply has been eliminated with the incorporation of a charge pump capable of generating a bottom rail as much as 1.6V below ground, for a 4.9V range on a single 3.3V supply. This performance is ideal for NTSC video with its negative-going sync pulses.

Video Performance

For good video performance, an amplifier is required to maintain the same output impedance and the same frequency and phase response as DC levels are changed at the output. This is especially difficult when driving a standard video load of 150Ω because of the change in output current with changing DC levels. Special circuitry has been incorporated into the ISL59830A for the reduction of output impedance variation with the current output. This results in outstanding differential gain and differential phase specifications of 0.06% and 0.1°, while driving 150Ω at a gain of +2. Driving higher impedance loads would result in similar or better differential gain and differential phase performance.

NTSC

The ISL59830A, generating a negative rail internally, is ideally suited for NTSC video with its accompanying negative-going sync signals; easily handled by the ISL59830A without the need of an additional supply as the ISL59830A generates a negative rail with an internal charge pump referenced at negative 1/2 the positive supply.

YPbPr

YPbPr signals originating from a DVD player requiring three channels of very tightly-controlled amplifier gain accuracy present no difficulty for the ISL59830A. Specifically, this standard encodes sync on the Y channel and it is a negative-going signal; easily handled by the ISL59830A without the need of an additional supply as the ISL59830A generates a negative rail placed at negative 1/2 the positive supply. Additionally, the Pb and Pr are



bipolar analog signals and the video signals are negative-going; and again easily handled by the ISL59830A.

Driving Capacitive Loads and Cables

The ISL59830A, internally-compensated to drive 75Ω cables, will drive 10pF loads in parallel with $1k\Omega$ with less than 5dB of peaking. If less peaking is required, a small series resistor, usually between 5Ω to 50Ω , can be placed in series with the output. This will reduce peaking at the expense of a slight closed loop gain reduction. When used as a cable driver, double termination is always recommended for reflection-free performance. For those applications, a back-termination series resistor at the amplifier's output will isolate the amplifier from the cable and allow extensive capacitive drive. However, other applications may have high capacitive loads without a back-termination resistor. Again, a small series resistor at the output can help to reduce peaking. The ISL59830A is a triple amplifier designed to drive three channels; simply deal with each channel separately as described in this section.

DC-Restore

When the ISL59830A is AC-coupled it becomes necessary to restore the DC reference for the signal. This is accomplished with a DC-restore system applied between the capacitive "AC" coupling and the input of the device. Refer to Application Circuit for reference DC-restore solution.

Disable/Power-Down

The ISL59830A can be disabled and its output placed in a high impedance state. The turn-off time is around 25ns and the turn-on time is around 200ns. When disabled, the amplifier's supply current is reduced to 0.9mA typically, thereby effectively eliminating the power consumption. The amplifier's power-down can be controlled by standard TTL or CMOS signal levels at the $\overline{\text{EN}}$ and PD pins. The applied logic signal is relative to V_S - pin. Letting the $\overline{\text{EN}}$ and PD pins float or applying a signal that is less than 0.8V above V_S - will enable the amplifier. The amplifier will be disabled when the signal at $\overline{\text{EN}}$ pin is 2V above V_S -. The amplifier must be disabled (EN pin is high) whenever the charge pump is disabled (PD pin is high). EN and PD pins should be connected together to allow amplifier and charge pump to enable/disable simultaneously.

Output Drive Capability

The ISL59830A does not have internal short-circuit protection circuitry. A short-circuit current of 80mA sourcing and 150mA sinking for the output is connected to half way between the rails with a 10Ω resistor. If the output is shorted indefinitely, the power dissipation could easily increase such that the part will be destroyed. Maximum reliability is maintained if the output current never exceeds $\pm 40\text{mA}$, after which the electromigration limit of the process will be exceeded and the part will be damaged. This limit is set by the design of the internal metal interconnections.

Power Dissipation

With the high output drive capability of the ISL59830A, it is possible to exceed the +150°C absolute maximum junction temperature under certain load current conditions. Therefore, it is important to calculate the maximum junction temperature for an application to determine if load conditions or package types need to be modified to assure operation of the amplifier in a safe operating area.

The maximum power dissipation allowed in a package is determined according to:

$$PD_{MAX} = \frac{T_{JMAX} - T_{AMAX}}{\Theta_{JA}}$$

Where:

T_{JMAX} = Maximum junction temperature

T_{AMAX} = Maximum ambient temperature

 Θ_{JA} = Thermal resistance of the package

The maximum power dissipation actually produced by an IC is the total quiescent supply current times the total power supply voltage, plus the power in the IC due to the load, or:

for sourcing:

$$PD_{MAX} = V_S \times I_{SMAX} + (V_S - V_{OUT}i) \times \frac{V_{OUT}i}{R_L i}$$

for sinking:

$$PD_{MAX} = V_S \times I_{SMAX} + (V_{OUT}i - V_S) \times I_{LOAD}i$$

Where:

V_S = Supply voltage

I_{SMAX} = Maximum quiescent supply current

V_{OUT} = Maximum output voltage of the application

RI OAD = Load resistance tied to ground

I_{LOAD} = Load current

i = Number of output channels

By setting the two P_{DMAX} equations equal to each other, we can solve the output current and R_{LOAD} to avoid the device overheat.



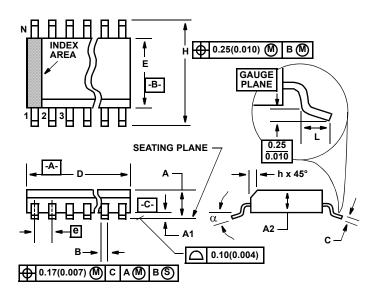
Power Supply Bypassing and Printed Circuit Board Layout

Strip line design techniques are recommended for the input and output signal traces. As with any high frequency device, a good printed circuit board layout is necessary for optimum performance. Lead lengths should be as short as possible. The power supply pin must be well bypassed to reduce the risk of oscillation. For normal single supply operation, where the V_S -pin is connected to the ground plane, a single 4.7µF tantalum capacitor in parallel with a $0.1\mu F$ ceramic capacitor from V_S + to GND will suffice. This same capacitor combination should be placed at each supply pin to ground if split-internal supplies are

to be used. In this case, the V_{S^-} pin becomes the negative supply rail.

For good AC performance, parasitic capacitance should be kept to a minimum. Use of wire-wound resistors should be avoided because of their additional series inductance. Use of sockets should also be avoided if possible. Sockets add parasitic inductance and capacitance can result in compromised performance. Minimizing parasitic capacitance at the amplifier's inverting input pin is also very important.

Shrink Small Outline Plastic Packages (SSOP) Quarter Size Outline Plastic Packages (QSOP)



NOTES:

- Symbols are defined in the "MO Series Symbol List" in Section 2.2 of Publication Number 95.
- 2. Dimensioning and tolerancing per ANSI Y14.5M-1982.
- Dimension "D" does not include mold flash, protrusions or gate burrs. Mold flash, protrusion and gate burrs shall not exceed 0.15mm (0.006 inch) per side.
- Dimension "E" does not include interlead flash or protrusions. Interlead flash and protrusions shall not exceed 0.25mm (0.010 inch) per side.
- 5. The chamfer on the body is optional. If it is not present, a visual index feature must be located within the crosshatched area.
- 6. "L" is the length of terminal for soldering to a substrate.
- 7. "N" is the number of terminal positions.
- 8. Terminal numbers are shown for reference only.
- Dimension "B" does not include dambar protrusion. Allowable dambar protrusion shall be 0.10mm (0.004 inch) total in excess of "B" dimension at maximum material condition.
- Controlling dimension: INCHES. Converted millimeter dimensions are not necessarily exact.

M16.15A

16 LEAD SHRINK SMALL OUTLINE PLASTIC PACKAGE
(0.150" WIDE BODY)

	INCHES MILLIMETERS				
SYMBOL	MIN	MAX	MIN	MAX	NOTES
Α	0.061	0.068	1.55	1.73	-
A1	0.004	0.0098	0.102	0.249	-
A2	0.055	0.061	1.40	1.55	-
В	0.008	0.012	0.20	0.31	9
С	0.0075	0.0098	0.191	0.249	-
D	0.189	0.196	4.80	4.98	3
Е	0.150	0.157	3.81	3.99	4
е	0.025 BSC		0.635	BSC	-
Н	0.230	0.244	5.84	6.20	-
h	0.010	0.016	0.25	0.41	5
L	0.016	0.035	0.41	0.89	6
N	16		1	6	7
α	0°	8°	0°	8°	-

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