



LM4947 Boomer® Audio Power Amplifier Series Mono Class D and Stereo Audio Subsystem with OCL Headphone Amplifier and National 3D General Description Key Specifications

The LM4947 is an audio subsystem capable of efficiently delivering 500mW (Class D operation) of continuous average power into a mono 8Ω bridged-tied load (BTL) with 1% THD+N, 37mW (Class AB operation) power channel of continuous average power into stereo 32Ω single-ended (SE) loads with 1% THD+N, or an output capacitor-less (OCL) configuration with identical specification as the SE configuration, from a 3.3V power supply.

The LM4947 has six input channels: one pair for a twochannel stereo signal, the second pair for a secondary twochannel stereo input, and the third pair for a differential single-channel mono input. Additionally, the two sets of stereo inputs may be configured as a single stereo differential input (differential left and differential right). The LM4947 features a 32-step digital volume control and eight distinct output modes. The digital volume control, 3D enhancement, and output modes are programmed through a two-wire I²C compatible interface that allows flexibility in routing and mixing audio channels.

The RF suppression circuitry in the LM4947 makes it wellsuited for GSM mobile phones and other portable applications in which strong RF signals generated by an antenna (and long output traces) may couple audibly into the amplifier.

The LM4947 is designed for cellular phones, PDAs, and other portable handheld applications. It delivers high quality output power from a surface-mount package and requires only eight external components in the OCL mode (two additional components in SE mode).

THD+N at 1kHz, 500mW	
into 8Ω BTL (3.3V)	1.0% (typ)
THD+N at 1kHz, 37mW	
into 32Ω SE (3.3V)	1.0% (typ)
 Single Supply Operation (V_{DD}) 	2.7 to 5.5V
 I²C Single Supply Operation 	2.2 to 5.5V

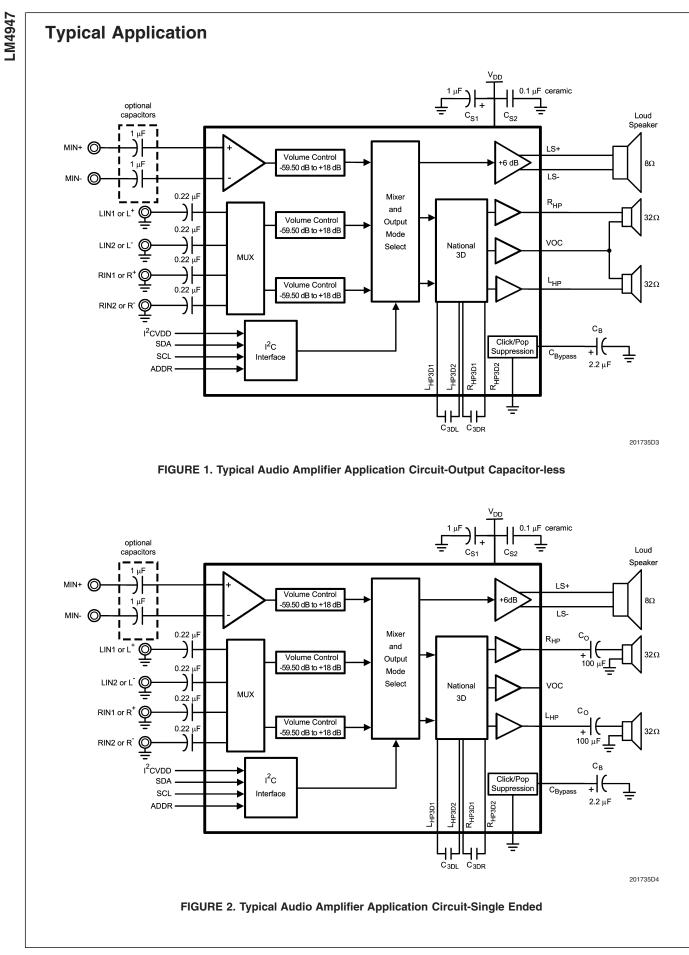
Features

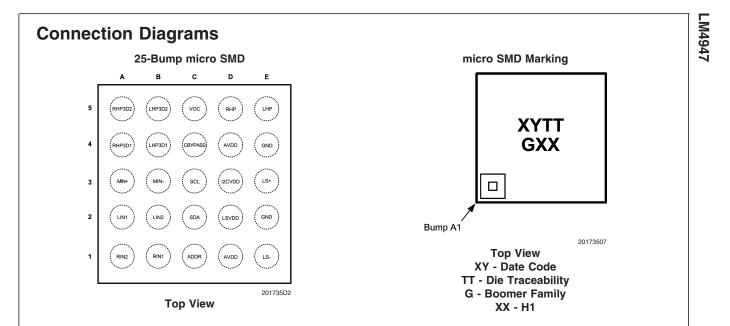
- I²C Control Interface
- I²C programmable National 3D Audio
- I²C controlled 32 step digital volume control (-59.5dB to +18dB)
- Three independent volume channels (Left, Right, Mono)
- Eight distinct output modes
- Small, 25-bump micro SMD packaging
- "Click and Pop" suppression circuitry
- Thermal shutdown protection
- Low shutdown current (0.1µA, typ)
- RF suppression
- Differential mono and stereo inputs
- Stereo input mux

Applications

- Mobile Phones
- PDAs

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Pin Descriptions

Bump	Name	Description
A1	R _{IN2}	Right Input Channel 2 or Right Differential Input -
A2	L _{IN1}	Left Input Channel 1 or Left Differential Input +
A3	MIN+	Mono Channel Non-inverting Input
A4	RHP _{3D1}	Right Headphone 3D Input 1
A5	RHP _{3D2}	Right Headphone 3D Input 2
B1	R _{IN1}	Right Input Channel 1 or Right Differential Input +
B2	L _{IN2}	Left Input Channel 2 or Left Differential Input -
B3	MIN-	Mono Channel Inverting Input
B4	L _{HP3D1}	Left Headphone 3D Input 2
B5	L _{HP3D2}	Left Headphone 3D Input 1
C1	ADDR	Address Identification
C2	SDA	Serial Data Input
C3	SCL	Serial Clock Input
C4	C _{BYPASS}	Half-Supply Bypass Capacitor
C5	VOC	Headphone return bias output
D1	AV _{DD}	Analog Power Supply
D2	LSV _{DD}	Loudspeaker Power Supply
D3	I2CV _{DD}	I2C Interface Power Supply
D4	AV _{DD}	Analog Power Supply
D5	R _{HP}	Right Headphone Output
E1	LS-	Loudspeaker Output Negative
E2	GND	Ground
E3	LS+	Loudspeaker Output Positive
E4	GND	Ground
E5	L _{HP}	Left Headphone Output

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Absolute Maximum Ratings (Note 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Supply Voltage	6.0V
Storage Temperature	–65°C to +150°C
Input Voltage	–0.3 to V_{DD} +0.3
ESD Susceptibility (Note 3)	2.0kV
ESD Machine model (Note 6)	200V
Junction Temperature (T _J)	150°C
Solder Information	

Vapor Phase (60 sec.)	215°C
Infrared (15 sec.)	220°C
Thermal Resistance	
θ _{JA} (typ) - TLA25CBA	65°C/W

Operating Ratings

Temperature Range	–40°C to 85°C
Supply Voltage (V _{DD})	$2.7V \leq V_{DD} \leq 5.5V$
Supply Voltage (I ² C)	$2.2V \leq V_{DD} \leq 5.5V$
Supply Voltage (Loudspeaker V_{DD})	$2.7V \le V_{DD} \le 5.5V$

Electrical Characteristics 3.3V (Notes 2, 7)

The following encodifications exply for $V = 0.0V = 0.000$	and all value are act for AdD unloss athematics are sified
The following specifications apply for $V_{DD} = 3.3V$, $T_A = 25^{\circ}C$,	and all dains are sel for UdB unless otherwise specified.
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Symbol	Parameter Conditions L				Units
			Typical (Note 4)	Limits (Note 5)	(Limits)
		Output Modes 2, 4, 6 $V_{IN} = 0V$; No load, OCL = 0 (Table 2)	4.5	6.5	mA (max)
I _{DDQ}	Quiescent Supply Current	Output Modes 1, 3, 5, 7 $V_{IN} = 0V$; No load, BTL, OCL = 0 (Table 2)	6.5	8	mA (max)
I _{SD}	Shutdown Current	Output Mode 0	0.1	1	μA (max)
		V _{IN} = 0V, Mode 7, Mono	2	15	
Vos	Output Offset Voltage	V _{IN} = 0V, Mode 7, Headphones	2	15	mV (max)
D	Output Dawar	$\label{eq:MONO_OUT} \begin{array}{l} \mbox{MONO}_{OUT}; \ \mbox{R}_L = 8\Omega \\ \mbox{THD+N} = 1\%; \ \mbox{f} = 1 \mbox{KHz}, \ \mbox{BTL}, \ \mbox{Mode} \ \ 1 \end{array}$	500	400	mW (min)
Po	Output Power	R_{OUT} and L_{OUT} ; $R_L = 32\Omega$ THD+N = 1%; f = 1kHz, SE, Mode 4	37	33	mW (min)
THD+N	Total Harmonic Distortion Plus Noise	$MONO_{OUT}$ f = 1kHz, P _{OUT} = 250mW; R _L = 8Ω, BTL, Mode 1	0.03		%
		R_{OUT} and L_{OUT} f = 1kHz, P_{OUT} = 12mW; R_{L} = 32 Ω , SE, Mode 4	0.02		%
		A-weighted, 0dB inputs terminated, output referred			
		Speaker; Mode 1	39		μV
		Speaker; Mode 3	39		μV
		Speaker; Mode 5	42		μV
N _{OUT}	Output Noise	Speaker; Mode 7	38		μV
	Output Noise	Headphone; SE, Mode 2	15		μV
		Headphone; SE, Mode 4	15		μV
		Headphone; SE, Mode 6	17		μV
		Headphone; OCL, Mode 2	12		μV
		Headphone; OCL, Mode 4	15		μV
		Headphone; OCL, Mode 6	17		μV

Symbol	Parameter	Conditions	LM4	1947	ecified. Units
			Typical (Note 4)	Limits (Note 5)	(Limits)
	Power Supply Rejection Ratio	$\label{eq:V_RIPPLE} \begin{array}{l} V_{RIPPLE} = 200 \text{mV}_{PP} \text{; } \text{f} = 217 \text{Hz}, \\ R_{L} = 8\Omega, \ C_{B} = 2.2 \mu \text{F}, \ BTL \\ \text{All audio inputs terminated to GND;} \\ \text{output referred} \end{array}$			
	Loudspeaker out	BTL, Output Mode 1	79		dB
		BTL, Output Mode 3	78		dB
		BTL, Output Mode 5	79		dB
		BTL, Output Mode 7	80		dB
PSRR	Power Supply Rejection Ratio R _{OUT} and L _{OUT}	$V_{\text{RIPPLE}} = 200 \text{mV}_{\text{PP}}; \text{ f} = 217 \text{Hz},$ $R_{\text{L}} = 32\Omega, C_{\text{B}} = 2.2 \mu\text{F}, \text{ BTL}$ All audio inputs terminated to GND; output referred			
		SE, Output Mode 2	78		dB
		SE, Output Mode 4	71		dB
		SE, Output Mode 6	71		dB
		OCL, Output Mode 2	83		dB
		OCL, Output Mode 4	74		dB
		OCL, Output Mode 6	74		dB
η	Class D Efficiency	Output Mode 1, 3, 5	86		%
CMRR	Common-Mode-Rejection Ratio	f = 217Hz, V_{CM} = 1Vpp, Mode 1, BTL, R_L = 8Ω	-49		dB
XTALK	Crosstalk	Headphone, $P_O = 12mW$, f = 1kHz, OCL, Mode 4, $R_L = 32\Omega$	-58		dB
		Headphone, $P_O = 12mW$, f = 1kHz, SE, Mode 4, $R_L = 32\Omega$	-73		
Twu	Wake-Up Time from Shutdown	$C_B = 2.2\mu F$, OCL, $R_L = 32\Omega$	90		ms
·wu		$C_B = 2.2 \mu F$, SE, $R_L = 32 \Omega$	115		1113
	Volume Control Step Size Error		±0.2		dB
		Input referred maximum attenuation	-59.5	-60.25 -58.75	dB (min) dB (max
	Digital Volume Range	Input referred maximum gain	+18	17.25 18.75	dB (min) dB (max
	Mute Attenuation	Output Mode 1, 3, 5	87		dB
	MONO_IN Input Impedance	Maximum gain setting	12	8 14	kΩ (min kΩ (max
	R_{IN} and L_{IN} Input Impedance	Maximum attenuation setting	100	75 125	kΩ (min) kΩ (max

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Electrical Characteristics 5V (Notes 2, 7) The following specifications apply for $V_{DD} = 5V$, $T_A = 25^{\circ}C$ and all gains are set for 0dB unless otherwise specified.

Symbol	Parameter Conditions		LM4	LM4947	
			Typical (Note 4)	Limits (Note 5)	(Limits)
1	Quiescent Supply Quirant	Output Modes 2, 4, 6 V _{IN} = 0V; No load, OCL = 0 (Table 2)	5.4	7.5	mA
I _{DDQ}	Quiescent Supply Current	Output Modes 1, 3, 5, 7 $V_{IN} = 0V$; No load, BTL, OCL = 0 (Table 2)	7.6	12	mA
I _{SD}	Shutdown Current	Output Mode 0	0.1	1	μA (max)
Vos	Output Offset Voltage	V _{IN} = 0V, Mode 7, Mono	2	15	mV (max)
VOS		$V_{IN} = 0V$, Mode 7, Headphones	2	15	inv (max)
D. Outrat Dawn		$\label{eq:mono_out} \begin{array}{l} MONO_{OUT}; \ R_L = 8\Omega \\ THD+N = 1\%; \ f = 1kHz, \ BTL, \ Mode \ 1 \end{array}$	1.19		W
Po	Output Power	R_{OUT} and L_{OUT} ; $R_L = 32\Omega$ THD+N = 1%; f = 1kHz, SE, Mode 4	87		mW
THD+N	Total Harmonic Distortion + Noise	$ \begin{array}{l} MONO_{OUT} \\ f = 1kHz, \ P_{OUT} = 500mW; \\ R_L = 8\Omega, \ BTL, \ Mode \ 1 \end{array} $	0.04		%
		R_{OUT} and L_{OUT} f = 1kHz, P_{OUT} = 30mW; R_L = 32 Ω , SE, Mode 4	0.01		%
		A-weighted, 0dB			
		inputs terminated, output referred			
		Speaker; Mode 1	38		· · · ·
		Speaker; Mode 3	38		
		Speaker; Mode 5	39		
N _{OUT}	Output Noise	Speaker; Mode 7	36		
		Headphone; SE, Mode 2	21		
		Headphone; SE, Mode 4	21		μV
		Headphone; SE, Mode 6	24		μV
		Headphone; OCL, Mode 2	16		μV
		Headphone; OCL, Mode 4	16		μV
		Headphone; OCL, Mode 6	19		μV

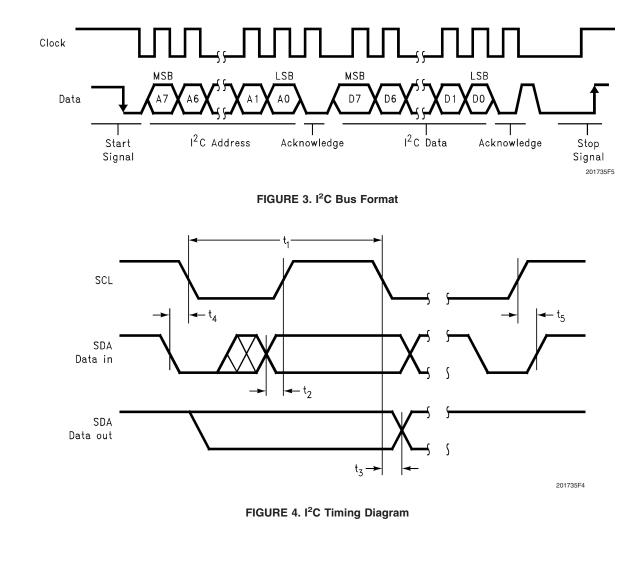
Symbol	Parameter	Conditions	LM4	1947	Units	
			Typical (Note 4)	Limits (Note 5)	(Limits)	
	Power Supply Rejection Ratio	$\label{eq:V_RIPPLE} \begin{array}{l} V_{RIPPLE} = 200 \text{m}V_{PP}; \ f = 217 \text{Hz}, \\ R_L = 8\Omega, \ C_B = 2.2 \mu \text{F}, \ BTL \\ \text{All audio inputs terminated to GND;} \\ \text{output referred} \end{array}$				
	Loudspeaker out	BTL, Output Mode 1	70		dB	
		BTL, Output Mode 3	61		dB	
		BTL, Output Mode 5	64		dB	
		BTL, Output Mode 7	61		dB	
PSRR	Power Supply Rejection Ratio R_{OUT} and L_{OUT}	$\label{eq:relation} \begin{array}{l} V_{\text{RIPPLE}} = 200 \text{mV}_{\text{PP}}; \ \text{f} = 217 \text{Hz}, \\ \text{R}_{\text{L}} = 32 \Omega, \ \text{C}_{\text{B}} = 2.2 \mu \text{F}, \ \text{BTL} \\ \text{All audio inputs terminated to GND;} \\ \text{output referred} \end{array}$				
		SE, Output Mode 2	72		dB	
		SE, Output Mode 4	70		dB	
		SE, Output Mode 6	65		dB	
		OCL, Output Mode 2	76		dB	
		OCL, Output Mode 4	72		dB	
		OCL, Output Mode 6	70		dB	
η	Class D Efficiency	Output Mode 1, 3, 5	86		%	
CMRR	Common-Mode Rejection Ratio	f = 1kHz, V _{CM} = 1Vpp, 0dB gain, Mode 1, BTL, R _L = 8Ω	-49		dB	
VTALV	Croootalk	Headphone, $P_O = 30$ mW, f = 1kHz, OCL, Mode 4	-55		dD	
XTALK	Crosstalk	Headphone, $P_O = 30$ mW, f = 1kHz, SE, Mode 4	-72		dB	
 т		$C_B = 2.2\mu$ F, OCL, $R_L = 32\Omega$	116		ms	
T _{WU}	Wake-Up Time from Shutdown	$C_B = 2.2\mu$ F, SE, $R_L = 32\Omega$	150			
	Volume Control Step Size Error		±0.2		dB	
	Digital Volume Penge	Input referred maximum attenuation	-59.5		dB	
	Digital Volume Range	Input referred maximum gain +18			dB	
	Mute Attenuation	Output Mode 1, 3, 5	90		dB	
	MONO_IN Input Impedance	Maximum gain setting	11		kΩ	
	R _{IN} and L _{IN} Input Impedance	Maximum attenuation setting	100		kΩ	

LM4947 **I²C** (Notes 2, 7) The following specifications apply for V_{DD} = 5V and 3.3V, T_A = 25 $^\circ\text{C}$ unless otherwise specified. Symbol Conditions LM4947 Parameter Units (Limits) Typical Limits (Note 4) (Note 5) **Clock Period** t₁ 2.5 µs (max) Clock Setup Time 100 ns (min) t₂ Data Hold Time 100 ns (min) t₃ Start Condition Time 100 ns (min) t_4 Stop Condition Time 100 t₅ ns (min) 0.7xl²C VIH SPI Input Voltage High V (min) V_{DD} 0.3xl²C VIL SPI Input Voltage Low V (max) V_{DD}

I²C Protocol Information

The I²C address for the LM4947 is determined using the ID_ENB pin. The LM4947's two possible I²C chip addresses are of the form $111110X_10$ (binary), where $X_1 = 0$, if

ID_ADDR is logic LOW; and $X_1 = 1$, if ID_ENB is logic HIGH. If the I²C interface is used to address a number of chips in a system, the LM4947's chip address can be changed to avoid any possible address conflicts.



Note 1: See AN-450 "Surface Mounting and their effects on Product Reliability" for other methods of soldering surface mount devices.

Note 2: Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

Note 3: Human body model, 100pF discharged through a 1.5k Ω resistor.

Note 4: Typical specifications are specified at +25°C and represent the most likely parametric norm.

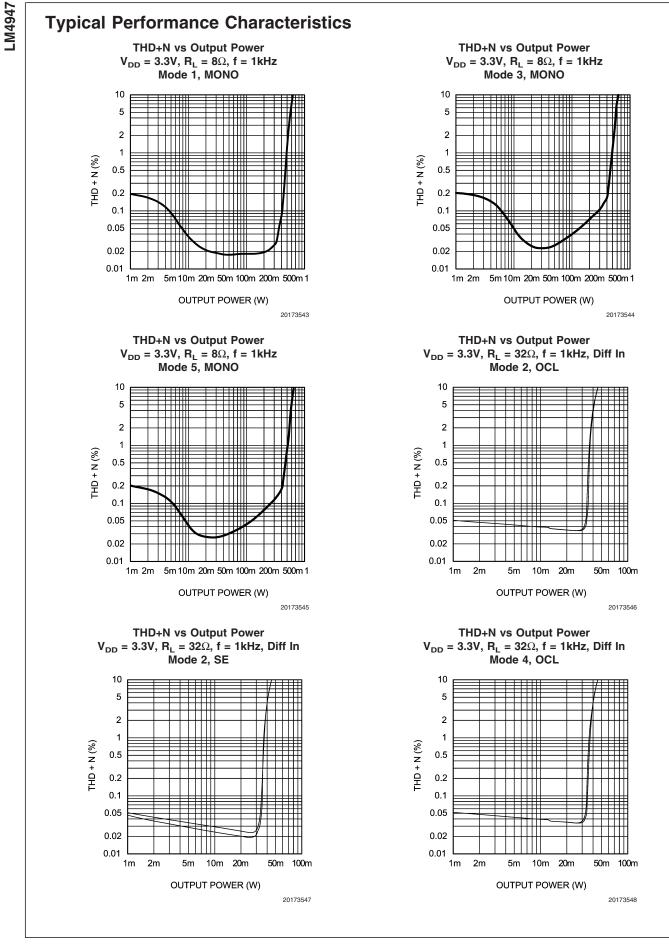
Note 5: Tested limits are guaranteed to National's AOQL (Average Outgoing Quality Level).

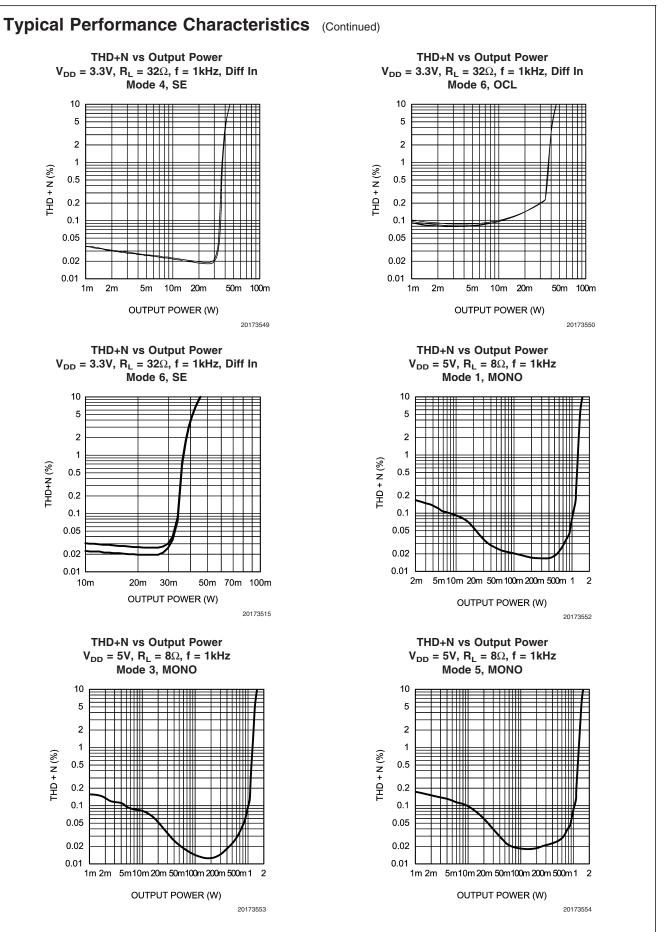
Note 6: Machine Model ESD test is covered by specification EIAJ IC-121-1981. A 200pF cap is charged to the specified voltage, then discharged directly into the IC with no external series resistor (resistance of discharge path must be under 50Ω).

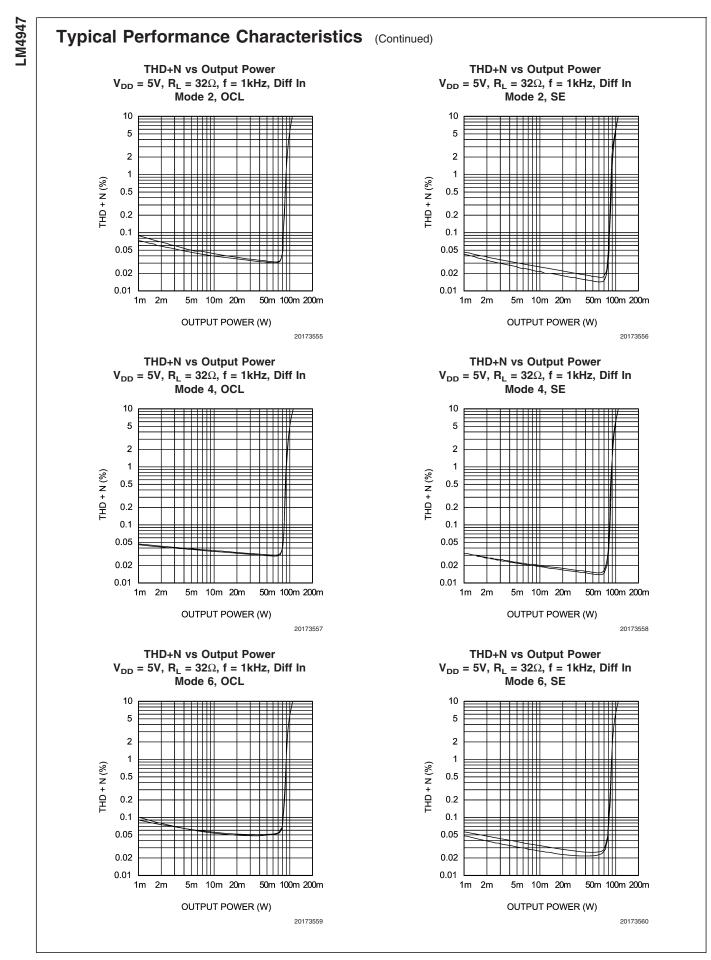
Note 7: All voltages are measured with respect to the ground pin, unless otherwise specified.

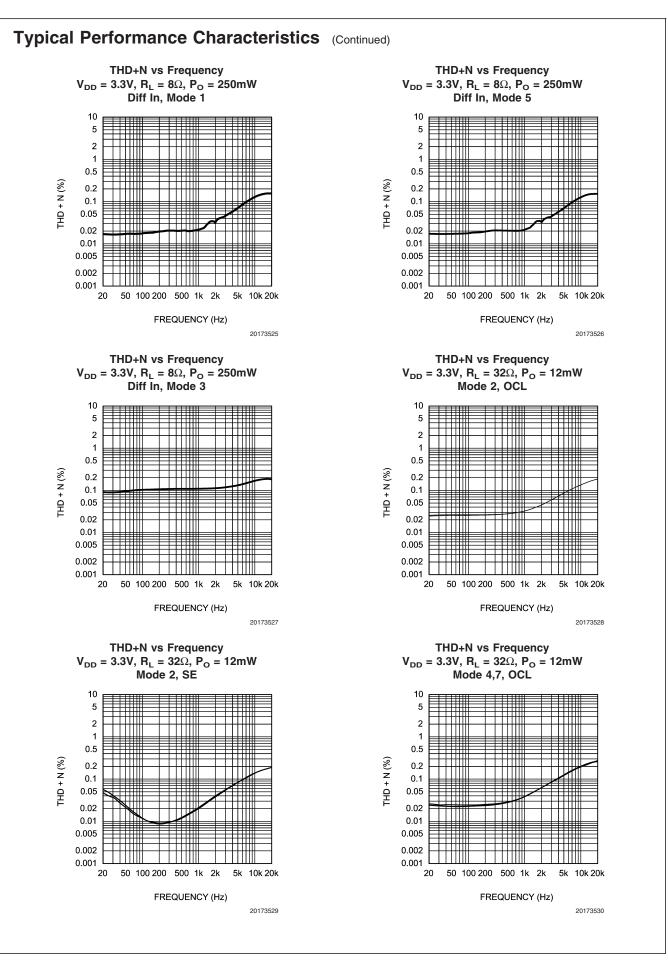
Note 8: The given θ_{JA} for an LM4947TL mounted on a demonstration board with a 9in² area of 1oz printed circuit board copper ground plane.

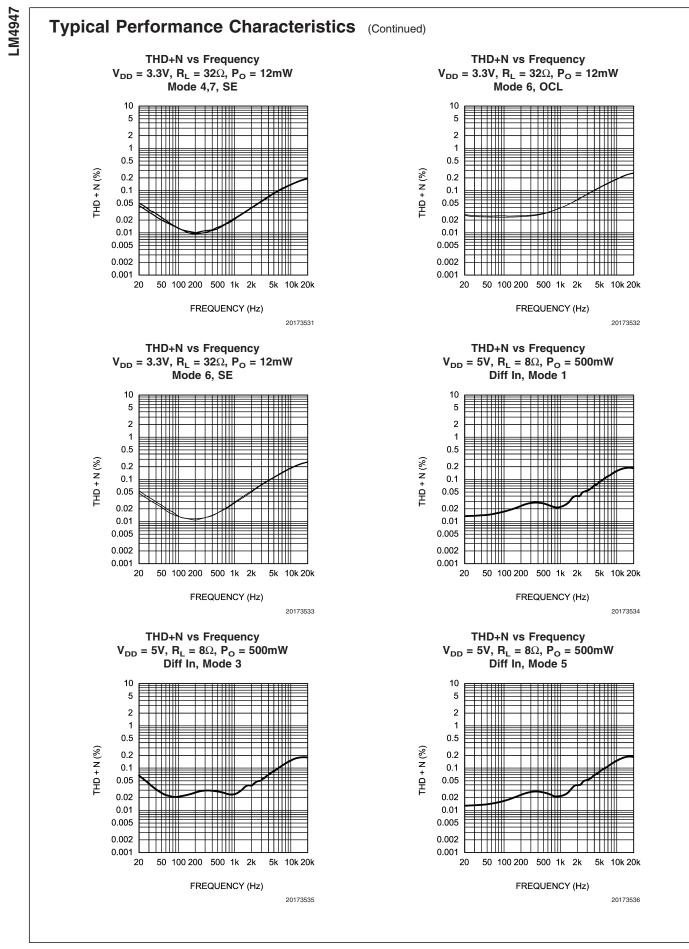
Note 9: Datasheet min/max specifications are guaranteed by design, test, or statistical analysis.

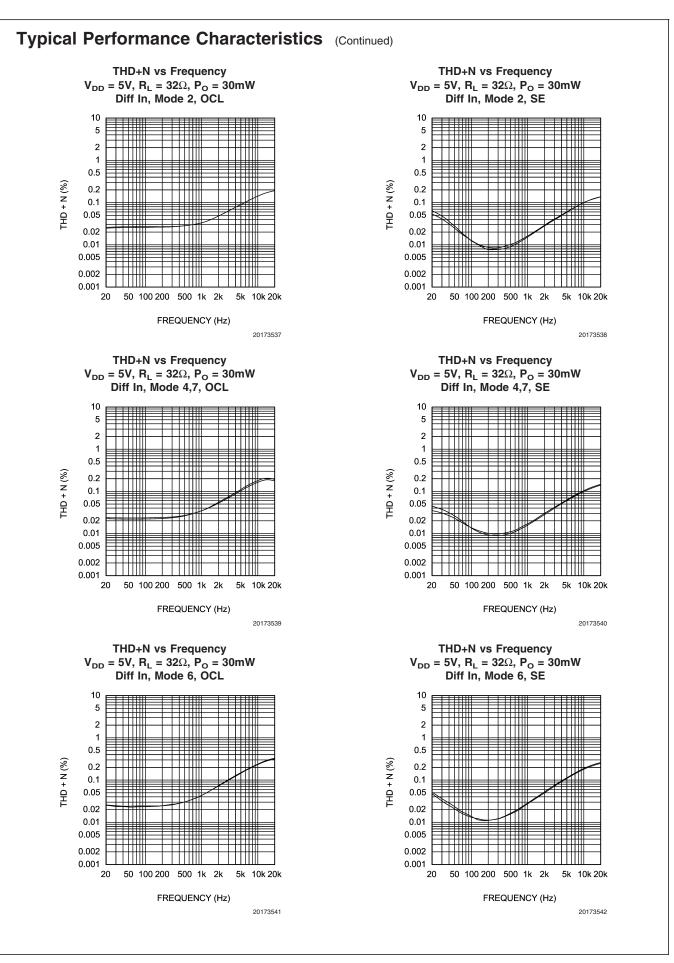


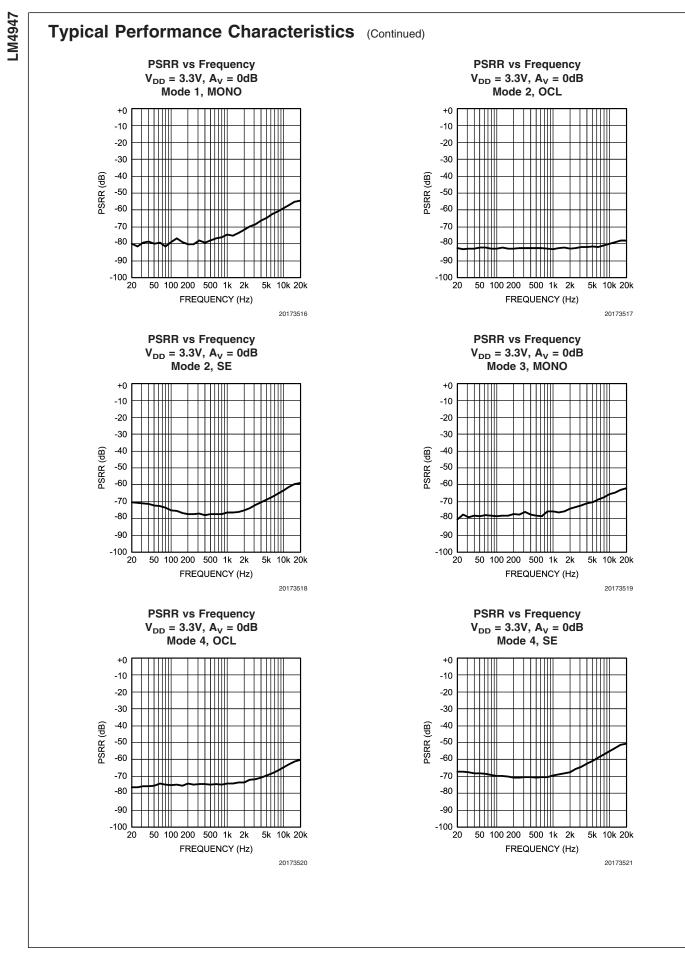


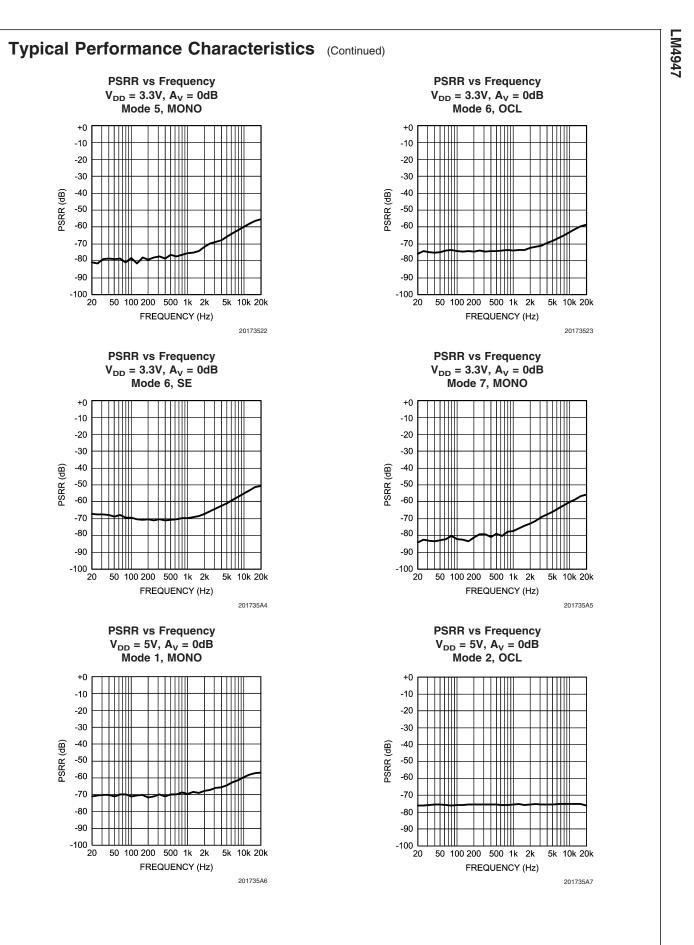


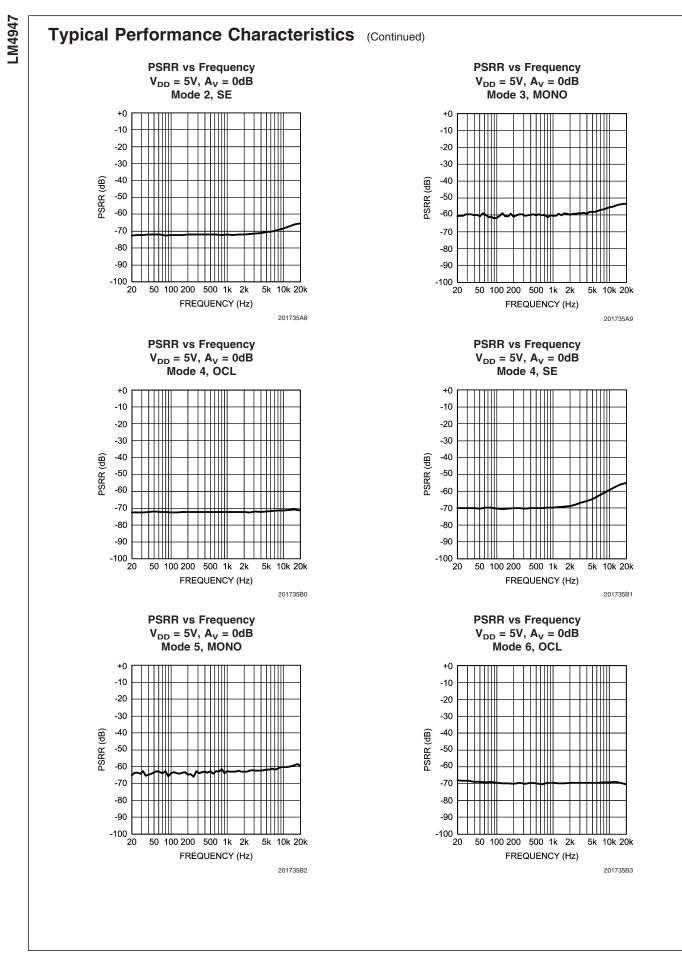


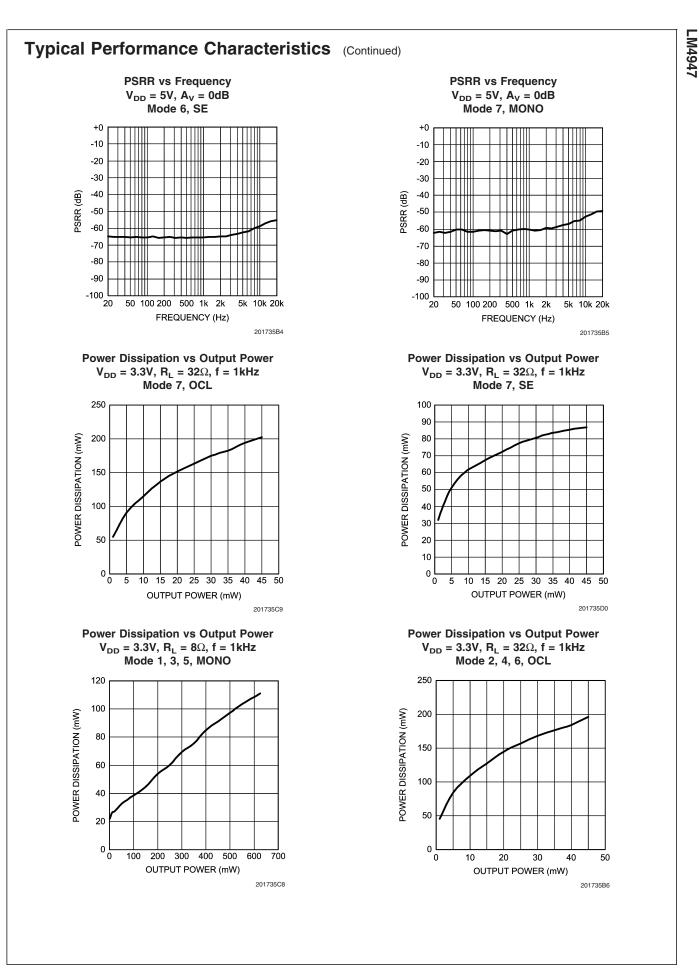




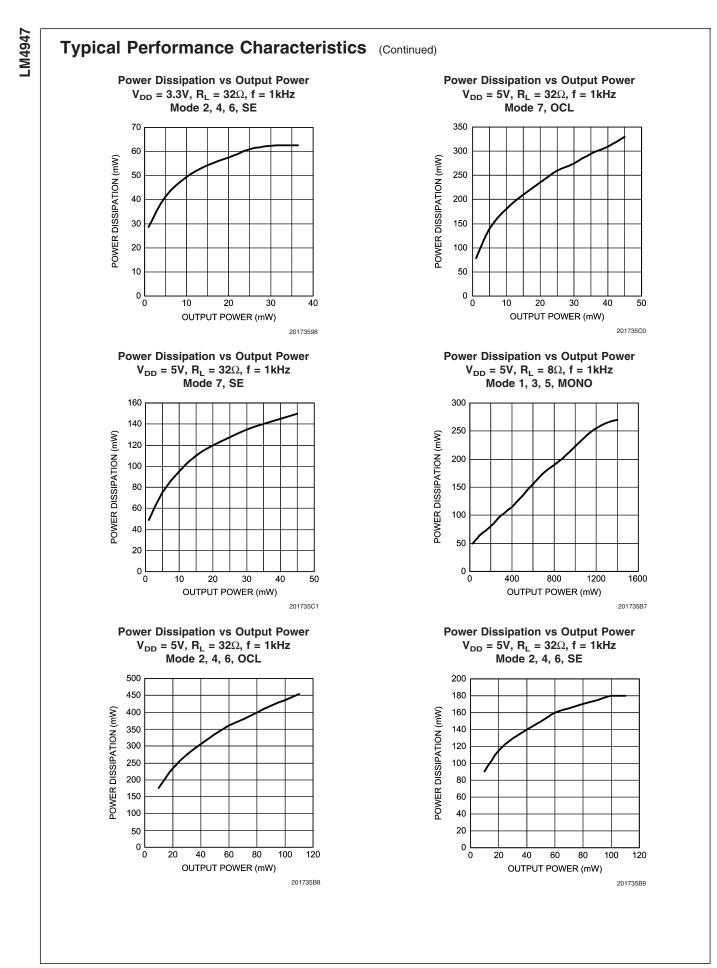


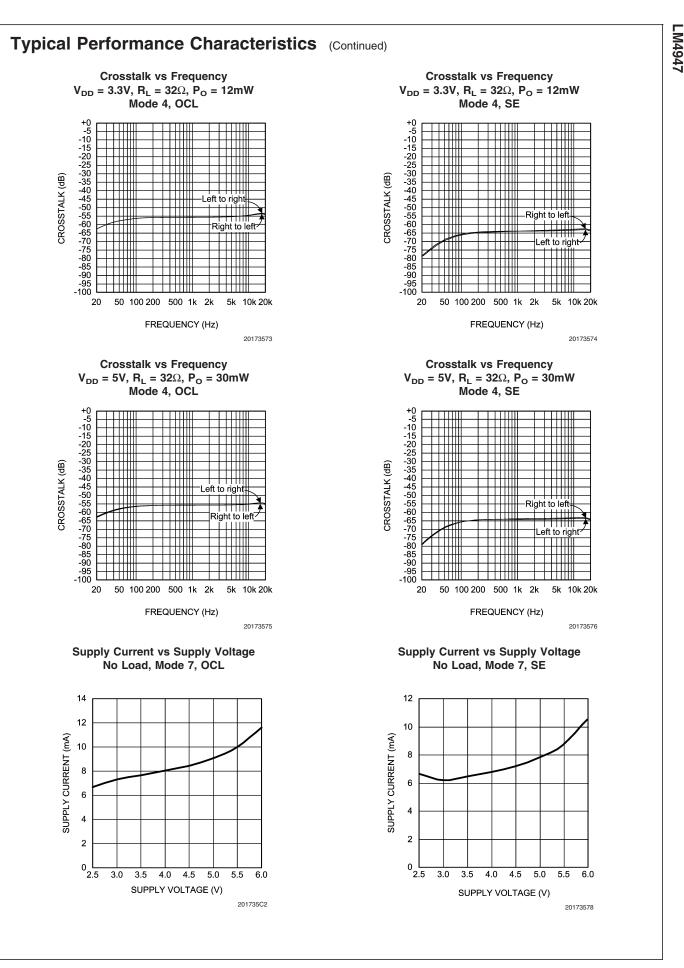


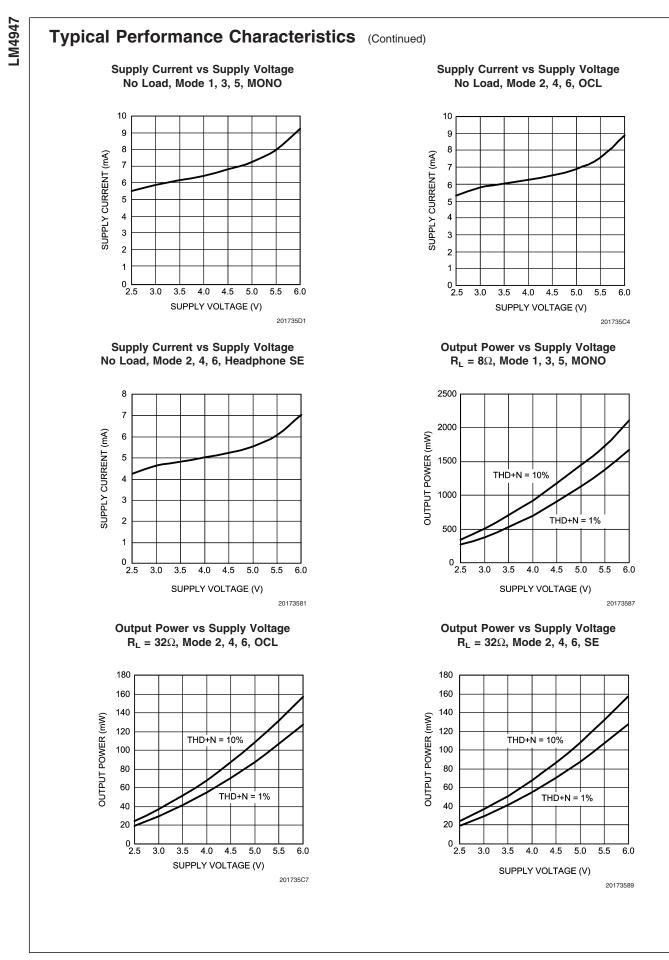


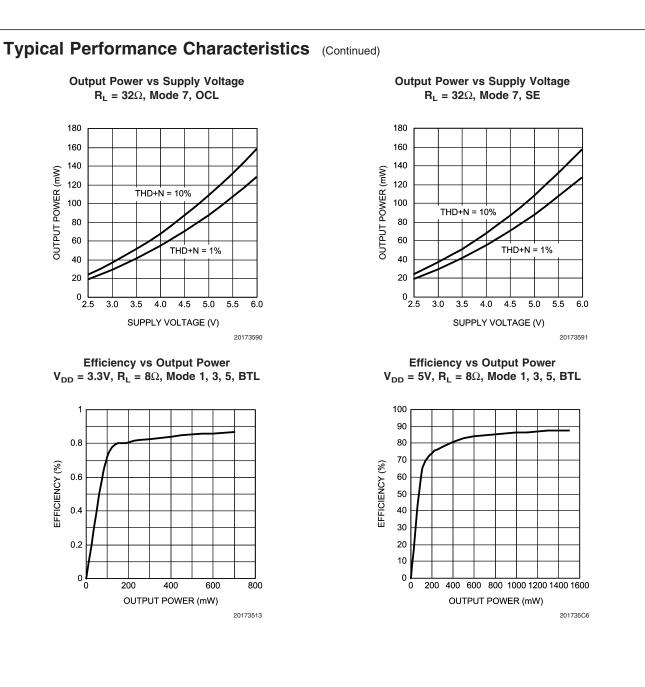


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Application Information

I²C PIN DESCRIPTION

SDA: This is the serial data input pin.

SCL: This is the clock input pin.

ID_ENB: This is the address select input pin.

I²C COMPATIBLE INTERFACE

The LM4947 uses a serial bus which conforms to the I^2C protocol to control the chip's functions with two wires: clock (SCL) and data (SDA). The clock line is uni-directional. The data line is bi-directional (open-collector). The maximum clock frequency specified by the I^2C standard is 400kHz. In this discussion, the master is the controlling microcontroller and the slave is the LM4947.

The I²C address for the LM4947 is determined using the ID_ENB pin. The LM4947's two possible I²C chip addresses are of the form 111110X₁0 (binary), where X₁ = 0, if ID_ADDR is logic LOW; and X₁ = 1, if ID_ENB is logic HIGH. If the I²C interface is used to address a number of chips in a system, the LM4947's chip address can be changed to avoid any possible address conflicts.

The bus format for the I²C interface is shown in Figure 3. The bus format diagram is broken up into six major sections:

The "start" signal is generated by lowering the data signal while the clock signal is HIGH. The start signal will alert all devices attached to the I^2C bus to check the incoming address against their own address.

The 8-bit chip address is sent next, most significant bit first. The data is latched in on the rising edge of the clock. Each address bit must be stable while the clock level is HIGH. After the last bit of the address bit is sent, the master releases the data line HIGH (through a pull-up resistor). Then the master sends an acknowledge clock pulse. If the LM4947 has received the address correctly, then it holds the data line LOW during the clock pulse. If the data line is not held LOW during the acknowledge clock pulse, then the master should abort the rest of the data transfer to the LM4947.

The 8 bits of data are sent next, most significant bit first. Each data bit should be valid while the clock level is stable HIGH.

After the data byte is sent, the master must check for another acknowledge to see if the LM4947 received the data.

The "stop" signal ends the transfer. To signal "stop", the data signal goes HIGH while the clock signal is HIGH. The data line should be held HIGH when not in use.

I²C INTERFACE POWER SUPPLY PIN (I²CV_{DD})

The LM4947's I²C interface is powered up through the I²CV_{DD} pin. The LM4947's I²C interface operates at a voltage level set by the I²CV_{DD} pin which can be set independent to that of the main power supply pin V_{DD}. This is ideal whenever logic levels for the I²C interface are dictated by a microcontroller or microprocessor that is operating at a lower supply voltage than the main battery of a portable system.

	TABLE	1.	Chip	Addre	ss
--	-------	----	------	-------	----

	A7	A6	A5	A4	A3	A2	A1	A0
Chip Address	1	1	1	1	1	0	EC	0
ID_ADDR = 0	1	1	1	1	1	0	0	0
ID_ADDR = 1	1	1	1	1	1	0	1	0

TABLE 2. Control Registers

	D7	D6	D5	D4	D3	D2	D1	D0
Mode Control	0	0	SE/Diff	0	OCL (select)	MC2	MC1	MC0
			(select)					
Programmable 3D	0	1	L2R2	L1R1	N3D3	N3D2	N3D1	N3D0
			(select)	(select)				
Mono Volume	1	0	0	MVC4	MVC3	MVC2	MVC1	MVC0
Control								
Left Volume Control	1	1	0	LVC4	LVC3	LVC2	LVC1	LVC0
Right Volume	1	1	1	RVC4	RVC3	RVC2	RVC1	RVC0
Control								

1. Bits MVC0 — MVC4 control 32 step volume control for MONO input

2. Bits LVC0 — LVC4 control 32 step volume control for LEFT input

3. Bits RVC0 — RVC4 control 32 step volume control for RIGHT input

4. Bits MC0 — MC2 control 8 distinct modes

5. Bits N3D3, N3D2, N3D1, N3D0 control programmable 3D function

6. N3D0 turns the 3D function ON (N3D0 = 1) or OFF (N3D0 = 0)

7. Bit OCL selects between SE with output capacitor (OCL = 0) or SE without output capacitors (OCL = 1). Default is OCL = 0

8. N3D1 selects between two different 3D configurations

9. SE/Diff-SE/Diff = 0 for SE mode; SE/Diff = 1 for Diff mode

Application Information (Continued)

TABLE 3. Programmable National 3D Audio

	N3D3	N3D2
Low	0	0
Medium	0	1
High	1	0
Maximum	1	1

TABLE 4. Input/Output Control

	L1R1	L2R2	SE/DIFF
Select LIN1 and RIN1 Stereo Pair	1	0	0
Select L_{IN2} and R_{IN2} Stereo Pair	0	1	0
Select $L_{\text{IN1}} + L_{\text{IN2}}$ and $R_{\text{IN1}} + R_{\text{IN2}}$ Stereo Pair	1	1	0
Sets Stereo Inputs to Differential	Х	х	1
V David Oans			

X = Don't Care

Application Information (Continued)

TABLE 5. Output Volume Control Table

Volume Step	xVC4	xVC3	xVC2	xVC1	xVC0	Gain, dB
1	0	0	0	0	0	-59.50
2	0	0	0	0	1	-48.00
3	0	0	0	1	0	-40.50
4	0	0	0	1	1	-34.50
5	0	0	1	0	0	-30.00
6	0	0	1	0	1	-27.00
7	0	0	1	1	0	-24.00
8	0	0	1	1	1	-21.00
9	0	1	0	0	0	-18.00
10	0	1	0	0	1	-15.00
11	0	1	0	1	0	-13.50
12	0	1	0	1	1	-12.00
13	0	1	1	0	0	-10.50
14	0	1	1	0	1	-9.00
15	0	1	1	1	0	-7.50
16	0	1	1	1	1	-6.00
17	1	0	0	0	0	-4.50
18	1	0	0	0	1	-3.00
19	1	0	0	1	0	-1.50
20	1	0	0	1	1	0.00
21	1	0	1	0	0	1.50
22	1	0	1	0	1	3.00
23	1	0	1	1	0	4.50
24	1	0	1	1	1	6.00
25	1	1	0	0	0	7.50
26	1	1	0	0	1	9.00
27	1	1	0	1	0	10.50
28	1	1	0	1	1	12.00
29	1	1	1	0	0	13.50
30	1	1	1	0	1	15.00
31	1	1	1	1	0	16.50
32	1	1	1	1	1	18.00

1. x = M, L, or R

TABLE 6. Output Mode Selection									
Output Mode Number	MC2	MC1	MC0	Handsfree Mono Output	Right HP Output	Left HP Output			
0	0	0	0	SD	SD	SD			
1	0	0	1	2 x G _M x M	MUTE	MUTE			
2	0	1	0	SD	G _M x M	G _м х М			
3	0	1	1	G _L x L + G _R x R	MUTE	MUTE			
4	1	0	0	SD	G _R x R	G _L x L			
5	1	0	1	$\begin{array}{c} G_{L} \times L + G_{R} \times R + 2(G_{M} \times M) \\ \end{array}$	MUTE	MUTE			
6	1	1	0	SD	G _R x R + G _M x M	G _L x L + G _M x M			
7	1	1	1	G _B x R + G _I x L	G _R x R	G _I x L			

Note: L and R are selected by modes from Table 4. On initial POWER ON, the default mode is 000

M = Mono

 $R = R_{IN}$

 $L = L_{IN}$

SD = Shutdown

MUTE = Mute Mode

 G_M = Mono volume control gain

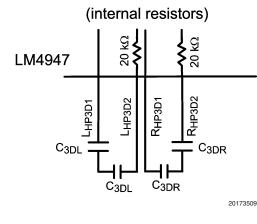
 $G_{\rm R}$ = Right stereo volume control gain

 G_L = Left stereo volume control gain

NATIONAL 3D ENHANCEMENT

The LM4947 features a stereo headphone, 3D audio enhancement effect that widens the perceived soundstage from a stereo audio signal. The 3D audio enhancement creates a perceived spatial effect optimized for stereo headphone listening. The LM4947 can be programmed for a "narrow" or "wide" soundstage perception. The narrow soundstage has a more focused approaching sound direction, while the wide soundstage has a spatial, theater-like effect. Within each of these two modes, four discrete levels of 3D effect that can be programmed: low, medium, high, and maximum (Table 2), each level with an ever increasing aural effect, respectively. The difference between each level is 3dB.

The external capacitors, shown in Figure 6, are required to enable the 3D effect. The value of the capacitors set the cutoff frequency of the 3D effect, as shown by Equations 1 and 2. Note that the internal $20k\Omega$ resistor is nominal (±25%).





$$f_{3DL(-3dB)} = 1 / 2\pi * 20k\Omega * C_{3DL}$$
 (1)

 $f_{3DR(-3dB)} = 1 / 2\pi * 20k\Omega * C_{3DR}$ (2)

Optional resistors R_{3DL} and R_{3DR} can also be added (Figure 7) to affect the -3dB frequency and 3D magnitude.

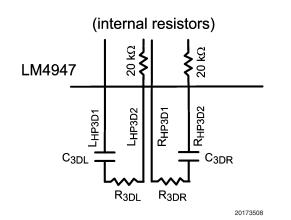


FIGURE 6. External RC Network with Optional $\rm R_{3DL}$ and $\rm R_{3DR}$ Resistors

 $f_{3DL(-3dB)} = 1 / 2\pi * (20k\Omega + R_{3DL}) * C_{3DL}$ (3)

$$f_{3DR(-3dB)} = 1 / 2\pi * 20k\Omega + R_{3DR}) * C_{3DR}$$
 (4)

Application Information (Continued)

 ΔAV (change in AC gain) = 1 / 1 + M, where M represents some ratio of the nominal internal resistor, $20k\Omega$ (see example below).

$$f_{3dB} (3D) = 1 / 2\pi (1 + M)(20k\Omega * C_{3D})$$
(5)

$$C_{Equivalent}$$
 (new) = C_{3D} / 1 + M (6)

TABLE 7. Pole Locations								
R _{3D} (kΩ) (optional)	C _{3D} (nF)	М	∆AV (dB)	f-3dB (3D) (Hz)	Value of C _{3D} to keep same pole location (nF)	new Pole Location (Hz)		
0	68	0	0	117				
1	68	0.05	-0.4	111	64.8	117		
5	68	0.25	-1.9	94	54.4	117		
10	68	0.50	-3.5	78	45.3	117		
20	68	1.00	-6.0	59	34.0	117		

PCB LAYOUT AND SUPPLY REGULATION CONSIDERATIONS FOR DRIVING 8Ω LOAD

Power dissipated by a load is a function of the voltage swing across the load and the load's impedance. As load impedance decreases, load dissipation becomes increasingly dependent on the interconnect (PCB trace and wire) resistance between the amplifier output pins and the load's connections. Residual trace resistance causes a voltage drop, which results in power dissipated in the trace and not in the load as desired. For example, 0.1Ω trace resistance reduces the output power dissipated by an 8Ω load from 158.3mW to 156.4mW. The problem of decreased load dissipation is exacerbated as load impedance decreases. Therefore, to maintain the highest load dissipation and widest output voltage swing, PCB traces that connect the output pins to a load must be as wide as possible.

Poor power supply regulation adversely affects maximum output power. A poorly regulated supply's output voltage decreases with increasing load current. Reduced supply voltage causes decreased headroom, output signal clipping, and reduced output power. Even with tightly regulated supplies, trace resistance creates the same effects as poor supply regulation. Therefore, making the power supply traces as wide as possible helps maintain full output voltage swing.

POWER DISSIPATION AND EFFICIENCY

In general terms, efficiency is considered to be the ratio of useful work output divided by the total energy required to produce it with the difference being the power dissipated, typically, in the IC. The key here is "useful" work. For audio systems, the energy delivered in the audible bands is considered useful including the distortion products of the input signal. Sub-sonic (DC) and super-sonic components (>22kHz) are not useful. The difference between the power flowing from the power supply and the audio band power being transduced is dissipated in the LM4947 and in the transducer load. The amount of power dissipation in the LM4947 is very low. This is because the ON resistance of the switches used to form the output waveforms is typically less than 0.25Ω . This leaves only the transducer load as a potential "sink" for the small excess of input power over audio band output power. The LM4947 dissipates only a fraction of the excess power requiring no additional PCB area or copper plane to act as a heat sink.

The LM4947 also has a pair of single-ended amplifiers driving stereo headphones, R_{HP} and L_{HP}. The maximum internal power dissipation for R_{HP} and L_{HP} is given by equation (9) and (10). From Equations (9) and (10), assuming a 5V power supply and a 32 Ω load, the maximum power dissipation for L_{HP} and R_{HP} is 40mW, or 80mW total.

 $P_{DMAX-LHP} = (V_{DD})^2 / (2\pi^2 R_L)$: Single-ended Mode (7)

 $P_{DMAX-RHP} = (V_{DD})^2 / (2\pi^2 R_L)$: Single-ended Mode (8)

The maximum internal power dissipation of the LM4947 occurs when all 3 amplifiers pairs are simultaneously on; and is given by Equation (11).

$$P_{DMAX-TOTAL} = P_{DMAX-SPKROUT} + P_{DMAX-LHP} + P_{DMAX-RHP}$$
(9)

The maximum power dissipation point given by Equation (11) must not exceed the power dissipation given by Equation (12):

$$P_{DMAX} = (T_{JMAX} - T_A) / \theta_{JA}$$
(10)

The LM4947's $T_{JMAX} = 150^{\circ}$ C. In the ITL package, the LM4947's θ_{JA} is 65°C/W. At any given ambient temperature T_A , use Equation (12) to find the maximum internal power dissipation supported by the IC packaging. Rearranging Equation (12) and substituting P_{DMAX} -TOTAL for P_{DMAX} ' results in Equation (13). This equation gives the maximum ambient temperature that still allows maximum stereo power dissipation without violating the LM4947's maximum junction temperature.

$$T_{A} = T_{JMAX} - P_{DMAX-TOTAL} \theta_{JA}$$
(11)

For a typical application with a 5V power supply and an 8Ω load, the maximum ambient temperature that allows maximum stereo power dissipation without exceeding the maximum junction temperature is approximately 104°C for the ITL package.

$$T_{JMAX} = P_{DMAX-TOTAL} \theta_{JA} + T_A$$
(12)

Equation (14) gives the maximum junction temperature $T_{\rm J}\text{-}$ MAX. If the result violates the LM4947's 150°C, reduce the

Application Information (Continued)

maximum junction temperature by reducing the power supply voltage or increasing the load resistance. Further allowance should be made for increased ambient temperatures.

The above examples assume that a device is a surface mount part operating around the maximum power dissipation point. Since internal power dissipation is a function of output power, higher ambient temperatures are allowed as output power or duty cycle decreases. If the result of Equation (11) is greater than that of Equation (12), then decrease the supply voltage, increase the load impedance, or reduce the ambient temperature. If these measures are insufficient, a heat sink can be added to reduce θ_{JA} . The heat sink can be created using additional copper area around the package, with connections to the ground pin(s), supply pin and amplifier output pins. External, solder attached SMT heatsinks such as the Thermalloy 7106D can also improve power dissipation. When adding a heat sink, the θ_{JA} is the sum of $\theta_{JC},\,\theta_{CS},$ and $\theta_{SA}.$ (θ_{JC} is the junction-to-case thermal impedance, θ_{CS} is the case-to-sink thermal impedance, and θ_{SA} is the sink-to-ambient thermal impedance). Refer to the Typical Performance Characteristics curves for power dissipation information at lower output power levels.

POWER SUPPLY BYPASSING

As with any power amplifier, proper supply bypassing is critical for low noise performance and high power supply rejection. Applications that employ a 5V regulator typically use a 1µF in parallel with a 0.1µF filter capacitors to stabilize the regulator's output, reduce noise on the supply line, and improve the supply's transient response. However, their presence does not eliminate the need for a local 1.1µF tantalum bypass capacitance connected between the LM4947's supply pins and ground. Keep the length of leads and traces that connect capacitors between the LM4947's power supply pin and ground as short as possible. Connecting a 2.2 μ F capacitor, C_B, between the BYPASS pin and ground improves the internal bias voltage's stability and improves the amplifier's PSRR. The PSRR improvements increase as the bypass pin capacitor value increases. Too large, however, increases turn-on time and can compromise the amplifier's click and pop performance. The selection of bypass capacitor values, especially C_B, depends on desired PSRR requirements, click and pop performance (as explained in the section, Proper Selection of External Components), system cost, and size constraints.

SELECTING EXTERNAL COMPONENTS

Input Capacitor Value Selection

Amplifying the lowest audio frequencies requires high value input coupling capacitor (C_i in Figures 1 & 2). A high value capacitor can be expensive and may compromise space efficiency in portable designs. In many cases, however, the speakers used in portable systems, whether internal or external, have little ability to reproduce signals below 150Hz. Applications using speakers with this limited frequency response reap little improvement by using large input capacitor.

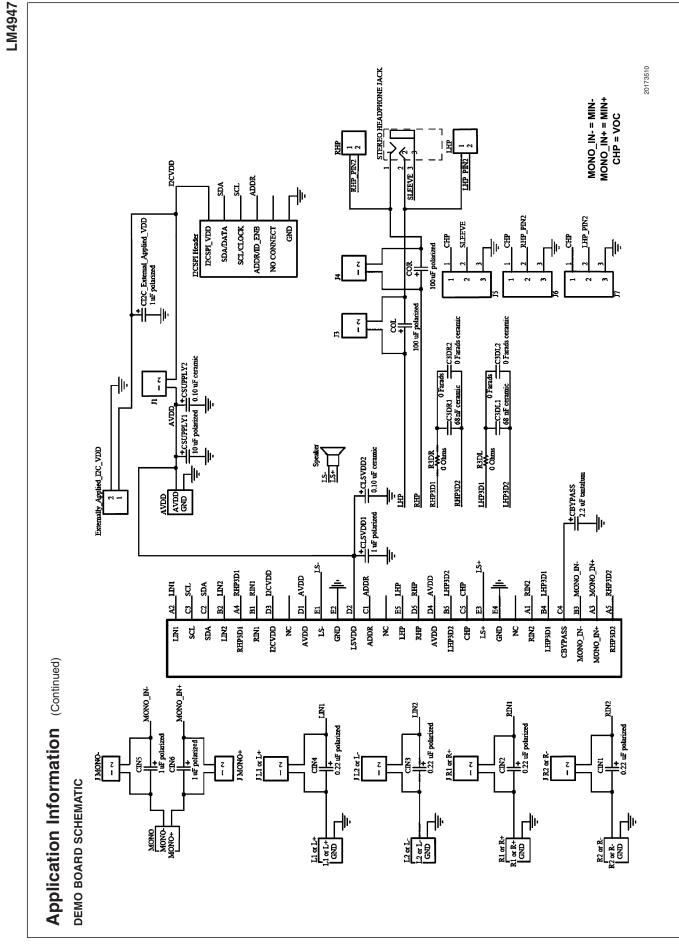
The internal input resistor (R_i), nominal 20k Ω , and the input capacitor (C_i) produce a high pass filter cutoff frequency that is found using Equation (15).

$$f_c = 1 / (2\pi R_i C_i)$$
 (13)

As an example when using a speaker with a low frequency limit of 150Hz, C_i, using Equation (15) is 0.053 μ F. The 0.22 μ F C_i shown in *Figure 1* allows the LM4947 to drive high efficiency, full range speaker whose response extends below 40Hz.

Bypass Capacitor Value Selection

Besides minimizing the input capacitor size, careful consideration should be paid to value of C_B , the capacitor connected to the BYPASS bump. Since C_B determines how fast the LM4947 settles to quiescent operation, its value is critical when minimizing turn-on pops. The slower the LM4947's outputs ramp to their quiescent DC voltage (nominally $V_{DD}/2$), the smaller the turn-on pop. Choosing C_B equal to 1.0µF along with a small value of C_i (in the range of 0.1µF to 0.39µF), produces a click-less and pop-less shutdown function. As discussed above, choosing C_i no larger than necessary for the desired bandwidth helps minimize clicks and pops. C_B 's value should be in the range of 5 times to 7 times the value of C_i . This ensures that output transients are eliminated when power is first applied or the LM4947 resumes operation after shutdown.



Revision Histor	У	
Rev	Date	Description
1.0	06/16/06	Initial release.
1.1	06/19/06	Changed the Class D Efficiency (n) on Typical limit (from 79 to 86) on the 5V specification table.
1.2	06/22/06	Added more Typ Perf curves.
1.3	07/18/06	Replaced some of the curves.
1.4	08/29/06	Text edits.
1.5	10/18/06	Edited micro SMD pkg drawing, Figure 1, and Figure 2. Changed I_{DDQ} typical and limit values on the 3.3V and 5.0V specification table. Removed CMRR SE condition and changed typical values for CMRR BTL on 3.3V and 5.0V specification table. Changed Mute Attenuation typical value on 5.0V specification table.

