National Semiconductor

Amplifiers

±1V to ±18V

LH0036/LH0036C Instrumentation Amplifier

General Description

The LH0036/LH0036C is a true micro power instrumentation amplifier designed for precision differential signal processing. Extremely high accuracy can be obtained due to the 300 M Ω input impedance and excellent 100 dB common mode rejection ratio. It is packaged in a hermetic TO-8 package. Gain is programmable with one external resistor from 1 to 1000. Power supply operating range is between ±1V and ±18V. Input bias current and output bandwidth are both externally adjustable or can be set by internally set values. The LH0036 is specified for operation over the -55° C to $+125^{\circ}$ C temperature range and the

LH0036C is specified for operation over the -25° C to $+85^{\circ}$ C temperature range.

Features

- High input impedance $300 \text{ M}\Omega$
- High CMRR
 100 dB
- Single resistor gain adjust 1 to 1000
- Low power 90µW
- Wide supply range
- Adjustable input bias current
- Adjustable output bandwidth
- Guard drive output

Equivalent Circuit and Connection Diagrams





Absolute Maximum Ratings

Supply Voltage Differential Input Voltage Input Voltage Range Shield Drive Voltage CMRR Preset Voltage CMRR Trim Voltage Power Dissipation (Note 3)
 ±18V
 Short Circuit Duration

 ±30V
 Operating Temperature Range

 ±V_S
 LH0036

 ±V_S
 LH0036C

 ±V_S
 Storage Temperature Range

±۷s

1.5W

Lead Temperature, Soldering 10 seconds

Continuous

-55°C to +125°C -25°C to +85°C -65°C to +150°C 300°C

Electrical Characteristics (Notes 1 and 2)

	CONDITIONS	LIMITS							
PARAMETER		LH0036			LH0036C			UNITS	
		MIN	Түр	MAX	MIN	ТҮР	MAX		
(V _{IOS})	$R_{S} = 1.0k\Omega, T_{A} = 25^{\circ}C$ $R_{S} = 1.0k\Omega$		0.5	1.0 2.0		1.0	2.0 3.0	mV mV	
Output Offset Voltage (V _{OOS})	$R_s = 1.0k\Omega$, $T_A = 25^{\circ}C$ $R_s = 1.0k\Omega$		2.0	5.0 6.0		5.0	10 12	mV mV	
Input Offset Voltage Tempco (ΔV _{IOS} /ΔT)	$R_{S} \leq 1.0 k\Omega$		10			10		µV/°C	
Output Offset Voltage Tempco (ΔV _{OOS} /ΔT)			15			15		µV/°C	
Overall Offset Referred to Input (V _{OS})	$A_V = 1.0$ $A_V = 10$ $A_V = 100$ $A_V = 1000$		2.5 0.7 0.52 0.502			6.0 1.5 1.05 1.005		mV mV mV mV	
Input Bias Current (I _B .)	T _A = 25°C		40	100 150		50	125 200	nA nA	
Input Offset Current (I _{OS})	T _A = 25°C		10	40 80		20	50 100	nA nA	
Small Signal Bandwidth			350 35 3.5 350			350 35 3.5 350		kHz kHz kHz Hz	
Full Power Bandwidth	$V_{IN} = \pm 10V, R_{\perp} = 10k,$ $A_V = 1,$		5.0			5.0		kHz	
Input Voltage Range	Differential Common Mode	±10 ±10	±12 ±12		±10 ±10	±12 ±12		v v	
Gain Nonlinearity			0.03			0.03		%	
Deviation From Gain Equation Formula	A _V = 1 to 1000		. ±0.3	±1.0		±1.0	±3.0	%	
PSRR	$\begin{array}{l} \pm 5.0V \leq V_{S} \leq \pm 15V, \\ A_{V} = 1.0 \\ \pm 5.0V \leq V_{S} \leq \pm 15V, \\ A_{V} = 100 \end{array}$		1.0 0.05	2.5 0.25		1.0 0.10	5.0 0.50	mV/V mV/V	
CMRR			1.0 0.1 50	2.5 0.25 100		2.5 0.25 50	5.0 0.50 100	mV/V mV/V μV/V	
Output Voltage	$V_{S} = \pm 15V, R_{L} = 10k\Omega, V_{S} = \pm 1.5V, R_{L} = 100k\Omega$	±10 ±0.6	±13.5 ±0.8		±10 ±C.6	±13.5 ±0.8		v v	
Output Resistance			0.5			0.5		Ω	
Supply Current			300	400		400	600	μA	
Equivalent Input Noise Voltage	0.1 Hz < f < 10 kHz, R _S < 50 Ω		20			20		μV/p-p	
Slew Rate	$\Delta V_{1N} = \pm 10V,$ R _L = 10k Ω , A _V = 1.0		0.3			0.3		V/µs	
Settling Time	To ±10 mV, R _L = 10k Ω , $\Delta V_{OUT} = 1.0V$					20			
	$A_V = 1.0$ $A_V = 100$		3.8 180			3.8 180		μs μs	

Note 1: Unless otherwise specified, all specifications apply for V_S = \pm 15V, Pins 1, 3, and 9 grounded, -25° C to $+85^{\circ}$ C for the LH0036C and -55° C to $+125^{\circ}$ C for the LH0036C.

Note 2: All typical values are for $T_A = 25^{\circ}C$.

Note 3: The maximum junction temperature is 150° C. For operation at elevated temperature derate the G package on a thermal resistance of 90° C/W, above 25° C.

Typical Performance Characteristics

LH0036/LH0036C



3-6

LH0036/LH0036C

3

Typical Applications





*Rew AND RE ARE OPTIONAL BANDWIDTH AND INPUT BIAS CURRENT CONTROLLING RESISTORS.

Instrumentation Amplifier with Logic Controlled Shut-Down

Pre MUX Signal Conditioning



Isolation Amplifier for Medical Telemetry



Thermocouple Amplifier with Cold Junction Compensation



Process Control Interface





High Pass Filter

Applications Information

THEORY OF OPERATION



The LH0036 is a 2 stage amplifier with a high input impedance gain stage comprised of A_1 and A_2 and a differential to single-ended unity gain stage, A_3 . Operational amplifier, A_1 , receives differential input signal, e_1 , and amplifies it by a factor equal to $(R1 + R_G)/R_G$.

 A_1 also receives input e_2 via A_2 and $R2, e_2$ is seen as an inverting signal with a gain of $R1/R_G.$ A_1 also receives the common mode signal e_{CM} and processes it with a gain of +1.

Hence:

$$V_{1} = \frac{R1 + R_{G}}{R_{G}} e_{1} - \frac{R1}{R_{G}} e_{2} + e_{CM}$$
(1)

By similar analysis V₂ is seen to be:

$$V_{2} = \frac{R2 + R_{G}}{R_{G}} e_{2} - \frac{R2}{R_{G}} e_{1} + e_{CM}$$
(2)

For R1 = R2:

$$V_2 - V_1 = \left[\left(\frac{2R1}{R_G} \right) + 1 \right] (e_2 - e_1)$$
 (3)

Also, for R3 = R5 = R4 = R6, the gain of $A_3 = 1$, and:

$$e_0 = (1)(V_2 - V_1) = (e_2 - e_1) \left[1 + \left(\frac{2R1}{R_G} \right) \right] (4)$$

As can be seen for identically matched resistors, e_{CM} is cancelled out, and the differential gain is dictated by equation (4).

For the LH0036, equation (4) reduces to:

$$A_{VCL} = \frac{e_0}{e_2 - e_1} = 1 + \frac{50k}{R_G}$$
(5a)

The closed loop gain may be set to any value from 1 ($R_G = \infty$) to 1000 ($R_G \cong 50\Omega$). Equation (5a) re-arranged in more convenient form may be used to select R_G for a desired gain:

$$R_{G} = \frac{50k}{A_{VCL} - 1}$$
(5b)

USE OF BANDWIDTH CONTROL (pin 1)

In the standard configuration, pin 1 of the LH0036 is simply grounded. The amplifier's slew rate in this configuration is typically $0.3V/\mu$ s and small

signal bandwidth 350 kHz for A_{VCL} = 1. In some applications, particularly at low frequency, it may be desirable to limit bandwidth in order to minimize the overall noise bandwidth of the device. A resistor R_{BW} may be placed between pin 1 and ground to accomplish this purpose. Figure 2 shows typical small signal bandwidth versus R_{BW} .



FIGURE 2. Bandwidth vs RBW

It also should be noted that large signal bandwidth and slew rate may be adjusted down by use of R_{BW} . Figure 3 is plot of slew rate versus R_{BW} .



FIGURE 3. Output Slew Rate vs RBW

CMRR CONSIDERATIONS

Use of Pin 9, CMRR Preset

Pin 9 should be grounded for nominal operation. An internal factory trimmed resistor, R6, will yield a CMRR in excess of 80 dB (for $A_{VCL} = 100$). Should a higher CMRR be desired, pin 9 should be left open and the procedure, in this section followed.

DC Off-set Voltage and Common Mode Rejection Adjustments

Off-set may be nulled using the circuit shown in Figure 4.



FIGURE 4. VOS Adjustment Circuit

Pin 8 is also used to improve the common mode rejection ratio as shown in Figure 5. Null is

-H0036/LH0036C

Applications Information (Cont'd)

achieved by alternately applying $\pm 10V$ (for V⁺ & V⁻ = 15V) to the inputs and adjusting R1 for minimum change at the output.



FIGURE 5. CMRR Adjustment Circuit

The circuits of Figure 4 and 5 may be combined as shown in Figure 6 to accomplish both V_{OS} and CMRR null. However, the V_{OS} and CMRR adjustment are interactive and several iterations are required. The procedure for null should start with the inputs grounded.



FIGURE 6. Combined CMRR, VOS Adjustment Circuit

R2 is adjusted for V_{OS} null. An input of +10V is then applied and R1 is adjusted for CMRR null. The procedure is then repeated until the optimum is achieved.

A circuit which overcomes adjustment interaction is shown in Figure 7. In this case, R2 is adjusted first for output null of the LH0036. R1 is then adjusted for output null with \pm 10V input. It is always a good idea to check CMRR null with a -10V input. The optimum null achievable will yield the highest CMRR over the amplifiers common mode range.



FIGURE 7. Improved VOS, CMRR Nulling Circuit

AC CMRR Considerations

The ac CMRR may be improved using the circuit of Figure 8.



FIGURE 8. Improved AC CMRR Circuit

After adjusting R1 for best dc CMRR as before, R2 should be adjusted for minimum peak-to-peak voltage at the output while applying an ac common mode signal of the maximum amplitude and frequency of interest.

INPUT BIAS CURRENT CONTROL

Under nominal operating conditions (pin 3 grounded), the LH0036 requires input currents of 40 nA. The input current may be reduced by inserting a resistor (R_B) between 3 and ground or, alternatively, between 3 and V^- . For R_B returned to ground, the input bias current may be predicted by:

$$_{\rm BIAS} \simeq \frac{\rm V^+ - 0.5}{\rm 4 \times 10^8 + 800 \ R_P}$$
(6a)

or R

$$R_{\rm B} = \frac{V^+ - 0.5 - (4 \times 10^8) (I_{\rm BIAS})}{800 I_{\rm BIAS}}$$
(6b)

Where:

I_{BIAS} = Input Bias Current (nA)

R_B = External Resistor connected between pin 3 and ground (Ohms)

V⁺ = Positive Supply Voltage (Volts)

Figure 9 is a plot of input bias current versus R_B.



FIGURE 9. Input Bias Current as a Function of RB

As indicated above, R_B may be returned to the negative supply voltage. Input bias current may then be predicted by:

$$I_{BIAS} \cong \frac{(V^+ - V^-) - 0.5}{4 \times 10^8 + 800 R_B}$$

Applications Information (Cont'd)

$$R_{B} \cong \frac{(V^{+} - V^{-}) - 0.5 - (4 \times 10^{8})(I_{BIAS})}{800 \text{ lows}}$$

Where:

or

IBIAS = Input Bias Current (nA)

R_B = External resistor connected between pin 3 and V⁻ (Ohms)

(8)

 V^+ = Positive Supply Voltage (Volts)

V⁻ = Negative Supply Voltage (Volts)





Figure 10 is a plot of input bias current versus R_B returned to V⁻ it should be noted that bandwidth is affected by changes in R_B . Figure 11 is a plot of bandwidth versus R_B .



FIGURE 11. Unity Gain Bandwidth as a Function of RB

BIAS CURRENT RETURN PATH CONSIDERATIONS

The LH0036 exhibits input bias currents typically in the 40 nA region in each input. This current must flow through $R_{\rm ISO}$ as shown in Figure 12.



FIGURE 12. Bias Current Return Path

In a typical application, V_S = ±15V, $I_{B1} \cong I_{B2} \cong$ 40 nA, the total current, I_T , would flow through R_{ISO} causing a voltage rise at point A. For values of $R_{ISO} \ge 150 \ M\Omega$, the voltage at point A exceeds the +12V common range of the device. Clearly, for $R_{ISO} = \infty$, the LH0036 would be driven to positive saturation.

The implication is that a finite impedance must be supplied between the input and power supply ground. The value of the resistor is dictated by the maximum input bias current, and the common mode voltage. Under worst case conditions:

$$R_{ISO} \leq \frac{V_{CMR} - V_{CM}}{I_{T}}$$
(9)

Where:

V_{CMR} = Common Mode Range (10V for the LH0036)

V_{CM} = Common Mode Voltage

 $I_T = I_{B1} + I_{B2}$

In applications in which the signal source is floating, such as a thermocouple, one end of the source may be grounded directly or through a resistor.

GUARD OUTPUT

Pin 2 of the LH0036 is provided as a guard drive pin in those stringent applications which require very low leakage and minimum input capacitance. Pin 2 will always be biased at the input common mode voltage. The source impedance looking into pin 2 is approximately 15 k Ω . Proper use of the guard/shield pin is shown in Figure 13.



FIGURE 13. Use of Guard

For applications requiring a lower source impedance than 15° k Ω , a unity gain buffer, such as the LH0002 may be inserted between pin 2 and the input shields as shown in Figure 14.



FIGURE 14. Guard Pin With Buffer

Definition of Terms

Bandwidth: The frequency at which the voltage gain is reduced to 0.707 of the low frequency (dc) value.

Closed Loop Gain, A_{VCL} : The ratio of the output voltage swing to the input voltage swing determined by A_{VCL} = 1 + (50k/R_G). Where: R_G = Gain Set Resistor.

Common Mode Rejection Ratio: The ratio of input voltage range to the peak-to-peak change in offset voltage over this range.

Gain Equation Accuracy: The deviation of the actual closed loop gain from the predicted closed loop gain, $A_{VCL} = 1 + (50k/R_G)$ for the specified closed loop gain.

Input Bias Current: The current flowing at pin 5 and 6 under the specified operating conditions.

Input Offset Current: The difference between the input bias current at pins 5 and 6; i.e. $I_{OS} = I_{15} - I_{6}I$.

Input Stage Offset Voltage, V_{IOS} : The voltage which must be applied to the input pins to force the output to zero volts for A_{VCL} = 100.

Output Stage Offset Voltage, VOCS: The voltage which must be applied to the input of the output stage to produce zero output voltage. It can be measured by measuring the overall offset at unity gain and subtracting V_{IOS} .

$$V_{OOS} = \left[V_{OS} \middle|_{A_{VCL}} = 1 \right]^{-} \left[V_{OS} \middle|_{A_{VCL}} = 1000 \right]$$

Overall Offset Voltage:

$$V_{OS} = V_{IOS} + \frac{V_{OOS}}{A_{VCL}}$$

Power Supply Rejection Ratio: The ratio of the change in offset voltage, V_{OS} , to the change in supply voltage producing it.

Resistor, R_B : An optional resistor placed between pin 3 of the LH0036 and ground (or V⁻) to reduce the input bias current.

Resistor, R_{BW} : An optional resistor placed between pin 1 of the LH0036 and ground (or V⁻) to reduce the bandwidth of the output stage.

Resistor, R_G : A gain setting resistor connected between pins 4 and 7 of the LH0036 in order to program the gain from 1 to 1000.

Settling Time: The time between the initiation of an input step function and the time when the output voltage has settled to within a specified error band of the final output voltage. LH0036/LH0036C