

## LM2746 Low Voltage N-Channel MOSFET Synchronous Buck Regulator Controller

Check for Samples: [LM2746](#)

### FEATURES

- Power stage input voltage from 1V to 16V
- Control stage input voltage from 3V to 5.5V
- Output voltage adjustable down to 0.6V
- Power good flag and shutdown
- Output overvoltage and undervoltage detection
- $\pm 1\%$  feedback voltage accuracy over temperature
- Low-side adjustable current sensing
- Adjustable soft-start

- Tracking and sequencing with shutdown and soft start pins
- Switching frequency from 50 kHz to 1 MHz
- Exposed pad TSSOP-14 package

### APPLICATIONS

- Cable Modem, DSL and ADSL
- Laser Jet and Ink Jet Printers
- Low Voltage Power Modules
- DSP, ASIC, Core and I/O

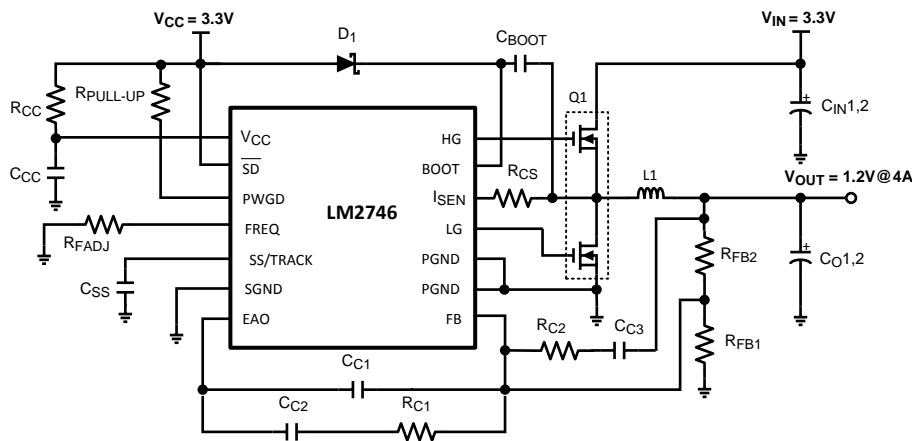
### DESCRIPTION

The LM2746 is a high-speed synchronous buck regulator controller with a feedback voltage accuracy of  $\pm 1\%$ . It can provide simple down conversion to output voltages as low as 0.6V. Though the control sections of the IC are rated for 3 to 5.5V, the driver sections are designed to accept input supply rails as high as 16V. The use of non-overlapping MOSFET gate drivers helps avoid potential shoot-through problems while maintaining high efficiency. The IC is designed for the more cost-effective option of driving only N-channel MOSFETs in both the high-side and low-side positions. It senses the low-side switch voltage drop for providing a simple, adjustable current limit.

The fixed-frequency voltage-mode PWM control architecture is adjustable from 50 kHz to 1 MHz with one external resistor. This wide range of switching frequency gives the power supply designer the flexibility to make better tradeoffs between component size, cost and efficiency.

Features include soft-start, input undervoltage lockout (UVLO) and Power Good (based on both undervoltage and overvoltage detection). In addition, the shutdown pin of the IC can be used for providing startup delay, and the soft-start pin can be used for implementing precise tracking, for the purpose of sequencing with respect to an external rail.

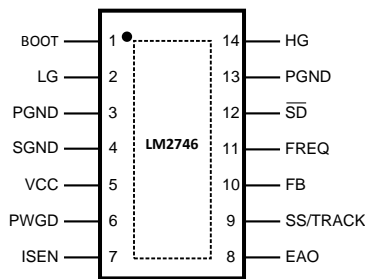
### Typical Application



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## Connection Diagram



**Figure 1. 14-Lead Plastic eTSSOP**

## Pin Functions

### Pin Descriptions

<b>BOOT (Pin 1)</b> - Bootstrap pin. This is the supply rail for the gate drivers. When the high-side MOSFET turns on, the voltage on this pin should be at least one gate threshold above the regulator input voltage $V_{IN}$ to properly turn on the MOSFET. See MOSFET Gate Drivers in the Application Information section for more details on how to select MOSFETs.
<b>LG (Pin 2)</b> - Low-gate drive pin. This is the gate drive for the low-side N-channel MOSFET. This signal is interlocked with the high-side gate drive HG (Pin 14), so as to avoid shoot-through.
<b>PGND (Pins 3, 13)</b> - Power ground. This is also the ground for the low-side MOSFET driver. Both pins must be connected together on the PCB to form a ground plane, which is usually the system ground.
<b>SGND (Pin 4)</b> - Signal ground. It should be connected appropriately to the ground plane with due regard to good layout practices in switching power regulator circuits.
<b>VCC (Pin 5)</b> Supply rail for the control sections of the IC.
<b>PWGD (Pin 6)</b> - Power Good pin. This is an open drain output, which is typically meant to be connected to $V_{CC}$ or any other low voltage source through a pull-up resistor. Choose the pull-up resistor so that the current going into this pin is kept below 1 mA. For most applications a recommended value for the pull-up resistor is 100 k $\Omega$ . The voltage on this pin is thus pulled low under output undervoltage or overvoltage fault conditions and also under input UVLO.
<b>ISEN (Pin 7)</b> - Current limit threshold setting pin. This sources a fixed 40 $\mu$ A current. A resistor of appropriate value should be connected between this pin and the drain of the low-side MOSFET (switch node). The minimum value for this resistor is 1 k $\Omega$ .
<b>EAO (Pin 8)</b> - Output of the error amplifier. The voltage level on this pin is compared with an internally generated ramp signal to determine the duty cycle. This pin is necessary for compensating the control loop.
<b>SS/TRACK (Pin 9)</b> - Soft-start and tracking pin. This pin is internally connected to the non-inverting input of the error amplifier during soft-start, and in fact any time the SS/TRACK pin voltage happens to be below the internal reference voltage. For the basic soft-start function, a capacitor of minimum value 1nF is connected from this pin to ground. To track the rising ramp of another power supply's output, connect a resistor divider from the output of that supply to this pin as described in Application Information.
<b>FB (Pin 10)</b> - Feedback pin. This is the inverting input of the error amplifier, which is used for sensing the output voltage and compensating the control loop.
<b>FREQ (Pin 11)</b> - Frequency adjust pin. The switching frequency is set by connecting a resistor of suitable value between this pin and ground. The equation for calculating the exact value is provided in Application Information, but some typical values (rounded up to the nearest standard values) are 324 k $\Omega$ for 100 kHz, 97.6 k $\Omega$ for 300 kHz, 56.2 k $\Omega$ for 500 kHz, 24.9 k $\Omega$ for 1 MHz.
<b>SD (Pin 12)</b> - IC shutdown pin. Pull this pin to $V_{CC}$ to ensure the IC is enabled. Connect to ground to disable the IC. Under shutdown, both high-side and low-side drives are off. This pin also features a precision threshold for power supply sequencing purposes, as well as a low threshold to ensure minimal quiescent current.
<b>HG (Pin 14)</b> - High-gate drive pin. This is the gate drive for the high-side N-channel MOSFET. This signal is interlocked with LG (Pin 2) to avoid shoot-through.
<b>EXPOSED PAD</b> - Connect to ground.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### Absolute Maximum Ratings <sup>(1)</sup>

V <sub>CC</sub>	-0.3 to 6.25V
BOOT Voltage	-0.3 to 21V
All other pins	-0.3 to V <sub>CC</sub> + 0.3V
Junction Temperature	150°C
Storage Temperature	-65°C to 150°C
Soldering Information	
Lead Temperature (soldering, 10sec)	260°C
Infrared or Convection (20sec)	235°C
ESD Rating <sup>(2)</sup>	2 kV

- (1) Absolute maximum ratings indicate limits beyond which damage to the device may occur. **Operating ratings** indicate conditions for which the device operates correctly. **Operating Ratings** do not imply guaranteed performance limits.
- (2) The human body model is a 100pF capacitor discharged through a 1.5k resistor into each pin.

### Operating Ratings

Supply Voltage Range (V <sub>CC</sub> )	3V to 5.5V
Power Stage Input Voltage (V <sub>IN</sub> )	1V to 16V
Junction Temperature Range (T <sub>J</sub> )	-40°C to +125°C
Thermal Resistance (θ <sub>JA</sub> )	38°C/W

## Electrical Characteristics

$V_{CC} = 3.3V$  unless otherwise indicated. Limits in standard type are for  $T_J = 25^\circ C$  only; limits in **boldface type** apply over the junction temperature ( $T_J$ ) range of  $-40^\circ C$  to  $+125^\circ C$ . Minimum and Maximum limits are guaranteed through test, design, or statistical correlation. Typical values represent the most likely parametric norm at  $T_J = 25^\circ C$ , and are provided for reference purposes only.

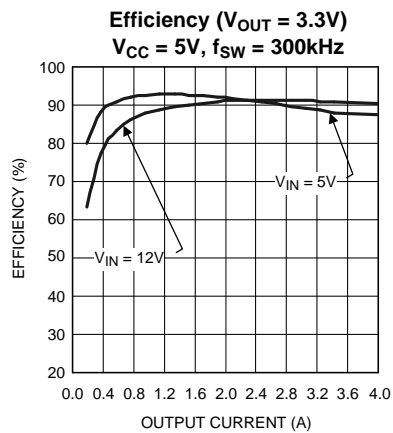
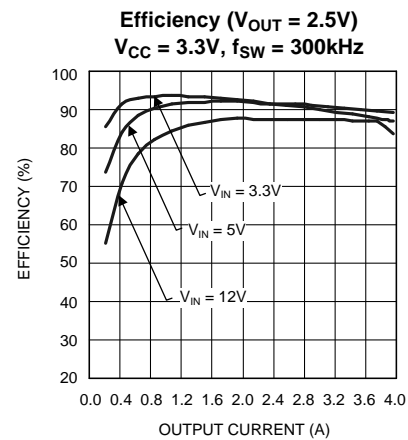
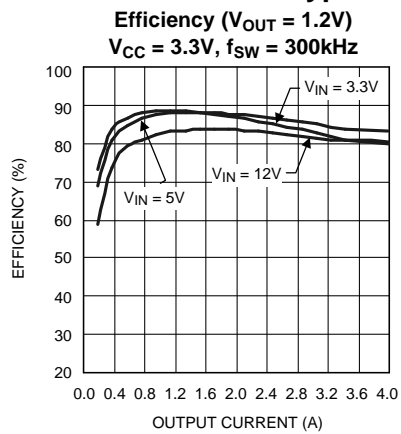
Symbol	Parameter	Conditions	Min	Typ	Max	Units
V <sub>FB</sub>	FB Pin Voltage	V <sub>CC</sub> = 3V to 5.5V				V
		T <sub>J</sub> = −25°C to +85°C	0.594	0.6	0.606	
		T <sub>J</sub> = −40°C to +125°C	0.592	0.6	0.608	
V <sub>ON</sub>	UVLO Thresholds	Rising Falling		2.76 2.42		V
I <sub>Q,VCC</sub>	Operating V <sub>CC</sub> Current	V <sub>CC</sub> = 3.3V, V <sub>SD</sub> = 3.3V F <sub>sw</sub> = 600kHz	1.0	1.5	2.1	mA
		V <sub>CC</sub> = 5V, V <sub>SD</sub> = 3.3V F <sub>sw</sub> = 600kHz	1.0	1.7	2.1	
	Shutdown V <sub>CC</sub> Current	V <sub>CC</sub> = 3.3V, V <sub>SD</sub> = 0V		1	5	μA
t <sub>PWGD1</sub>	PWGD Pin Response Time	V <sub>FB</sub> Rising		10		μs
t <sub>PWGD2</sub>	PWGD Pin Response Time	V <sub>FB</sub> Falling		10		μs
I <sub>SS-ON</sub>	SS Pin Source Current	V <sub>SS</sub> = 0V	7	10	14	μA
I <sub>SS-OC</sub>	SS Pin Sink Current During Over Current	V <sub>SS</sub> = 2.5V		100		μA
I <sub>SEN-TH</sub>	I <sub>SEN</sub> Pin Source Current Trip Point		25	40	55	μA
ERROR AMPLIFIER						
GBW	Error Amplifier Unity Gain Bandwidth			9		MHz
G	Error Amplifier DC Gain			106		dB
SR	Error Amplifier Slew Rate			3.2		V/μs
I <sub>EAO</sub>	EAO Pin Current Sourcing and Sinking Capability	V <sub>EAO</sub> = 1.5, FB = 0.55V V <sub>EAO</sub> = 1.5, FB = 0.65V		2.6 9.2		mA
V <sub>EA</sub>	Error Amplifier Output Voltage	Minimum		0		V
		Maximum		3.3		V
GATE DRIVE						
I <sub>Q-BOOT</sub>	BOOT Pin Quiescent Current	V <sub>BOOT</sub> = 12V, V <sub>SD</sub> = 0		18	90	μA
R <sub>HG_UP</sub>	High-Side MOSFET Driver Pull-Up ON resistance	V <sub>BOOT</sub> = 5V @ 350mA Sourcing		3		Ω
R <sub>HG_DN</sub>	High-Side MOSFET Driver Pull-Down ON resistance	V <sub>BOOT</sub> = 5V @ 350mA Sinking		2		Ω
R <sub>LG_UP</sub>	Low-Side MOSFET Driver Pull-Up ON resistance	V <sub>BOOT</sub> = 5V @ 350mA Sourcing		3		Ω
R <sub>LG_DN</sub>	Low-Side MOSFET Driver Pull-Down ON resistance	V <sub>BOOT</sub> = 5V @ 350mA Sinking		2		Ω
OSCILLATOR						
f <sub>SW</sub>	PWM Frequency	R <sub>FADJ</sub> = 702.1 kΩ		50		kHz
		R <sub>FADJ</sub> = 98.74 kΩ		300		
		R <sub>FADJ</sub> = 45.74 kΩ	475	600	725	
		R <sub>FADJ</sub> = 24.91 kΩ		1000		
D	Max High-Side Duty Cycle	f <sub>SW</sub> = 300kHz f <sub>SW</sub> = 600kHz f <sub>SW</sub> = 1MHz		80 76 73		%
LOGIC INPUTS AND OUTPUTS						
V <sub>SD-IH</sub>	$\overline{SD}$ Pin Logic High Trip Point	V <sub>SD</sub> Rising			1.3	V
V <sub>SD-IL</sub>	$\overline{SD}$ Pin Logic Low Trip Point	V <sub>SD</sub> Falling	0.8			V
V <sub>PWGD-TH-LO</sub>	PWGD Pin Trip Points	FB Falling	0.408	0.434	0.457	V
V <sub>PWGD-TH-HI</sub>	PWGD Pin Trip Points	FB Rising	0.677	0.710	0.742	V

## Electrical Characteristics (continued)

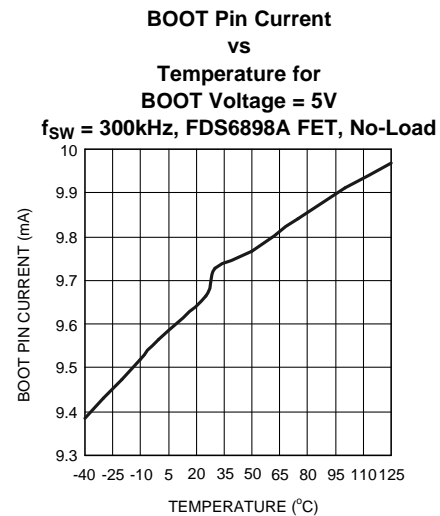
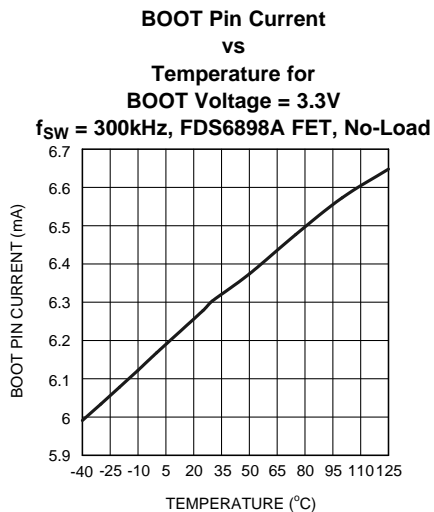
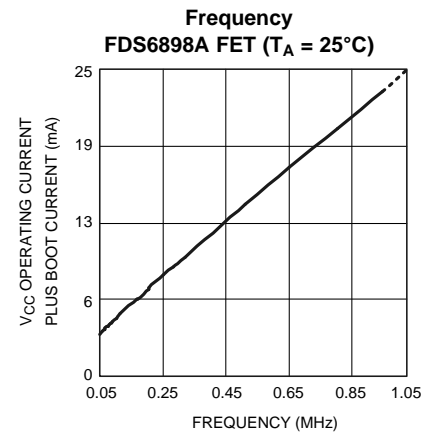
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Symbol	Parameter	Conditions	Min	Typ	Max	Units
$V_{PWGD-HYS}$	PWGD Hysteresis	FB Falling FB Rising		60 90		mV

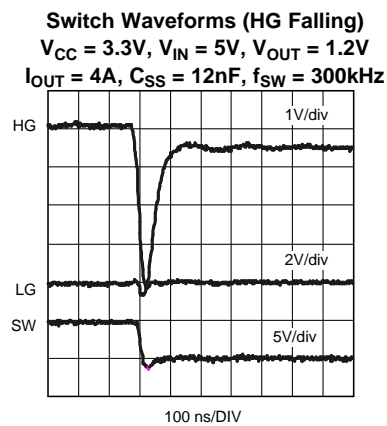
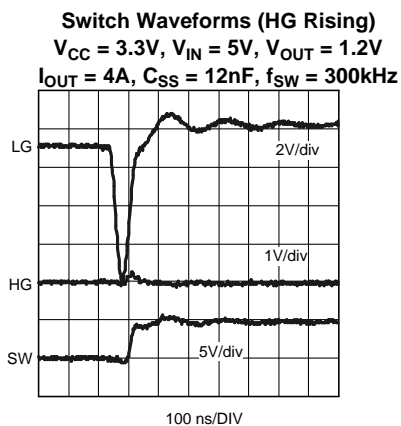
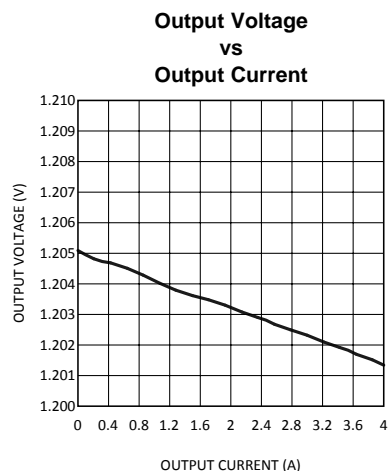
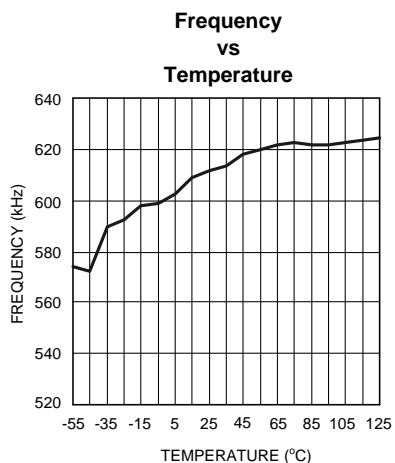
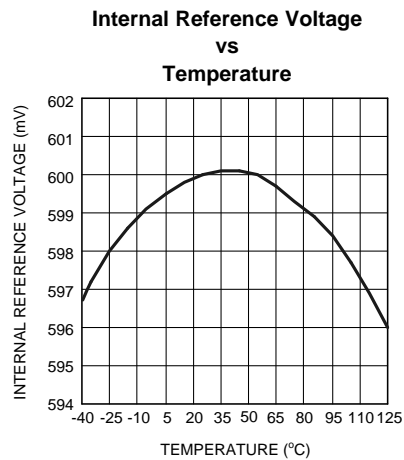
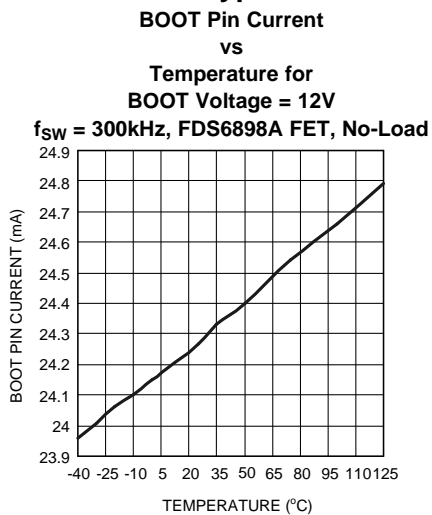
## Typical Performance Characteristics



**$V_{CC}$  Operating Current plus BOOT Current  
vs**



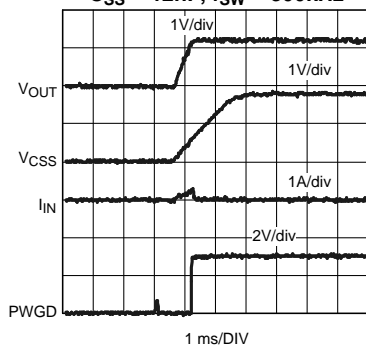
## Typical Performance Characteristics (continued)



## Typical Performance Characteristics (continued)

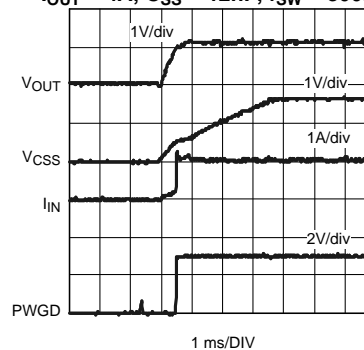
### Start-Up (No-Load)

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



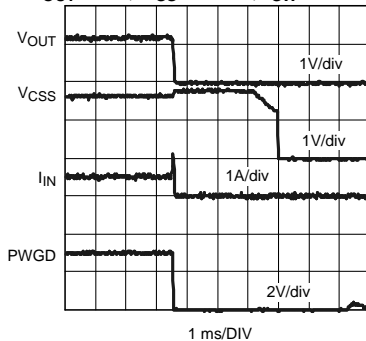
### Start-Up (Full-Load)

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $I_{OUT} = 4A$ ,  $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



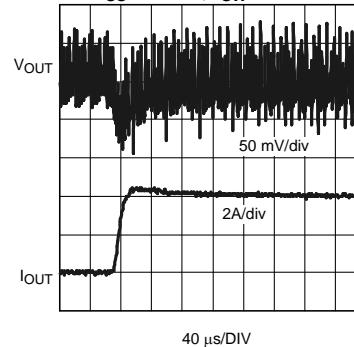
### Shutdown (Full-Load)

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $I_{OUT} = 4A$ ,  $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



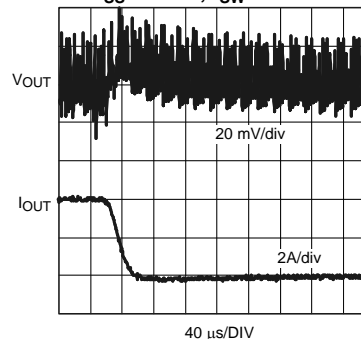
### Load Transient Response ( $I_{OUT} = 0A$ to $4A$ )

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



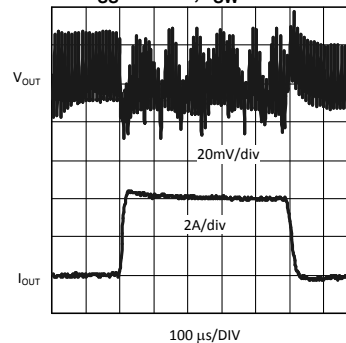
### Load Transient Response ( $I_{OUT} = 4A$ to $0A$ )

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



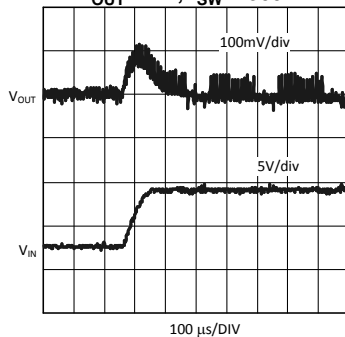
### Load Transient Response

$V_{CC} = 3.3V$ ,  $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$   
 $C_{SS} = 12nF$ ,  $f_{SW} = 300kHz$



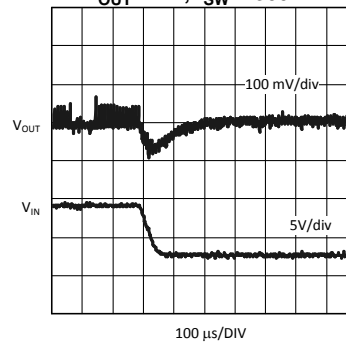
### Line Transient Response ( $V_{IN} = 3V$ to $9V$ )

$V_{CC} = 3.3V$ ,  $V_{OUT} = 1.2V$   
 $I_{OUT} = 2A$ ,  $f_{SW} = 300kHz$



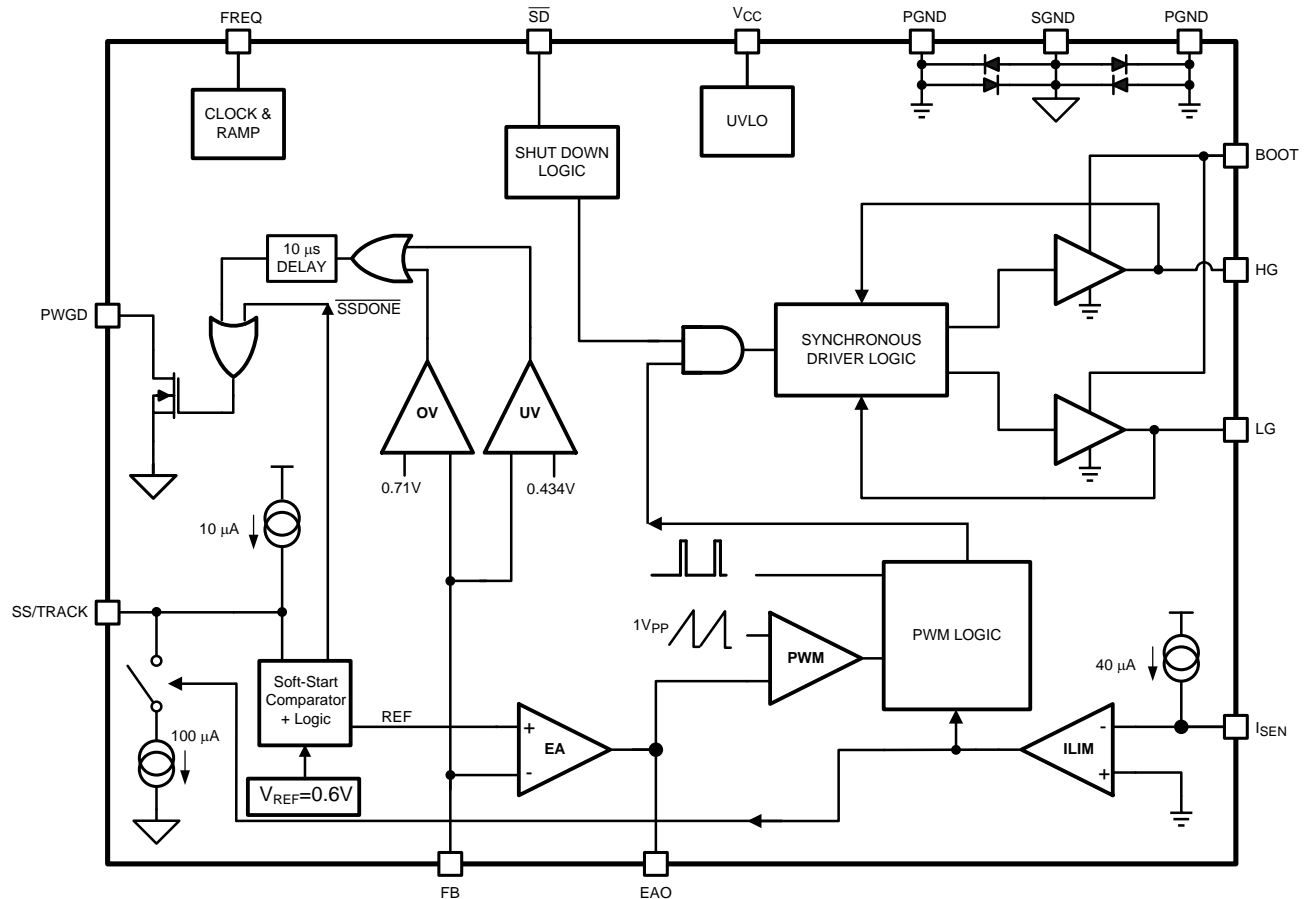
### Line Transient Response ( $V_{IN} = 9V$ to $3V$ )

$V_{CC} = 3.3V$ ,  $V_{OUT} = 1.2V$   
 $I_{OUT} = 2A$ ,  $f_{SW} = 300kHz$





## BLOCK DIAGRAM



## APPLICATION INFORMATION

### THEORY OF OPERATION

The LM2746 is a voltage-mode, high-speed synchronous buck regulator with a PWM control scheme. It is designed for use in set-top boxes, thin clients, DSL/Cable modems, and other applications that require high efficiency buck converters. It has output shutdown ( $\overline{SD}$ ), input undervoltage lock-out (UVLO) mode and power good (PWGD) flag (based on overvoltage and undervoltage detection). The overvoltage and undervoltage signals are logically OR'ed to drive the power good signal and provide a logic signal to the system if the output voltage goes out of regulation. Current limit is achieved by sensing the voltage  $V_{DS}$  across the low side MOSFET.

### START UP/SOFT-START

When  $V_{CC}$  exceeds 2.76V and the shutdown pin ( $\overline{SD}$ ) sees a logic high, the soft-start period begins. Then an internal, fixed 10  $\mu A$  source begins charging the soft-start capacitor. During soft-start the voltage on the soft-start capacitor  $C_{SS}$  is connected internally to the non-inverting input of the error amplifier. The soft-start period lasts until the voltage on the soft-start capacitor exceeds the LM2746 reference voltage of 0.6V. At this point the reference voltage takes over at the non-inverting error amplifier input. The capacitance of  $C_{SS}$  determines the length of the soft-start period, and can be approximated by:

$$C_{SS} = \frac{t_{SS}}{60} \quad (1)$$

Where  $C_{SS}$  is in  $\mu F$  and  $t_{SS}$  is in ms.

During soft start the Power Good flag is forced low and it is released when the FB pin voltage reaches 70% of 0.6V. At this point the chip enters normal operation mode, and the output overvoltage and undervoltage monitoring starts.

## NORMAL OPERATION

While in normal operation mode, the LM2746 regulates the output voltage by controlling the duty cycle of the high side and low side MOSFETs (see Typical Application Circuit). The equation governing output voltage is:

$$V_{OUT} = \frac{R_{FB1} + R_{FB2}}{R_{FB1}} V_{FB}$$

$$(V_{FB} = 0.6V)$$
(2)

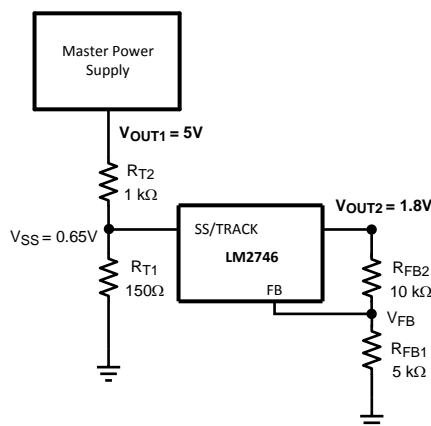
The PWM frequency is adjustable between 50 kHz and 1 MHz and is set by an external resistor,  $R_{FADJ}$ , between the FREQ pin and ground. The resistance needed for a desired frequency is approximately:

$$R_{FADJ} = -5.93 + 3.06 \frac{10^7}{f_{SW}} + 0.24 \frac{10^{12}}{f_{SW}^2}$$
(3)

Where  $f_{SW}$  is in Hz and  $R_{FADJ}$  is in k $\Omega$ .

## TRACKING A VOLTAGE LEVEL

The LM2746 can track the output of a master power supply during soft-start by connecting a resistor divider to the SS/TRACK pin. In this way, the output voltage slew rate of the LM2746 will be controlled by the master supply for loads that require precise sequencing. Because the output of the master supply is divided down, in order to track properly the output voltage of the LM2746 must be lower than the voltage of the master supply. When the tracking function is used no soft-start capacitor should be connected to the SS/TRACK pin. However in all other cases, a  $C_{SS}$  value of at least 1nF between the soft-start pin and ground should be used.



**Figure 2. Tracking Circuit**

One way to use the tracking feature is to design the tracking resistor divider so that the master supply's output voltage ( $V_{OUT1}$ ) and the LM2746's output voltage (represented symbolically in Figure 2 as  $V_{OUT2}$ , i.e. without explicitly showing the power components) both rise together and reach their target values at the same time. For this case, the equation governing the values of the tracking divider resistors  $R_{T1}$  and  $R_{T2}$  is:

$$0.65 = V_{OUT1} \frac{R_{T1}}{R_{T1} + R_{T2}}$$
(4)

The current through  $R_{T1}$  should be about 3-4 mA for precise tracking. The final voltage of the SS/TRACK pin should be set higher than the feedback voltage of 0.6V (say about 0.65V as in the above equation). If the master supply voltage were 5V and the LM2746 output voltage were 1.8V, for example, then the value of  $R_{T1}$  needed to give the two supplies identical soft-start times would be 150 $\Omega$ . A timing diagram for the equal soft-start time case is shown in Figure 3.

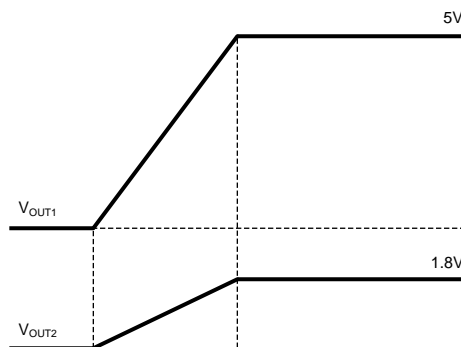


Figure 3. Tracking with Equal Soft-Start Time

### TRACKING A VOLTAGE SLEW RATE

The tracking feature can alternatively be used not to make both rails reach regulation at the same time but rather to have similar rise rates (in terms of output  $dV/dt$ ). This method ensures that the output voltage of the LM2746 always reaches regulation before the output voltage of the master supply. In this case, the tracking resistors can be determined based on the following equation:

$$0.65 = V_{OUT2} \frac{R_{T1}}{R_{T1} + R_{T2}} \quad (5)$$

For the example case of  $V_{OUT1} = 5V$  and  $V_{OUT2} = 1.8V$ , with  $R_{T1}$  set to  $150\Omega$  as before,  $R_{T2}$  is calculated from the above equation to be  $265\Omega$ . A timing diagram for the case of equal slew rates is shown in Figure 4.

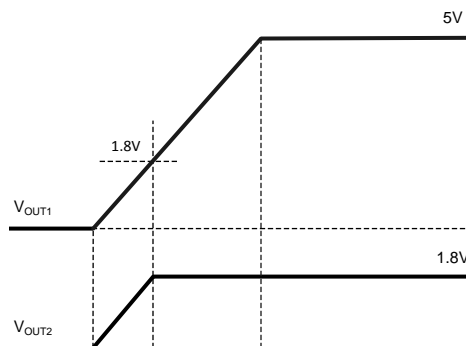


Figure 4. Tracking with Equal Slew Rates

### SEQUENCING

The start up/soft-start of the LM2746 can be delayed for the purpose of sequencing by connecting a resistor divider from the output of a master power supply to the  $\overline{SD}$  pin, as shown in Figure 5.

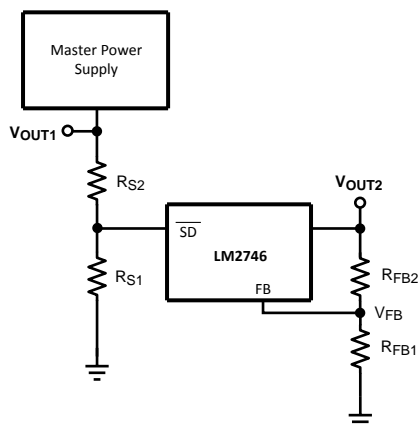


Figure 5. Sequencing Circuit

A desired delay time  $t_{\text{DELAY}}$  between the startup of the master supply output voltage and the LM2746 output voltage can be set based on the  $\overline{\text{SD}}$  pin low-to-high threshold  $V_{\text{SD-IH}}$  and the slew rate of the voltage at the  $\overline{\text{SD}}$  pin,  $\text{SR}_{\text{SD}}$ :

$$t_{\text{DELAY}} = V_{\text{SD-IH}} / \text{SR}_{\text{SD}} \quad (6)$$

Note again, that in Figure 5, the LM2746's output voltage has been represented symbolically as  $V_{\text{OUT2}}$ , i.e. without explicitly showing the power components.

$V_{\text{SD-IH}}$  is typically 1.08V and  $\text{SR}_{\text{SD}}$  is the slew rate of the  $\overline{\text{SD}}$  pin voltage. The values of the sequencing divider resistors  $R_{\text{S1}}$  and  $R_{\text{S2}}$  set the  $\text{SR}_{\text{SD}}$  based on the master supply output voltage slew rate,  $\text{SR}_{\text{OUT1}}$ , using the following equation:

$$\text{SR}_{\text{SD}} = \text{SR}_{\text{OUT1}} \frac{R_{\text{S1}}}{R_{\text{S1}} + R_{\text{S2}}} \quad (7)$$

For example, if the master supply output voltage slew rate were 1V/ms and the desired delay time between the startup of the master supply and LM2746 output voltage were 5ms, then the desired  $\overline{\text{SD}}$  pin slew rate would be  $(1.08\text{V}/5\text{ms}) = 0.216\text{V/ms}$ . Due to the internal impedance of the  $\overline{\text{SD}}$  pin, the maximum recommended value for  $R_{\text{S2}}$  is 1k $\Omega$ . To achieve the desired slew rate,  $R_{\text{S1}}$  would then be 274 $\Omega$ . A timing diagram for this example is shown in Figure 6.

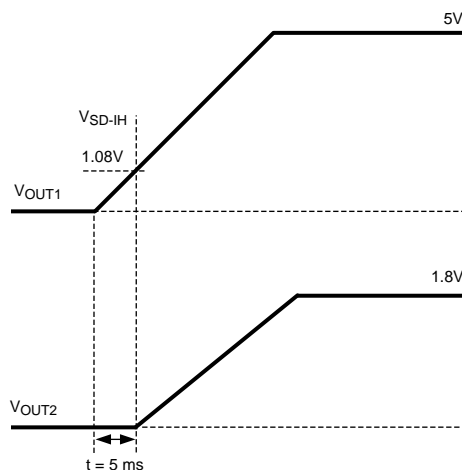


Figure 6. Delay for Sequencing

## $\overline{\text{SD}}$ PIN IMPEDANCE

When connecting a resistor divider to the  $\overline{\text{SD}}$  pin of the LM2746 some care has to be taken. Once the  $\overline{\text{SD}}$  voltage goes above  $V_{\text{SD-IH}}$ , a 17  $\mu\text{A}$  pull-up current is activated as shown in Figure 7. This current is used to create the internal hysteresis ( $\approx 170\text{mV}$ ); however, high external impedances will affect the  $\overline{\text{SD}}$  pin logic thresholds as well. The external impedance used for the sequencing divider network should preferably be a small fraction of the impedance of the  $\overline{\text{SD}}$  pin for good performance (around  $1\text{k}\Omega$ ).

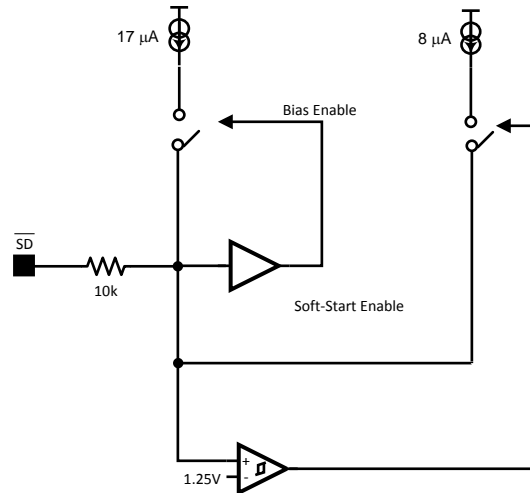


Figure 7.  $\overline{\text{SD}}$  Pin Logic

## MOSFET GATE DRIVERS

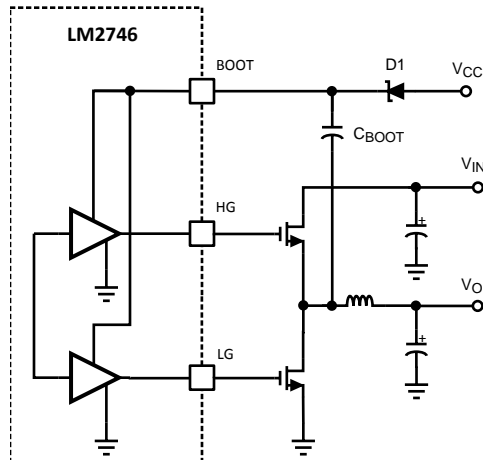
The LM2746 has two gate drivers designed for driving N-channel MOSFETs in a synchronous mode. Note that unlike most other synchronous controllers, the bootstrap capacitor of the LM2746 provides power not only to the driver of the upper MOSFET, but the lower MOSFET driver too (both drivers are ground referenced, i.e. no floating driver). To fully turn the top MOSFET on, the BOOT voltage must be at least one gate threshold greater than  $V_{\text{IN}}$  when the high-side drive goes high. This bootstrap voltage is usually supplied from a local charge pump structure. But looking at the Typical Application schematic, this also means that the difference voltage  $V_{\text{CC}} - V_{\text{D1}}$ , which is the voltage the bootstrap capacitor charges up to, must be always greater than the maximum tolerance limit of the threshold voltage of the upper MOSFET. Here  $V_{\text{D1}}$  is the forward voltage drop across the bootstrap diode D1. This therefore may place restrictions on the minimum input voltage and/or type of MOSFET used.

Two things must be kept in mind here. First, the BOOT pin has an absolute maximum rating of 21V. Since the bootstrap capacitor is connected to the SW node, the peak voltage impressed on the BOOT pin is the sum of the input voltage ( $V_{\text{IN}}$ ) plus the voltage across the bootstrap capacitor (ignoring any forward drop across the bootstrap diode). The bootstrap capacitor is charged up by a given rail (called  $V_{\text{BOOT\_DC}}$  here) whenever the upper MOSFET turns off. This rail can be the same as  $V_{\text{CC}}$  or it can be any external ground-referenced DC rail. But care has to be exercised when choosing this bootstrap DC rail that the BOOT pin is not damaged. For example, if the desired maximum  $V_{\text{IN}}$  is 16V, and  $V_{\text{BOOT\_DC}}$  is chosen to be the same as  $V_{\text{CC}}$ , then clearly if the  $V_{\text{CC}}$  rail is 5.5V, the peak voltage on the BOOT pin is  $16\text{V} + 5.5\text{V} = 21.5\text{V}$ . This is unacceptable, as it is in excess of the rating of the BOOT pin. A  $V_{\text{CC}}$  of 3V would be acceptable in this case. Or the  $V_{\text{IN}}$  range must be reduced accordingly. There is also the option of deriving the bootstrap DC rail from another 3V external rail, independent of  $V_{\text{CC}}$ .

The second thing to be kept in mind here is that the output of the low-side driver swings between the bootstrap DC rail level of  $V_{BOOT\_DC}$  and Ground, whereas the output of the high-side driver swings between  $V_{IN} + V_{BOOT\_DC}$  and Ground. To keep the high-side MOSFET fully on when desired, the Gate pin voltage of the MOSFET must be higher than its instantaneous Source pin voltage by an amount equal to the 'Miller plateau'. It can be shown that this plateau is equal to the threshold voltage of the chosen MOSFET plus a small amount equal to  $I_o/g$ . Here  $I_o$  is the maximum load current of the application, and  $g$  is the transconductance of this MOSFET (typically about 100 for logic-level devices). That means we must choose  $V_{BOOT\_DC}$  to at least exceed the Miller plateau level. This may therefore affect the choice of the threshold voltage of the external MOSFETs, and that in turn may depend on the chosen  $V_{BOOT\_DC}$  rail.

So far, in the discussion above, the forward drop across the bootstrap diode has been ignored. But since that does affect the output of the driver, it is a good idea to include this drop in the following examples. Looking at the Typical Application schematic, this means that the difference voltage  $V_{CC} - V_{D1}$ , which is the voltage the bootstrap capacitor charges up to, must always be greater than the maximum tolerance limit of the threshold voltage of the upper MOSFET. Here  $V_{D1}$  is the forward voltage drop across the bootstrap diode D1. This may place restrictions on the minimum input voltage and/or type of MOSFET used.

The basic bootstrap pump circuit can be built using one Schottky diode and a small capacitor, as shown in Figure 8. The capacitor  $C_{BOOT}$  serves to maintain enough voltage between the top MOSFET gate and source to control the device even when the top MOSFET is on and its source has risen up to the input voltage level. The charge pump circuitry is fed from  $V_{CC}$ , which can operate over a range from 3.0V to 6.0V. Using this basic method the voltage applied to the gates of both high-side and low-side MOSFETs is  $V_{CC} - V_D$ . This method works well when  $V_{CC}$  is  $5V \pm 10\%$ , because the gate drives will get at least 4.0V of drive voltage during the worst case of  $V_{CC\_MIN} = 4.5V$  and  $V_{D\_MAX} = 0.5V$ . Logic level MOSFETs generally specify their on-resistance at  $V_{GS} = 4.5V$ . When  $V_{CC} = 3.3V \pm 10\%$ , the gate drive at worst case could go as low as 2.5V. Logic level MOSFETs are not guaranteed to turn on, or may have much higher on-resistance at 2.5V. Sub-logic level MOSFETs, usually specified at  $V_{GS} = 2.5V$ , will work, but are more expensive, and tend to have higher on-resistance. The circuit in Figure 8 works well for input voltages ranging from 1V up to 16V and  $V_{CC} = 5V \pm 10\%$ , because the drive voltage depends only on  $V_{CC}$ .



**Figure 8. Basic Charge Pump (Bootstrap)**

Note that the LM2746 can be paired with a low cost linear regulator like the LM78L05 to run from a single input rail between 6.0 and 16V. The 5V output of the linear regulator powers both the  $V_{CC}$  and the bootstrap circuit, providing efficient drive for logic level MOSFETs. An example of this circuit is shown in Figure 9.

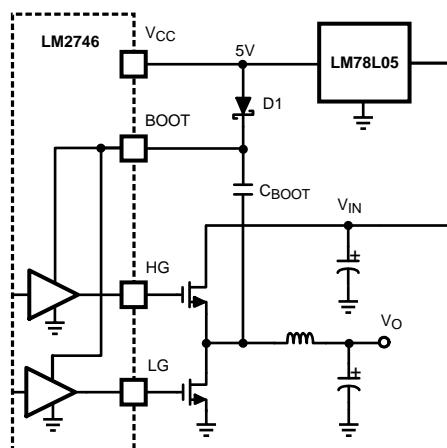


Figure 9. LM78L05 Feeding Basic Charge Pump

Figure 10 shows a second possibility for bootstrapping the MOSFET drives using a doubler. This circuit provides an equal voltage drive of  $V_{CC} - 3V_D + V_{IN}$  to both the high-side and low-side MOSFET drives. This method should only be used in circuits that use 3.3V for both  $V_{CC}$  and  $V_{IN}$ . Even with  $V_{IN} = V_{CC} = 3.0V$  (10% lower tolerance on 3.3V) and  $V_D = 0.5V$  both high-side and low-side gates will have at least 4.5V of drive. The power dissipation of the gate drive circuitry is directly proportional to gate drive voltage, hence the thermal limits of the LM2746 IC will quickly be reached if this circuit is used with  $V_{CC}$  or  $V_{IN}$  voltages over 5V.

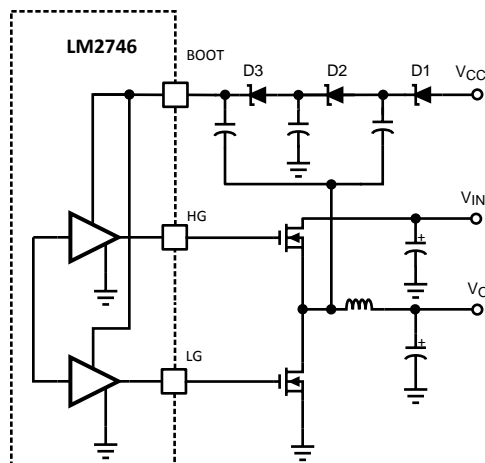


Figure 10. Charge Pump with Added Gate Drive

All the gate drive circuits shown in the above figures typically use 100nF ceramic capacitors in the bootstrap locations.

## POWER GOOD SIGNAL

The open drain output on the Power Good pin needs a pull-up resistor to a low voltage source. The pull-up resistor should be chosen so that the current going into the Power Good pin is less than 1 mA. A 100 kΩ resistor is recommended for most applications.

The Power Good signal is an OR-gated flag which takes into account both output overvoltage and undervoltage conditions. If the feedback pin (FB) voltage is 18% above its nominal value ( $118\% \times V_{FB} = 0.708V$ ) or falls 28% below that value ( $72\% \times V_{FB} = 0.42V$ ) the Power Good flag goes low. The Power Good flag can be used to signal other circuits that the output voltage has fallen out of regulation, however the switching of the LM2746 continues regardless of the state of the Power Good signal. The Power Good flag will return to logic high whenever the feedback pin voltage is between 72% and 118% of 0.6V.

## UVLO

The 2.76V turn-on threshold on  $V_{CC}$  has a built in hysteresis of about 300mV. If  $V_{CC}$  drops below 2.42V, the chip enters UVLO mode. UVLO consists of turning off the top and bottom MOSFETS and remaining in that condition until  $V_{CC}$  rises above 2.76V. As with shutdown, the soft-start capacitor is discharged through an internal MOSFET, ensuring that the next start-up will be controlled by the soft-start circuitry.

## CURRENT LIMIT

Current limit is realized by sensing the voltage across the low-side MOSFET while it is on. The  $R_{DS(on)}$  of the MOSFET is a known value; hence the current through the MOSFET can be determined as:

$$V_{DS} = I_{OUT} \times R_{DS(on)} \quad (8)$$

The current through the low-side MOSFET while it is on is also the falling portion of the inductor current. The current limit threshold is determined by an external resistor,  $R_{CS}$ , connected between the switching node and the  $I_{SEN}$  pin. A constant current of 40  $\mu A$  is forced through  $R_{CS}$ , causing a fixed voltage drop. This fixed voltage is compared against  $V_{DS}$  and if the latter is higher, the current limit of the chip has been reached. To obtain a more accurate value for  $R_{CS}$  you must consider the operating values of  $R_{DS(on)}$  and  $I_{SEN-TH}$  at their operating temperatures in your application and the effect of slight parameter differences from part to part.  $R_{CS}$  can be found by using the following equation using the  $R_{DS(on)}$  value of the low side MOSFET at its expected hot temperature and the absolute minimum value expected over the full temperature range for the  $I_{SEN-TH}$  which is 25  $\mu A$ :

$$R_{CS} = R_{DS(on)-HOT} \times I_{LIM} / 40 \mu A \quad (9)$$

For example, a conservative 15A current limit in a 10A design with a minimum  $R_{DS(on)}$  of 10m $\Omega$  would require a 6k $\Omega$  resistor. The minimum value for  $R_{CS}$  in any application is 1 k $\Omega$ . Because current sensing is done across the low-side MOSFET, no minimum high-side on-time is necessary. The LM2746 enters current limit mode if the inductor current exceeds the current limit threshold at the point where the high-side MOSFET turns off and the low-side MOSFET turns on. (The point of peak inductor current, see [Figure 11](#)). Note that in normal operation mode the high-side MOSFET always turns on at the beginning of a clock cycle. In current limit mode, by contrast, the high-side MOSFET on-pulse is skipped. This causes inductor current to fall. Unlike a normal operation switching cycle, however, in a current limit mode switching cycle the high-side MOSFET will turn on as soon as inductor current has fallen to the current limit threshold. The LM2746 will continue to skip high-side MOSFET pulses until the inductor current peak is below the current limit threshold, at which point the system resumes normal operation.

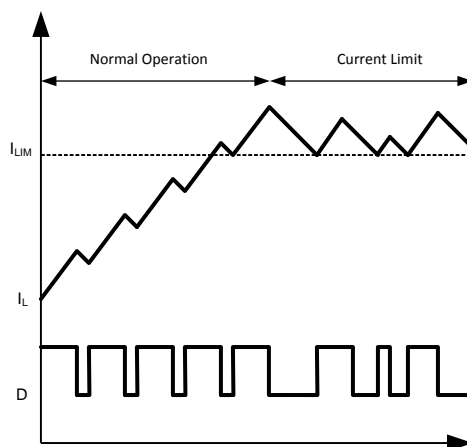


Figure 11. Current Limit Threshold



Unlike a high-side MOSFET current sensing scheme, which limits the peaks of inductor current, low-side current sensing is only allowed to limit the current during the converter off-time, when inductor current is falling. Therefore in a typical current limit plot the valleys are normally well defined, but the peaks are variable, according to the duty cycle. The PWM error amplifier and comparator control the off-pulse of the high-side MOSFET, even during current limit mode, meaning that peak inductor current can exceed the current limit threshold. Assuming that the output inductor does not saturate, the maximum peak inductor current during current limit mode can be calculated with the following equation:

$$I_{PK-CL} = I_{LIM} + (T_{SW} - 200 \text{ ns}) \frac{V_{IN} - V_O}{L} \quad (10)$$

Where  $T_{SW}$  is the inverse of switching frequency  $f_{SW}$ . The 200ns term represents the minimum off-time of the duty cycle, which ensures enough time for correct operation of the current sensing circuitry.

In order to minimize the time period in which peak inductor current exceeds the current limit threshold, the IC also discharges the soft-start capacitor through a fixed 90  $\mu$ A sink. The output of the LM2746 internal error amplifier is limited by the voltage on the soft-start capacitor. Hence, discharging the soft-start capacitor reduces the maximum duty cycle D of the controller. During severe current limit this reduction in duty cycle will reduce the output voltage if the current limit conditions last for an extended time. Output inductor current will be reduced in turn to a flat level equal to the current limit threshold. The third benefit of the soft-start capacitor discharge is a smooth, controlled ramp of output voltage when the current limit condition is cleared.

## SHUTDOWN

If the shutdown pin is pulled low, (below 0.8V) the LM2746 enters shutdown mode, and discharges the soft-start capacitor through a MOSFET switch. The high and low-side MOSFETs are turned off. The LM2746 remains in this state as long as  $V_{SD}$  sees a logic low (see the Electrical Characteristics table). To assure proper IC start-up the shutdown pin should not be left floating. For normal operation this pin should be connected directly to  $V_{CC}$  or to another voltage between 1.3V to  $V_{CC}$  (see the Electrical Characteristics table).

## DESIGN CONSIDERATIONS

The following is a design procedure for all the components needed to create the Typical Application Circuit shown on the front page. This design converts 3.3V ( $V_{IN}$ ) to 1.2V ( $V_{OUT}$ ) at a maximum load of 4A with an efficiency of 89% and a switching frequency of 300kHz. The same procedures can be followed to create many other designs with varying input voltages, output voltages, and load currents.

### Duty Cycle Calculation

The complete duty cycle for a buck converter is defined with the following equation:

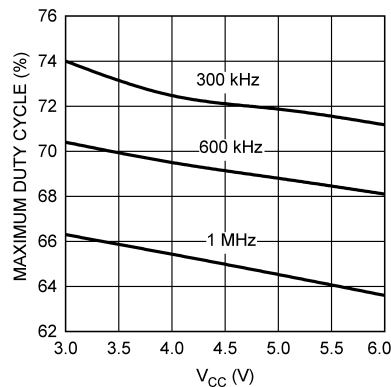
$$D = \frac{V_{OUT} + V_{SWL}}{V_{IN} - V_{SWH} + V_{SWL}} \quad (11)$$

where  $V_{SWL}$  and  $V_{SWH}$  are the respective forward voltage drops that develop across the low side and high side MOSFETs. Assuming the inductor ripple current is 20% to 30% of the output current, therefore:

$$V_{SWL} = I_{OUT} \times R_{DS(on)LOW} \text{ (Low-Side MOSFET)} \quad (12)$$

$$V_{SWH} = I_{OUT} \times R_{DS(on)HIGH} \text{ (High-Side MOSFET)} \quad (13)$$

To calculate the maximum duty cycle use the estimated 'hot'  $R_{DS(on)}$  value of the MOSFETs, the minimum input voltage, and maximum load. As shown in [Figure 12](#), the worst case maximum duty cycles of the LM2746 occurs at 125°C junction temperature vs  $V_{CC}$  (IC control section voltage). Ensure that the operating duty cycle is below the curve in [Figure 12](#), if this condition is not satisfied, the system will be unable to develop the required duty cycle to derive the necessary system power and so the output voltage will fall out of regulation.



**Figure 12. Maximum Duty Cycle vs V<sub>CC</sub>**  
**T<sub>J</sub> = 125°C**

### Input Capacitor

The input capacitors in a Buck converter are subjected to high stress due to the input current trapezoidal waveform. Input capacitors are selected for their ripple current capability and their ability to withstand the heat generated since that ripple current passes through their ESR. Input rms current is approximately:

$$I_{RMS} = I_{OUT} \times \sqrt{D(1-D)} \quad (14)$$

The power dissipated by each input capacitor is:

$$P_{CAP} = \frac{(I_{RMS})^2 \times ESR}{n^2} \quad (15)$$

where n is the number of capacitors, and ESR is the equivalent series resistance of each capacitor. The equation above indicates that power loss in each capacitor decreases rapidly as the number of input capacitors increases. The worst-case ripple for a Buck converter occurs during full load and when the duty cycle (D) is 0.5. For this 3.3V to 1.2V design the duty cycle is 0.364. For a 4A maximum load the ripple current is 1.92A.

### Output Inductor

The output inductor forms the first half of the power stage in a Buck converter. It is responsible for smoothing the square wave created by the switching action and for controlling the output current ripple ( $\Delta I_{OUT}$ ). The inductance is chosen by selecting between tradeoffs in efficiency and response time. The smaller the output inductor, the more quickly the converter can respond to transients in the load current. However, as shown in the efficiency calculations, a smaller inductor requires a higher switching frequency to maintain the same level of output current ripple. An increase in frequency can mean increasing loss in the MOSFETs due to the charging and discharging of the gates. Generally the switching frequency is chosen so that conduction loss outweighs switching loss. The equation for output inductor selection is:

$$L = \frac{V_{IN} - V_{OUT}}{\Delta I_{OUT} \times f_{SW}} \times D \quad (16)$$

$$L = \frac{3.3V - 1.2V}{0.4 \times 4A \times 300 \text{ kHz}} \times \frac{1.2V}{3.3V} \quad (17)$$

$$L = 1.6\mu H \quad (18)$$

Here we have plugged in the values for output current ripple, input voltage, output voltage, switching frequency, and assumed a 40% peak-to-peak output current ripple. This yields an inductance of 1.6  $\mu$ H. The output inductor must be rated to handle the peak current (also equal to the peak switch current), which is  $(I_{OUT} + 0.5 \times \Delta I_{OUT}) = 4.8A$ , for a 4A design. The Coilcraft DO3316P-222P is 2.2  $\mu$ H, is rated to 7.4A peak, and has a direct current resistance (DCR) of 12m $\Omega$ .

After selecting an output inductor, inductor current ripple should be re-calculated with the new inductance value, as this information is needed to select the output capacitor. Re-arranging the equation used to select inductance yields the following:

$$\Delta I_{OUT} = \frac{V_{IN(MAX)} - V_O}{F_{SW} \times L_{ACTUAL}} \times D \quad (19)$$

$V_{IN(MAX)}$  is assumed to be 10% above the steady state input voltage, or 3.6V. The actual current ripple will then be 1.2A. Peak inductor/switch current will be 4.6A.

## Output Capacitor

The output capacitor forms the second half of the power stage of a Buck switching converter. It is used to control the output voltage ripple ( $\Delta V_{OUT}$ ) and to supply load current during fast load transients.

In this example the output current is 4A and the expected type of capacitor is an aluminum electrolytic, as with the input capacitors. Other possibilities include ceramic, tantalum, and solid electrolyte capacitors, however the ceramic type often do not have the large capacitance needed to supply current for load transients, and tantalums tend to be more expensive than aluminum electrolytic. Aluminum capacitors tend to have very high capacitance and fairly low ESR, meaning that the ESR zero, which affects system stability, will be much lower than the switching frequency. The large capacitance means that at the switching frequency, the ESR is dominant, hence the type and number of output capacitors is selected on the basis of ESR. One simple formula to find the maximum ESR based on the desired output voltage ripple,  $\Delta V_{OUT}$  and the designed output current ripple,  $\Delta I_{OUT}$ , is:

$$ESR_{MAX} = \frac{\Delta V_{OUT}}{\Delta I_{OUT}} \quad (20)$$

In this example, in order to maintain a 2% peak-to-peak output voltage ripple and a 40% peak-to-peak inductor current ripple, the required maximum ESR is 20mΩ. The Sanyo 4SP560M electrolytic capacitor will give an equivalent ESR of 14mΩ. The capacitance of 560 μF is enough to supply energy even to meet severe load transient demands.

## MOSFETs

Selection of the power MOSFETs is governed by a tradeoff between cost, size, and efficiency. One method is to determine the maximum cost that can be endured, and then select the most efficient device that fits that price. Breaking down the losses in the high-side and low-side MOSFETs and then creating spreadsheets is one way to determine relative efficiencies between different MOSFETs. Good correlation between the prediction and the bench result is not guaranteed, however. Single-channel buck regulators that use a controller IC and discrete MOSFETs tend to be most efficient for output currents of 2-10A.

Losses in the high-side MOSFET can be broken down into conduction loss, gate charging loss, and switching loss. Conduction, or  $I^2R$  loss, is approximately:

$$P_C = D (I_O^2 \times R_{DS(on-HI)} \times 1.3) \text{ (High-Side MOSFET)} \quad (21)$$

$$P_C = (1 - D) \times (I_O^2 \times R_{DS(on-LO)} \times 1.3) \text{ (Low-Side MOSFET)} \quad (22)$$

In the above equations the factor 1.3 accounts for the increase in MOSFET  $R_{DS(on)}$  due to heating. Alternatively, the 1.3 can be ignored and the  $R_{DS(on)}$  of the MOSFET estimated using the  $R_{DS(on)}$  Vs. Temperature curves in the MOSFET datasheets.

Gate charging loss results from the current driving the gate capacitance of the power MOSFETs, and is approximated as:

$$P_{GC} = n \times (V_{DD}) \times Q_G \times f_{SW} \quad (23)$$

where 'n' is the number of MOSFETs (if multiple devices have been placed in parallel),  $V_{DD}$  is the driving voltage (see MOSFET Gate Drivers section) and  $Q_{GS}$  is the gate charge of the MOSFET. If different types of MOSFETs are used, the 'n' term can be ignored and their gate charges simply summed to form a cumulative  $Q_G$ . Gate charge loss differs from conduction and switching losses in that the actual dissipation occurs in the LM2746, and not in the MOSFET itself.

Switching loss occurs during the brief transition period as the high-side MOSFET turns on and off, during which both current and voltage are present in the channel of the MOSFET. It can be approximated as:

$$P_{SW} = 0.5 \times V_{IN} \times I_O \times (t_r + t_f) \times f_{SW} \quad (24)$$

where  $t_r$  and  $t_f$  are the rise and fall times of the MOSFET. Switching loss occurs in the high-side MOSFET only.

For this example, the maximum drain-to-source voltage applied to either MOSFET is 3.6V. The maximum drive voltage at the gate of the high-side MOSFET is 3.1V, and the maximum drive voltage for the low-side MOSFET is 3.3V. Due to the low drive voltages in this example, a MOSFET that turns on fully with 3.1V of gate drive is needed. For designs of 5A and under, dual MOSFETs in SO-8 provide a good tradeoff between size, cost, and efficiency.

### Support Components

**C<sub>IN2</sub>** - A small (0.1 to 1  $\mu$ F) ceramic capacitor should be placed as close as possible to the drain of the high-side MOSFET and source of the low-side MOSFET (dual MOSFETs make this easy). This capacitor should be X5R type dielectric or better.

**R<sub>CC</sub>, C<sub>CC</sub>** - These are standard filter components designed to ensure smooth DC voltage for the chip supply. R<sub>CC</sub> should be 1-10 $\Omega$ . C<sub>CC</sub> should 1  $\mu$ F, X5R type or better.

**C<sub>BOOT</sub>** - Bootstrap capacitor, typically 100nF.

**R<sub>PULL-UP</sub>** - This is a standard pull-up resistor for the open-drain power good signal (PWGD). The recommended value is 10 k $\Omega$  connected to V<sub>CC</sub>. If this feature is not necessary, the resistor can be omitted.

**D<sub>1</sub>** - A small Schottky diode should be used for the bootstrap. It allows for a minimum drop for both high and low-side drivers. The MBR0520 or BAT54 work well in most designs.

**R<sub>CS</sub>** - Resistor used to set the current limit. Since the design calls for a peak current magnitude ( $I_{OUT} + 0.5 \Delta I_{OUT}$ ) of 4.8A, a safe setting would be 6A. (This is below the saturation current of the output inductor, which is 7A.) Following the equation from the Current Limit section, a 1.3k $\Omega$  resistor should be used.

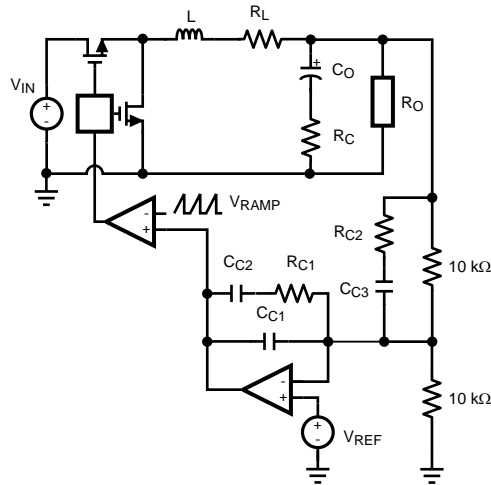
**R<sub>FADJ</sub>** - This resistor is used to set the switching frequency of the chip. The resistor value is calculated from equation in Normal Operation section. For 300 kHz operation, a 97.6 k $\Omega$  resistor should be used.

**C<sub>SS</sub>** - The soft-start capacitor depends on the user requirements and is calculated based on the equation given in the section titled *START UP/SOFT-START*. Therefore, for a 700 $\mu$ s delay, a 12nF capacitor is suitable.

### Control Loop Compensation

The LM2746 uses voltage-mode ('VM') PWM control to correct changes in output voltage due to line and load transients. One of the attractive advantages of voltage mode control is its relative immunity to noise and layout. However VM requires careful small signal compensation of the control loop for achieving high bandwidth and good phase margin.

The control loop is comprised of two parts. The first is the power stage, which consists of the duty cycle modulator, output inductor, output capacitor, and load. The second part is the error amplifier, which for the LM2746 is a 9MHz op-amp used in the classic inverting configuration. [Figure 13](#) shows the regulator and control loop components.



**Figure 13. Power Stage and Error Amp**

One popular method for selecting the compensation components is to create Bode plots of gain and phase for the power stage and error amplifier. Combined, they make the overall bandwidth and phase margin of the regulator easy to see. Software tools such as Excel, MathCAD, and Matlab are useful for showing how changes in compensation or the power stage affect system gain and phase.

The power stage modulator provides a DC gain  $A_{DC}$  that is equal to the input voltage divided by the peak-to-peak value of the PWM ramp. This ramp is 1.0V-P for the LM2746. The inductor and output capacitor create a double pole at frequency  $f_{DP}$ , and the capacitor ESR and capacitance create a single zero at frequency  $f_{ESR}$ . For this example, with  $V_{IN} = 3.3V$ , these quantities are:

$$A_{DC} = \frac{V_{IN}}{V_{RAMP}} = \frac{3.3}{1.0} = 10.4 \text{ dB} \quad (25)$$

$$f_{DP} = \frac{1}{2\pi} \sqrt{\frac{R_O + R_L}{LC_O(R_O + ESR)}} = 4.5 \text{ kHz} \quad (26)$$

$$f_{ESR} = \frac{1}{2\pi C_O ESR} = 20.3 \text{ kHz} \quad (27)$$

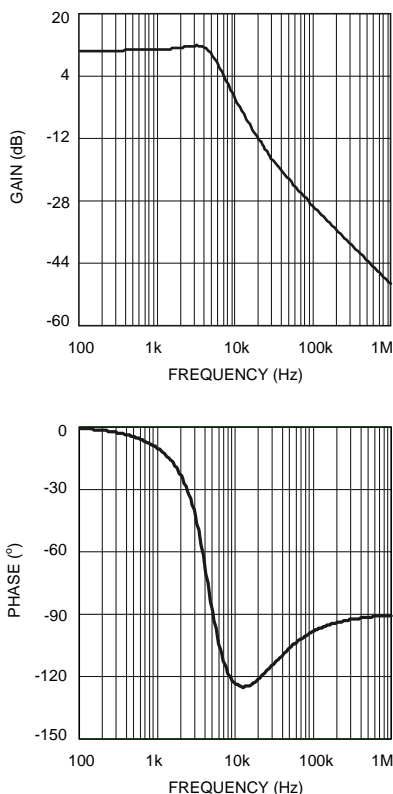
In the equation for  $f_{DP}$ , the variable  $R_L$  is the power stage resistance, and represents the inductor DCR plus the on resistance of the top power MOSFET.  $R_O$  is the output voltage divided by output current. The power stage transfer function  $G_{PS}$  is given by the following equation, and [Figure 14](#) shows Bode plots of the phase and gain in this example.

$$G_{PS} = \frac{V_{IN} \times R_O}{V_{RAMP}} \times \frac{sC_O R_C + 1}{a \times s^2 + b \times s + c} \quad (28)$$

$$a = LC_O(R_O + R_C)$$

$$b = L + C_O(R_O R_L + R_O R_C + R_C R_L)$$

$$c = R_O + R_L$$



**Figure 14. Power Stage Gain and Phase**

The double pole at 4.5kHz causes the phase to drop to approximately  $-130^\circ$  at around 10kHz. The ESR zero, at 20.3kHz, provides a  $+90^\circ$  boost that prevents the phase from dropping to  $-180^\circ$ . If this loop were left uncompensated, the bandwidth would be approximately 10kHz and the phase margin  $53^\circ$ . In theory, the loop would be stable, but would suffer from poor DC regulation (due to the low DC gain) and would be slow to respond to load transients (due to the low bandwidth.) In practice, the loop could easily become unstable due to tolerances in the output inductor, capacitor, or changes in output current, or input voltage. Therefore, the loop is compensated using the error amplifier and a few passive components.

For this example, a Type III, or three-pole-two-zero approach gives optimal bandwidth and phase.

In most voltage mode compensation schemes, including Type III, a single pole is placed at the origin to boost DC gain as high as possible. Two zeroes  $f_{Z1}$  and  $f_{Z2}$  are placed at the double pole frequency to cancel the double pole phase lag. Then, a pole,  $f_{P1}$  is placed at the frequency of the ESR zero. A final pole  $f_{P2}$  is placed at one-half of the switching frequency. The gain of the error amplifier transfer function is selected to give the best bandwidth possible without violating the Nyquist stability criteria. In practice, a good crossover point is one-fifth of the switching frequency, or 60kHz for this example. The generic equation for the error amplifier transfer function is:

$$G_{EA} = A_{EA} \times \frac{\left(\frac{s}{2\pi f_{Z1}} + 1\right)\left(\frac{s}{2\pi f_{Z2}} + 1\right)}{s\left(\frac{s}{2\pi f_{P1}} + 1\right)\left(\frac{s}{2\pi f_{P2}} + 1\right)} \quad (29)$$

In this equation the variable  $A_{EA}$  is a ratio of the values of the capacitance and resistance of the compensation components, arranged as shown in [Figure 13](#).  $A_{EA}$  is selected to provide the desired bandwidth. A starting value of 80,000 for  $A_{EA}$  should give a conservative bandwidth. Increasing the value will increase the bandwidth, but will also decrease phase margin. Designs with  $45^\circ$ - $60^\circ$  are usually best because they represent a good tradeoff between bandwidth and phase margin. In general, phase margin is lowest and gain highest (worst-case) for maximum input voltage and minimum output current. One method to select  $A_{EA}$  is to use an iterative process beginning with these worst-case conditions.

1. Increase  $A_{EA}$
2. Check overall bandwidth and phase margin
3. Change  $V_{IN}$  to minimum and recheck overall bandwidth and phase margin
4. Change  $I_O$  to maximum and recheck overall bandwidth and phase margin

The process ends when both bandwidth and phase margin are sufficiently high. For this example input voltage can vary from 3.0 to 3.6V and output current can vary from 0 to 4A, and after a few iterations a moderate gain factor of 101dB is used.

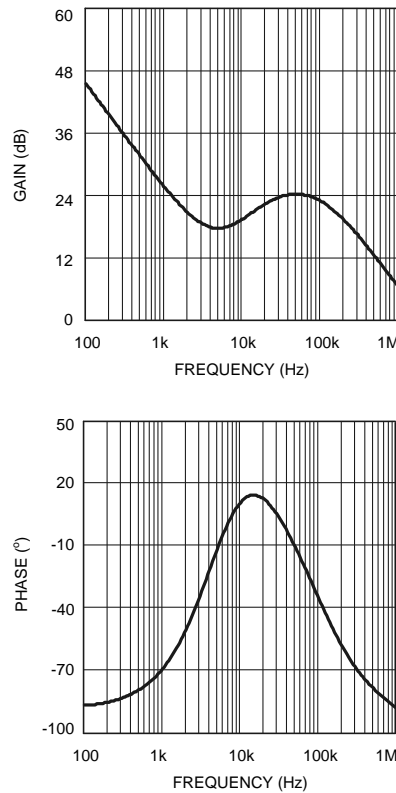
The error amplifier of the LM2746 has a unity-gain bandwidth of 9MHz. In order to model the effect of this limitation, the open-loop gain can be calculated as:

$$OPG = \frac{2\pi \times 9 \text{ MHz}}{s} \quad (30)$$

The new error amplifier transfer function that takes into account unity-gain bandwidth is:

$$H_{EA} = \frac{G_{EA} \times OPG}{1 + G_{EA} + OPG} \quad (31)$$

The gain and phase of the error amplifier are shown in [Figure 15](#).



**Figure 15. Error Amp. Gain and Phase**

In VM regulators, the top feedback resistor  $R_{FB2}$  forms a part of the compensation. Setting  $R_{FB2}$  to 10k $\Omega$ ,  $\pm 1\%$  usually gives values for the other compensation resistors and capacitors that fall within a reasonable range. (Capacitances > 1pF, resistances < 1M $\Omega$ )  $C_{C1}$ ,  $C_{C2}$ ,  $C_{C3}$ ,  $R_{C1}$ , and  $R_{C2}$  are selected to provide the poles and zeroes at the desired frequencies, using the following equations:

$$C_{C1} = \frac{f_{Z1}}{A_{EA} \times 10,000 \times f_{P2}} = 27 \text{ pF} \quad (32)$$

$$C_{C2} = \frac{1}{A_{EA} \times 10,000} - C_{C1} = 882 \text{ pF} \quad (33)$$

$$C_{C3} = \frac{1}{2\pi \times 10,000} \times \left( \frac{1}{f_{Z2}} - \frac{1}{f_{P1}} \right) = 2.73 \text{ nF} \quad (34)$$

$$R_{C1} = \frac{1}{2\pi \times C_{C2} \times f_{Z1}} = 39.8 \text{ k}\Omega \quad (35)$$

$$R_{C2} = \frac{1}{2\pi \times C_{C3} \times f_{P1}} = 2.55 \text{ k}\Omega \quad (36)$$

In practice, a good trade off between phase margin and bandwidth can be obtained by selecting the closest  $\pm 10\%$  capacitor values above what are suggested for  $C_{C1}$  and  $C_{C2}$ , the closest  $\pm 10\%$  capacitor value below the suggestion for  $C_{C3}$ , and the closest  $\pm 1\%$  resistor values below the suggestions for  $R_{C1}$ ,  $R_{C2}$ . Note that if the suggested value for  $R_{C2}$  is less than  $100\Omega$ , it should be replaced by a short circuit. Following this guideline, the compensation components will be:

$$C_{C1} = 27\text{pF} \pm 10\%, C_{C2} = 820\text{pF} \pm 10\%$$

$$C_{C3} = 2.7\text{nF} \pm 10\%, R_{C1} = 39.2\text{k}\Omega \pm 1\%$$

$$R_{C2} = 2.55\text{k}\Omega \pm 1\%$$

The transfer function of the compensation block can be derived by considering the compensation components as impedance blocks  $Z_F$  and  $Z_I$  around an inverting op-amp:

$$G_{EA-ACTUAL} = \frac{Z_F}{Z_I} \quad (37)$$

$$Z_F = \frac{\frac{1}{sC_{C1}} \times \left( 10,000 + \frac{1}{sC_{C2}} \right)}{10,000 + \frac{1}{sC_{C1}} + \frac{1}{sC_{C2}}} \quad (38)$$

$$Z_I = \frac{R_{C1} \left( R_{C2} + \frac{1}{sC_{C3}} \right)}{R_{C1} + R_{C2} + \frac{1}{sC_{C3}}} \quad (39)$$

As with the generic equation,  $G_{EA-ACTUAL}$  must be modified to take into account the limited bandwidth of the error amplifier. The result is:

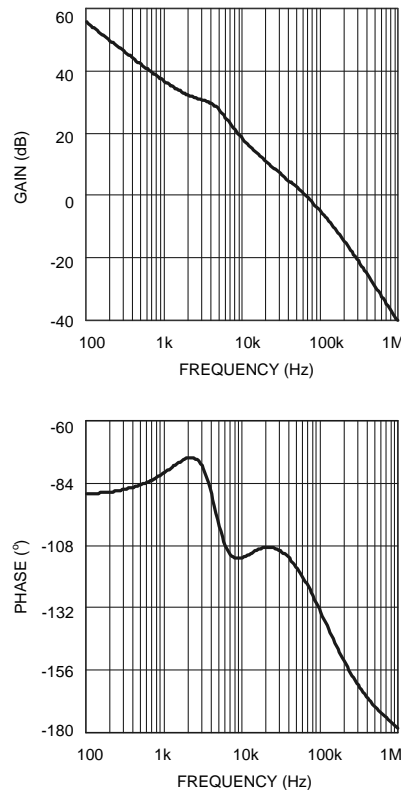
$$H_{EA} = \frac{G_{EA-ACTUAL} \times OPG}{1 + G_{EA-ACTUAL} \times OPG} \quad (40)$$

The total control loop transfer function  $H$  is equal to the power stage transfer function multiplied by the error amplifier transfer function.

$$H = G_{PS} \times H_{EA} \quad (41)$$

The bandwidth and phase margin can be read graphically from Bode plots of  $H_{EA}$  are shown in [Figure 16](#).





**Figure 16. Overall Loop Gain and Phase**

The bandwidth of this example circuit is 59kHz, with a phase margin of 60°.

## EFFICIENCY CALCULATIONS

The following is a sample calculation.

A reasonable estimation of the efficiency of a switching buck controller can be obtained by adding together the Output Power ( $P_{OUT}$ ) loss and the Total Power ( $P_{TOTAL}$ ) loss:

$$\eta = \frac{P_{OUT}}{P_{OUT} + P_{TOTAL}} \times 100\% \quad (42)$$

The Output Power ( $P_{OUT}$ ) for the Typical Application Circuit design is  $(1.2V \times 4A) = 4.8W$ . The Total Power ( $P_{TOTAL}$ ), with an efficiency calculation to complement the design, is shown below.

The majority of the power losses are due to low and high side of MOSFET's losses. The losses in any MOSFET are group of switching ( $P_{SW}$ ) and conduction losses ( $P_{CND}$ ).

$$P_{FET} = P_{SW} + P_{CND} = 61.38mW + 270.42mW \quad (43)$$

$$P_{FET} = 331.8mW \quad (44)$$

### FET Switching Loss ( $P_{SW}$ )

$$P_{SW} = P_{SW(ON)} + P_{SW(OFF)} \quad (45)$$

$$P_{SW} = 0.5 \times V_{IN} \times I_{OUT} \times (t_r + t_f) \times f_{SW} \quad (46)$$

$$P_{SW} = 0.5 \times 3.3V \times 4A \times 300kHz \times 31ns \quad (47)$$

$$P_{SW} = 61.38mW \quad (48)$$

The FDS6898A has a typical turn-on rise time  $t_r$  and turn-off fall time  $t_f$  of 15ns and 16ns, respectively. The switching losses for this type of dual N-Channel MOSFETs are 0.061W.

### FET Conduction Loss ( $P_{CND}$ )

$$P_{CND} = P_{CND1} + P_{CND2} \quad (49)$$

$$P_{CND1} = I_{OUT}^2 \times R_{DS(ON)} \times k \times D \quad (50)$$

$$P_{CND2} = I_{OUT}^2 \times R_{DS(ON)} \times k \times (1-D) \quad (51)$$

$R_{DS(ON)} = 13m\Omega$  and the factor is a constant value ( $k = 1.3$ ) to account for the increasing  $R_{DS(ON)}$  of a FET due to heating.

$$P_{CND1} = (4A)^2 \times 13m\Omega \times 1.3 \times 0.364 \quad (52)$$

$$P_{CND2} = (4A)^2 \times 13m\Omega \times 1.3 \times (1 - 0.364) \quad (53)$$

$$P_{CND} = 98.42mW + 172mW = 270.42mW \quad (54)$$

There are few additional losses that are taken into account:

#### IC Operating Loss ( $P_{IC}$ )

$$P_{IC} = I_{Q-VCC} \times V_{CC}, \quad (55)$$

where  $I_{Q-VCC}$  is the typical operating  $V_{CC}$  current

$$P_{IC} = 1.5mA \times 3.3V = 4.95mW \quad (56)$$

#### FET Gate Charging Loss ( $P_{GATE}$ )

$$P_{GATE} = n \times V_{CC} \times Q_{GS} \times f_{SW} \quad (57)$$

$$P_{GATE} = 2 \times 3.3V \times 3nC \times 300kHz \quad (58)$$

$$P_{GATE} = 5.94mW \quad (59)$$

The value  $n$  is the total number of FETs used and  $Q_{GS}$  is the typical gate-source charge value, which is 3nC. For the FDS6898A the gate charging loss is 5.94mW.

#### Input Capacitor Loss ( $P_{CAP}$ )

$$P_{CAP} = \frac{(I_{RMS})^2 \times ESR}{n^2} \quad (60)$$

where,

$$I_{RMS} = I_{OUT} \times \sqrt{D(1-D)} \quad (61)$$

Here  $n$  is the number of paralleled capacitors, ESR is the equivalent series resistance of each, and  $P_{CAP}$  is the dissipation in each. So for example if we use only one input capacitor of 24 mΩ.

$$P_{CAP} = \frac{(1.924A)^2 \times 24 \text{ m}\Omega}{1^2} \quad (62)$$

$$P_{CAP} = 88.8mW \quad (63)$$

#### Output Inductor Loss ( $P_{IND}$ )

$$P_{IND} = I_{OUT}^2 \times DCR \quad (64)$$

where DCR is the DC resistance. Therefore, for example

$$P_{IND} = (4A)^2 \times 11m\Omega \quad (65)$$

$$P_{IND} = 176mW \quad (66)$$

#### Total System Efficiency

$$P_{TOTAL} = P_{FET} + P_{IC} + P_{GATE} + P_{CAP} + P_{IND} \quad (67)$$

$$\eta = \frac{P_{OUT}}{P_{OUT} + P_{TOTAL}} \times 100\% \quad (68)$$

$$\eta = \frac{4.8W}{4.8W + 0.6W} = 89\% \quad (69)$$

## Example Circuits

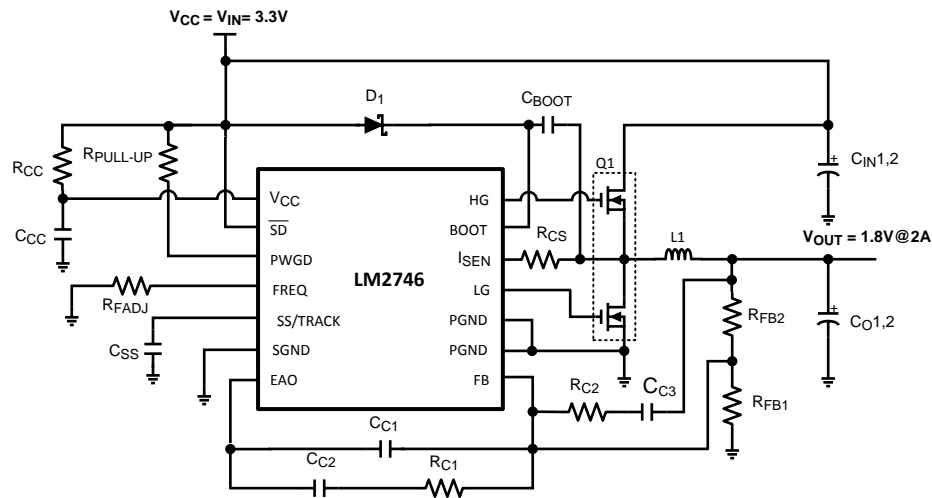
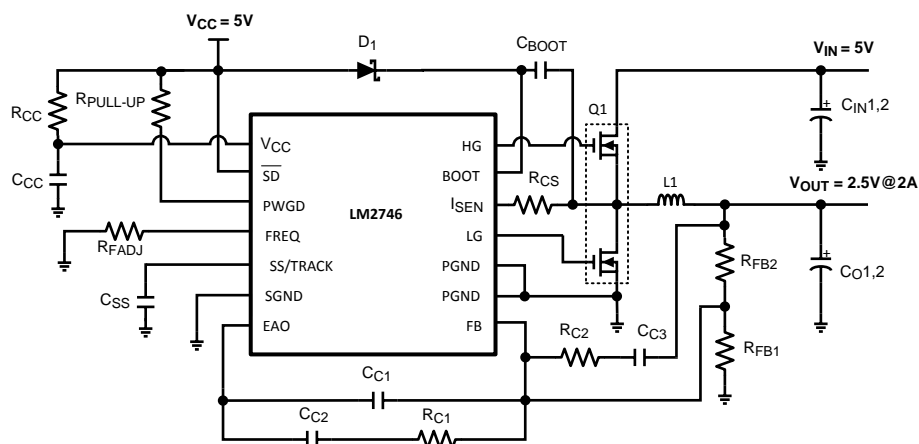


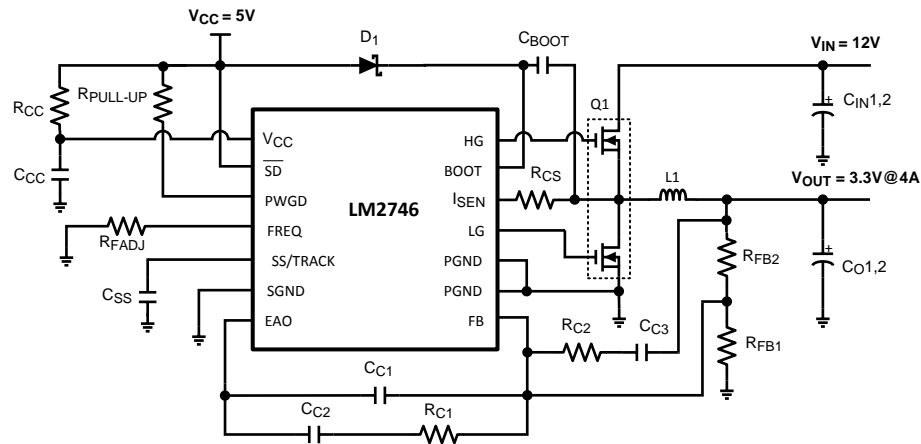
Figure 17. 3.3V to 1.8V @ 2A,  $f_{sw} = 300kHz$

PART	PART NUMBER	TYPE	PACKAGE	DESCRIPTION	VENDOR
U1	LM2746	Synchronous Controller	TSSOP-14		NSC
Q1	FDS6898A	Dual N-MOSFET	SO-8	20V, 10mΩ @ 4.5V, 16nC	Fairchild
D1	MBR0520LTI	Schottky Diode	SOD-123		
L1	DO3316P-472	Inductor		4.7μH, 4.8Arms 18mΩ	Coilcraft
C <sub>IN1</sub>	16SP100M	Aluminum Electrolytic	10mm x 6mm	100μF, 16V, 2.89Arms	Sanyo
C <sub>O1</sub>	6SP220M	Aluminum Electrolytic	10mm x 6mm	220μF, 6.3V 3.1Arms	Sanyo
C <sub>CC</sub> , C <sub>BOOT</sub> , C <sub>IN2</sub> , C <sub>O2</sub>	VJ1206Y104KXXA	Capacitor	1206	0.1μF, 10%	Vishay
C <sub>C3</sub>	VJ0805Y332KXXA	Capacitor	805	3300pF, 10%	Vishay
C <sub>SS</sub>	VJ0805A123KXAA	Capacitor	805	12nF, 10%	Vishay
C <sub>C2</sub>	VJ0805A821KXAA	Capacitor	805	820pF 10%	Vishay
C <sub>C1</sub>	VJ0805A220KXAA	Capacitor	805	22pF, 10%	Vishay
R <sub>FB2</sub>	CRCW08051002F	Resistor	805	10.0kΩ 1%	Vishay
R <sub>FB1</sub>	CRCW08054991F	Resistor	805	4.99kΩ 1%	Vishay
R <sub>FADJ</sub>	CRCW08051103F	Resistor	805	110kΩ 1%	Vishay
R <sub>C2</sub>	CRCW08052101F	Resistor	805	2.1kΩ 1%	Vishay
R <sub>CS</sub>	CRCW08052101F	Resistor	805	2.1 kΩ 1%	Vishay
R <sub>CC</sub>	CRCW080510R0F	Resistor	805	10.0Ω 1%	Vishay
R <sub>C1</sub>	CRCW08055492F	Resistor	805	54.9kΩ 1%	Vishay
R <sub>PULL-UP</sub>	CRCW08051003J	Resistor	805	100kΩ 5%	Vishay



**Figure 18. 5V to 2.5V @ 2A,  $f_{sw} = 300kHz$**

PART	PART NUMBER	TYPE	PACKAGE	DESCRIPTION	VENDOR
U1	LM2746	Synchronous Controller	TSSOP-14		NSC
Q1	FDS6898A	Dual N-MOSFET	SO-8	20V, 10mΩ@ 4.5V, 16nC	Fairchild
D1	MBR0520LTI	Schottky Diode	SOD-123		
L1	DO3316P-682	Inductor		6.8μH, 4.4Arms, 27mΩ	Coilcraft
C <sub>IN1</sub>	16SP100M	Aluminum Electrolytic	10mm x 6mm	100μF, 16V, 2.89Arms	Sanyo
C <sub>O1</sub>	10SP56M	Aluminum Electrolytic	6.3mm x 6mm	56μF, 10V 1.7Arms	Sanyo
C <sub>CC</sub> , C <sub>BOOT</sub> , C <sub>IN2</sub> , C <sub>O2</sub>	VJ1206Y104KXXA	Capacitor	1206	0.1μF, 10%	Vishay
C <sub>C3</sub>	VJ0805Y182KXXA	Capacitor	805	1800pF, 10%	Vishay
C <sub>SS</sub>	VJ0805A123KXAA	Capacitor	805	12nF, 10%	Vishay
C <sub>C2</sub>	VJ0805A821KXAA	Capacitor	805	820pF 10%	Vishay
C <sub>C1</sub>	VJ0805A330KXAA	Capacitor	805	33pF, 10%	Vishay
R <sub>FB2</sub>	CRCW08051002F	Resistor	805	10.0kΩ 1%	Vishay
R <sub>FB1</sub>	CRCW08053161F	Resistor	805	3.16kΩ 1%	Vishay
R <sub>FADJ</sub>	CRCW08051103F	Resistor	805	110kΩ 1%	Vishay
R <sub>C2</sub>	CRCW08051301F	Resistor	805	1.3kΩ 1%	Vishay
R <sub>CS</sub>	CRCW08052101F	Resistor	805	2.1 kΩ 1%	Vishay
R <sub>CC</sub>	CRCW080510R0F	Resistor	805	10.0Ω 1%	Vishay
R <sub>C1</sub>	CRCW08053322F	Resistor	805	33.2kΩ 1%	Vishay
R <sub>PULL-UP</sub>	CRCW08051003J	Resistor	805	100kΩ 5%	Vishay



**Figure 19. 12V to 3.3V @ 4A,  $f_{SW} = 300kHz$**

PART	PART NUMBER	TYPE	PACKAGE	DESCRIPTION	VENDOR
U1	LM2746	Synchronous Controller	TSSOP-14		NSC
Q1	FDS6898A	Dual N-MOSFET	SO-8	20V, 10mΩ@ 4.5V, 16nC	Fairchild
D1	MBR0520LTI	Schottky Diode	SOD-123		
L1	DO3316P-332	Inductor		3.3μH, 5.4Arms 15mΩ	Coilcraft
CIN1	16SP100M	Aluminum Electrolytic	10mm x 6mm	100μF, 16V, 2.89Arms	Sanyo
CO1	6SP220M	Aluminum Electrolytic	10mm x 6mm	220μF, 6.3V 3.1Arms	Sanyo
C <sub>CC</sub> , C <sub>BOOT</sub> , C <sub>IN2</sub> , C <sub>O2</sub>	VJ1206Y104KXXA	Capacitor	1206	0.1μF, 10%	Vishay
CC3	VJ0805Y222KXXA	Capacitor	805	2200pF, 10%	Vishay
CSS	VJ0805A123KXAA	Capacitor	805	12nF, 10%	Vishay
CC2	VJ0805Y332KXXA	Capacitor	805	3300pF 10%	Vishay
CC1	VJ0805A820KXAA	Capacitor	805	82pF, 10%	Vishay
RFB2	CRCW08051002F	Resistor	805	10.0kΩ 1%	Vishay
RFB1	CRCW08052211F	Resistor	805	2.21kΩ 1%	Vishay
RFADJ	CRCW08051103F	Resistor	805	110kΩ 1%	Vishay
RC2	CRCW08052611F	Resistor	805	2.61kΩ 1%	Vishay
RCS	CRCW08054121F	Resistor	805	4.12 kΩ 1%	Vishay
RCC	CRCW080510R0F	Resistor	805	10.0Ω 1%	Vishay
RC1	CRCW08051272F	Resistor	805	12.7kΩ 1%	Vishay
RPULL-UP	CRCW08051003J	Resistor	805	100kΩ 5%	Vishay

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