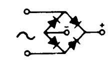
MOTOROLA

MDA2500 series

RECTIFIER ASSEMBLY

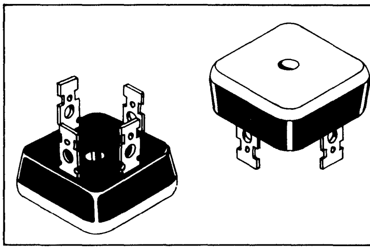
. . . utilizing individual void-free molded rectifiers, interconnected and mounted on an electrically isolated aluminum heat sink by a high thermal-conductive epoxy resin.

- 400 Ampere Surge Capability
- Electrically Isolated Base
- UL Recognized
- 1800 Volt Heat Sink Isolation



SINGLE-PHASE
FULL-WAVE BRIDGE

25 AMPERES
50-600 VOLTS



3

MAXIMUM RATINGS

Rating (Per Diode)	Symbol	MDA 2500	MDA 2501	MDA 2502	MDA 2504	MDA 2506	Unit
Peak Repetitive Reverse Voltage Working Peak Reverse Voltage DC Blocking Voltage	V_{RRM} V_{RWM} V_R	50	100	200	400	600	Volts
DC Output Voltage Resistive Load Capacitive Load	Vdc	 30 50	 62 100	 124 200	 250 400	 380 600	Volts
Sine Wave RMS Input Voltage	$V_{R(RMS)}$	35	70	140	280	420	Volts
Average Rectified Forward Current (Single phase bridge resistive load, 60 Hz, T_C = 55°C)	I_O	←	—	25	—	→	Amp
Nonrepetitive Peak Surge Current (Surge applied at rated load conditions)	I_{FSM}	←	—	400	—	→	Amp
Operating and Storage Junction Temperature Range	T_J, T_{stg}	←	—	−65 to +175	—	→	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Typ	Max	Unit
Thermal Resistance, Junction to Case Each Die Total Bridge	$R_{\theta JC}$	 8.0 2.0	 10 2.8	°C/W

ELECTRICAL CHARACTERISTICS (T_C = 25°C unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Instantaneous Forward Voltage (Per Diode) (i_F = 40 A)	v_F	—	0.95	1.05	Volts
Reverse Current (Per Diode) (Rated V_R)	I_R	—	—	0.10	mA

MECHANICAL CHARACTERISTICS

CASE: Plastic case with an electrically isolated aluminum base.

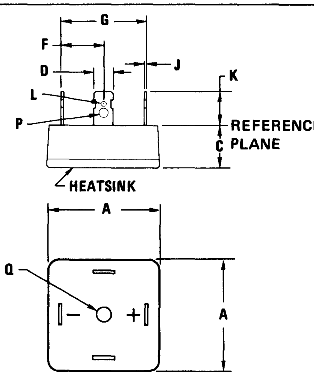
POLARITY: Terminal designation embossed on case:
+DC output
−DC output
AC not marked

MOUNTING POSITION: Bolt down. Highest heat transfer efficiency accomplished through the surface opposite the terminals. Use silicone heat sink compound on mounting surface for maximum heat transfer.

WEIGHT: 25 grams (approx.)

TERMINALS: Suitable for fast-on connections. Readily solderable, corrosion resistant. Soldering recommended for applications greater than 15 amperes.

MOUNTING TORQUE: 20 in. lb. max.



NOTES:
1. DIMENSION "Q" SHALL BE MEASURED ON HEATSINK SIDE OF PACKAGE.
2. DIMENSIONS "F" AND "G" SHALL BE MEASURED AT THE REFERENCE PLANE.

DIM	MILLIMETERS MIN	MILLIMETERS MAX	INCHES MIN	INCHES MAX
A	25.65	26.16	1.010	1.030
C	12.44	13.97	0.490	0.550
D	6.10	6.60	0.240	0.260
F	10.01	10.49	0.394	0.413
G	19.99	21.01	0.787	0.827
J	0.71	0.86	0.028	0.034
K	9.52	11.43	0.375	0.450
L	1.52	2.06	0.060	0.081
P	2.79	2.92	0.110	0.115
Q	4.42	4.67	0.174	0.184

CASE 309A-03

3

FIGURE 1 — FORWARD VOLTAGE

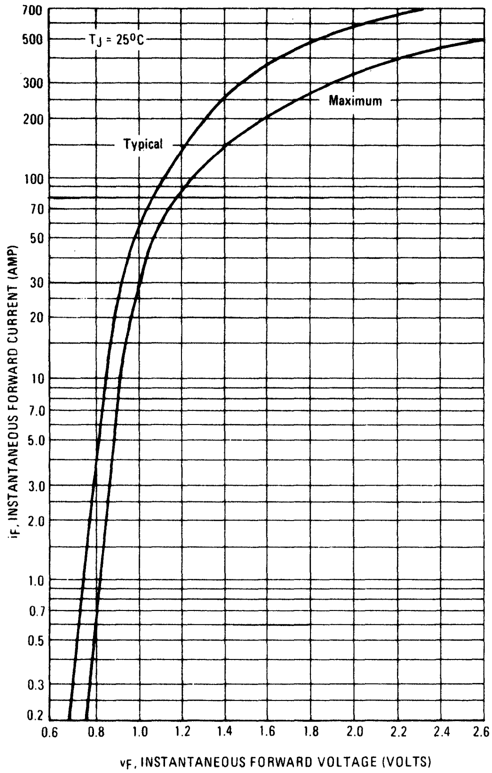


FIGURE 2 — NON REPETITIVE SURGE CURRENT

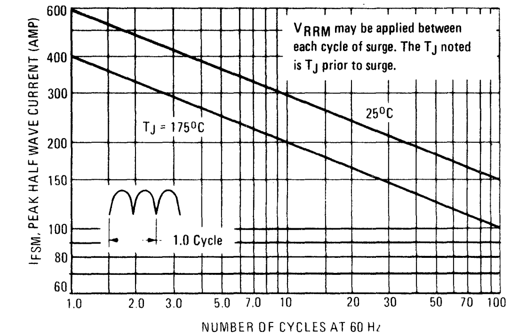


FIGURE 3 — FORWARD VOLTAGE TEMPERATURE COEFFICIENT

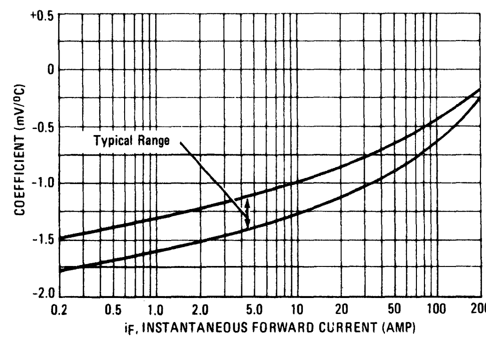


FIGURE 4 — CURRENT DERATING

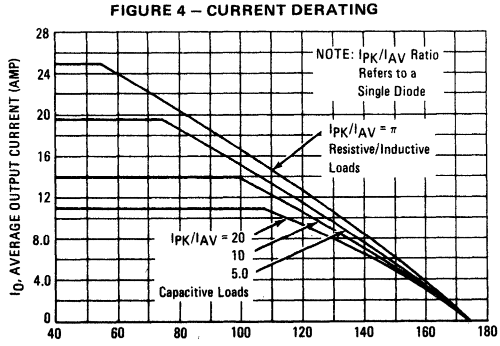


FIGURE 5 — FORWARD POWER DISSIPATION

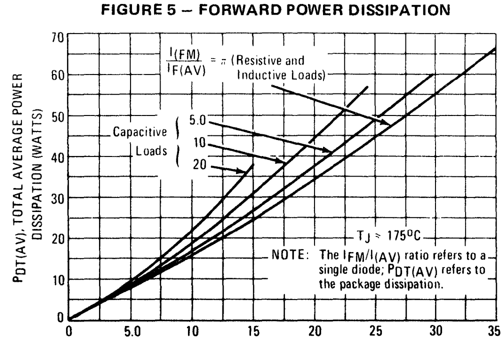
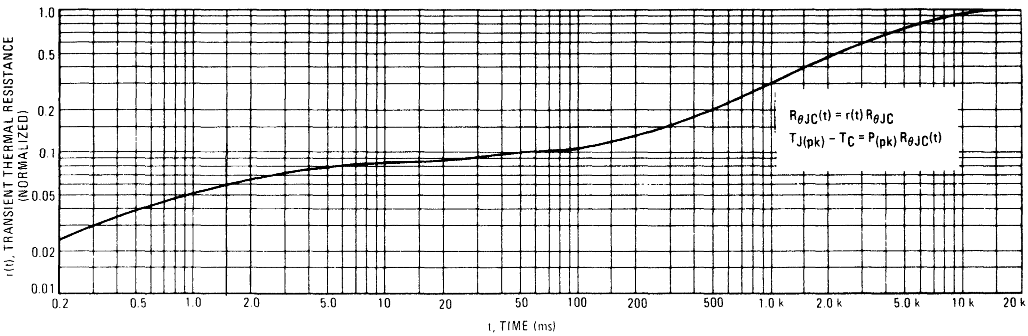
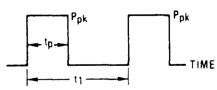


FIGURE 6 — TYPICAL THERMAL RESPONSE



NOTE 1



DUTY CYCLE, $D = t_p/t_1$
PEAK POWER, P_{pk}, is peak of an equivalent square power pulse

To determine maximum junction temperature of the diode in a given situation, the following procedure is recommended.

The temperature of the case should be measured using a thermocouple placed on the case at the temperature reference point (see the outline drawing on page 1). The thermal mass connected to the case is normally large enough so that it will not significantly respond to heat surges generated in the diode as a result of pulsed operation once steady state conditions are achieved. Using the measured value of T_C, the junction temperature may be determined by:

$$T_J = T_C + \Delta T_{JC}$$

where ΔT_{JC} is the increase in junction temperature above the case temperature. It may be determined by

$$\Delta T_{JC} = P_{pk} \bullet R_{\theta JC}\,[D + (1 - D) \bullet r(t_1 + t_p) + r(t_p) - r(t_1)]$$

where

$r(t)$ = normalized value of transient thermal resistance at time, t, from Figure 6, i.e.,

$r(t_1 + t_p)$ = normalized value of transient thermal resistance at time $t_1 + t_p$

FIGURE 7 — CAPACITANCE

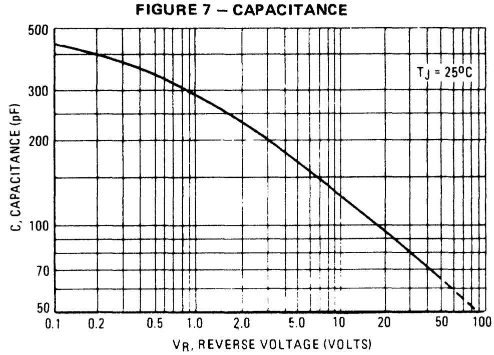


FIGURE 8 — FORWARD RECOVERY TIME

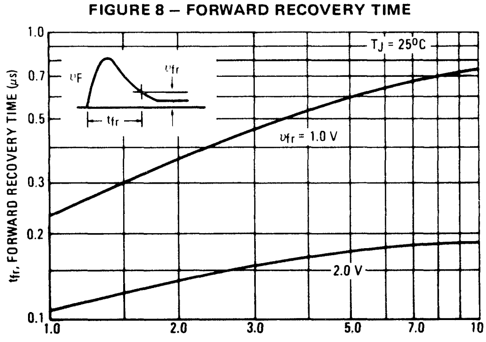
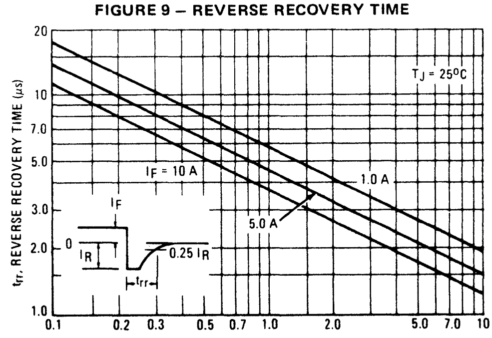


FIGURE 9 — REVERSE RECOVERY TIME



3

AMBIENT TEMPERATURE DERATING INFORMATION

FIGURE 10A — THERMALLOY HEAT SINK 6005B

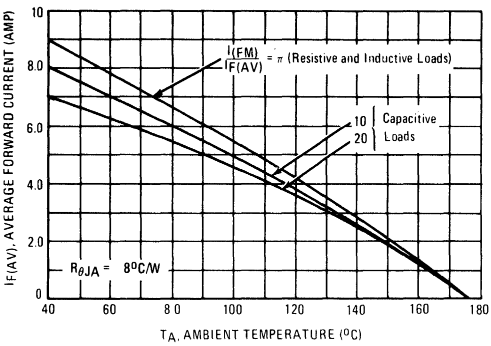
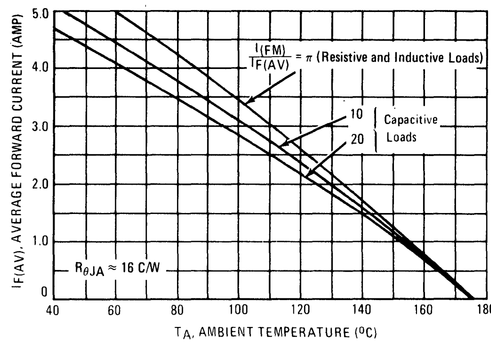


FIGURE 10B — IERC HEAT SINK UP3



NOTE 2: THERMAL COUPLING AND EFFECTIVE THERMAL RESISTANCE

In multiple chip devices where there is coupling of heat between die, the junction temperature can be calculated as follows:

(1) $\Delta T_{J1} = R_{\theta 1}P_{D1} + R_{\theta 2}K_{\theta 2}P_{D2} + R_{\theta 3}K_{\theta 3}P_{D3} + R_{\theta 4}K_{\theta 4}P_{D4}$

where ΔT_{J1} is the change in junction temperature of diode 1, $R_{\theta 1}$ through 4 is the thermal resistance of diodes 1 through 4, P_{D1} through 4 is the power dissipated in diodes 1 through 4, $K_{\theta 2}$ through 4 is the thermal coupling between diode 1, and diodes 2 through 4.

An effective package thermal resistance can be defined as follows:

(2) $R_{\theta(EFF)} = \Delta T_{J1}/P_{DT}$

where P_{DT} is the total package power dissipation.

Assuming equal thermal resistance for each die, equation (1) simplifies to

(3) $\Delta T_{J1} = R_{\theta 1}(P_{D1} + K_{\theta 2}P_{D2} + K_{\theta 3}P_{D3} + K_{\theta 4}P_{D4})$

For the conditions where $P_{D1} = P_{D2} = P_{D3} = P_{D4}$, P_{DT} = 4 P_{D1}, equation (3) can be further simplified and by substituting into equation (2) results in

(4) $R_{\theta(EFF)} = R_{\theta 1}(1 + K_{\theta 2} + K_{\theta 3} + K_{\theta 4})/4$

When the case is used as a reference point, coupling between opposite die is negligible for the MDA2500, and coupling between adjacent die is approximately 6%.

NOTE 3: SPLIT LOAD DERATING INFORMATION

Bridge rectifiers are used in two basic configurations as shown by circuits A and B of Figure 11. The current derating data of Figure 4 applies to the standard bridge circuit (A) where $I_A = I_B$. For circuit B where $I_A = I_B$, derating information can be calculated as follows:

(6) $T_{R(max)} = T_{J(max)} - \Delta T_{J1}$

Where $T_{R(max)}$ is the reference temperature (either case or ambient), ΔT_{J1} can be calculated using equation (3) in Note 2.

For example, to determine $T_{C(max)}$ for the MDA2500 with the following capacitive load conditions:

I_A = 20 A average with a peak of 60 A,
I_B = 10 A average with a peak of 70 A,

first calculate the peak to average ratio for I_A. $I_{(PK)}/I_{(AV)}$ = 60/10 = 6.0. (Note that the peak to average ratio is on a per diode basis and each diode provides 10 A average.)

From Figure 5, for an average current of 20 A and an $I_{(PK)}/I_{(AV)}$ = 6.0, read $P_{DT(AV)}$ = 40 watts or 10 watts/diode. Thus $P_{D1} = P_{D3}$ = 10 watts.

Similarly, for a load current I_B of 10 A, diode #2 and diode #4 each see 5.0 A average resulting in an $I_{(PK)}/I_{(AV)}$ = 14. Thus, the package power dissipation for 10 A is 20 watts or 5.0 watts/diode. Therefore, $P_{D2} = P_{D4}$ = 5.0 watts.

The maximum junction temperature occurs in diodes #1 and #3. From equation (3) for diode #1,

$$\Delta T_{J1} = 10[10 + 0(5) + 0.06(10) + 0.06(5)]$$
$$\Delta T_{J1} \approx 109^{\circ}C.$$

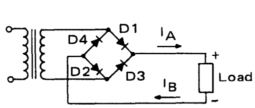
Thus, $T_{C(max)}$ = 175 − 109 = 66°C.

The total package dissipation in this example is

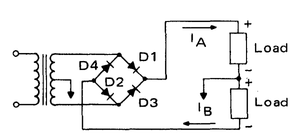
$$P_{DT(AV)} = 2 \times 10 + 2 \times 5.0 = 30 \text{ watts},$$

which must be considered when selecting a heat sink.

FIGURE 11 — BASIC CIRCUIT USES FOR BRIDGE RECTIFIERS



Circuit A



Circuit B