

2N5193 thru 2N5195/MJE5193 thru MJE5195 (continued)

FIGURE 1 – DC CURRENT GAIN

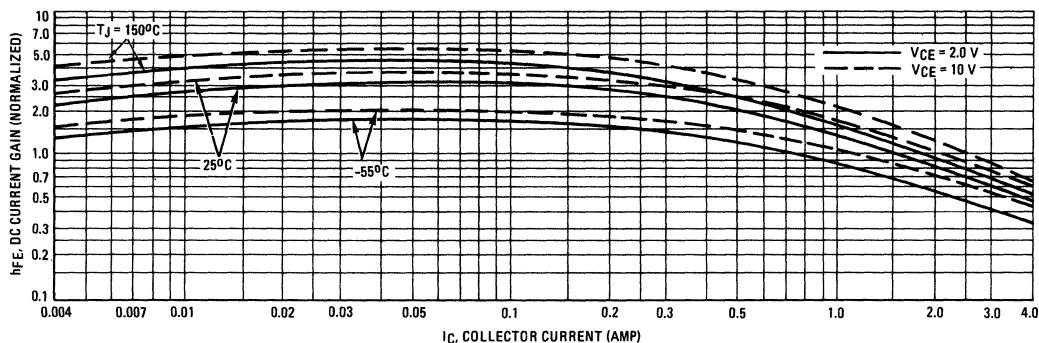


FIGURE 2 – COLLECTOR SATURATION REGION

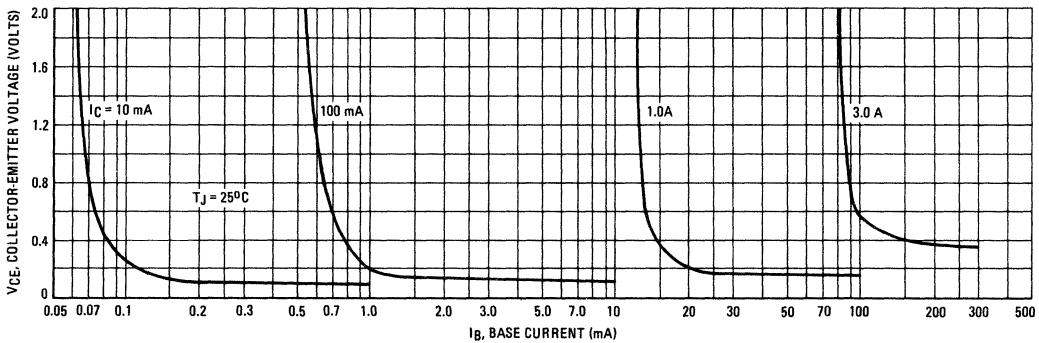


FIGURE 3 – "ON" VOLTAGE

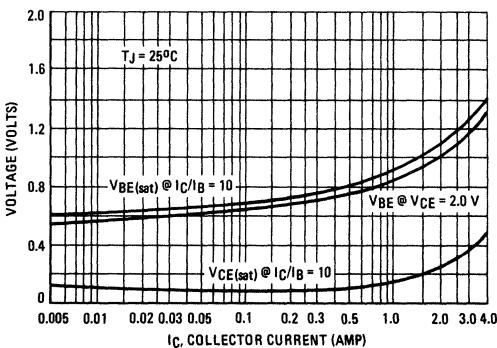
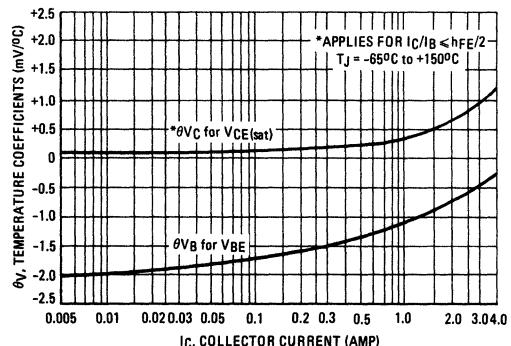


FIGURE 4 – TEMPERATURE COEFFICIENTS



2N5193 thru 2N5195/MJE5193 thru MJE5195 (continued)

FIGURE 5 – COLLECTOR CUT-OFF REGION

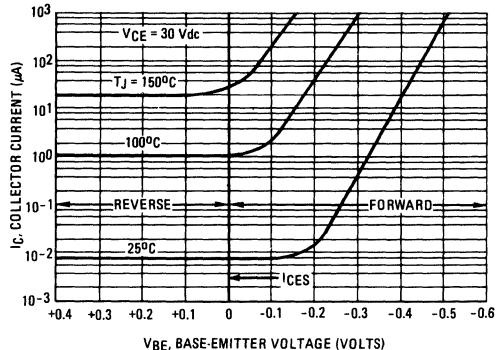


FIGURE 6 – EFFECTS OF BASE-EMITTER RESISTANCE

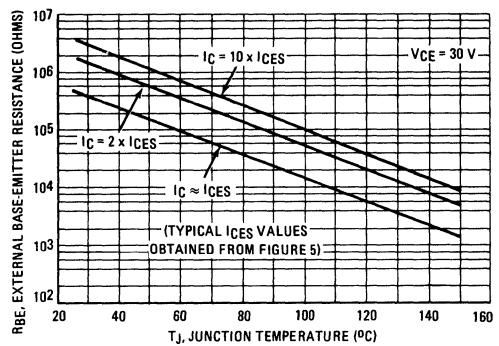


FIGURE 7 – SWITCHING TIME EQUIVALENT CIRCUIT

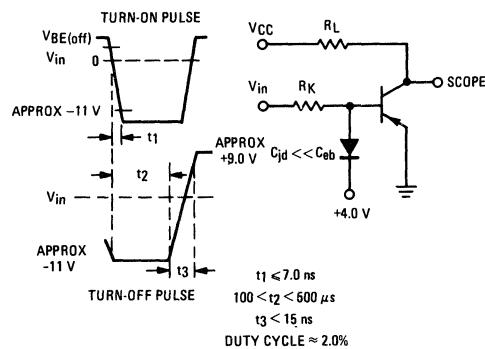


FIGURE 8 – CAPACITANCE

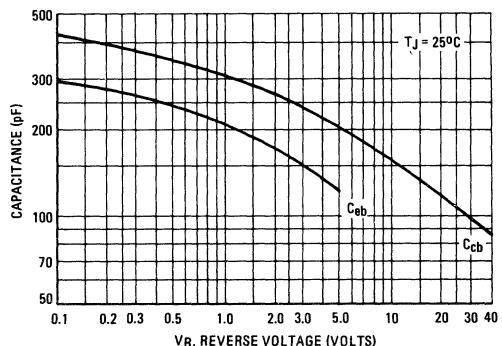


FIGURE 9 – TURN-ON TIME

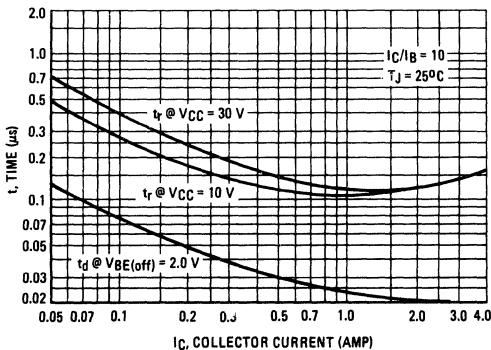
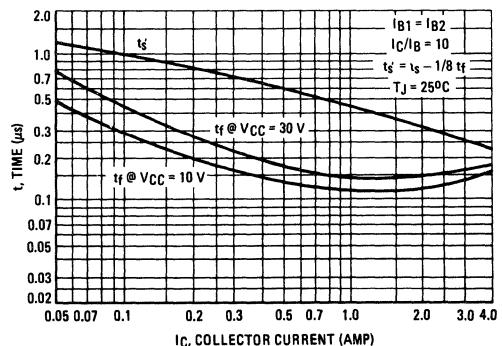
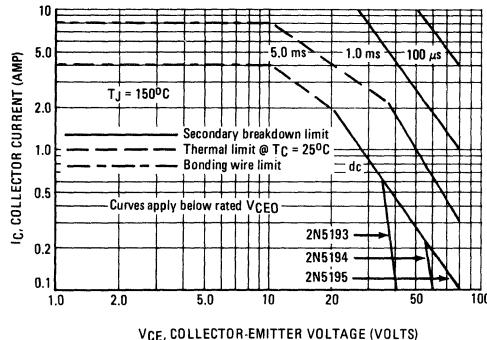


FIGURE 10 – TURN-OFF TIME



**RATING AND THERMAL DATA
ACTIVE-REGION SAFE OPERATING AREA**

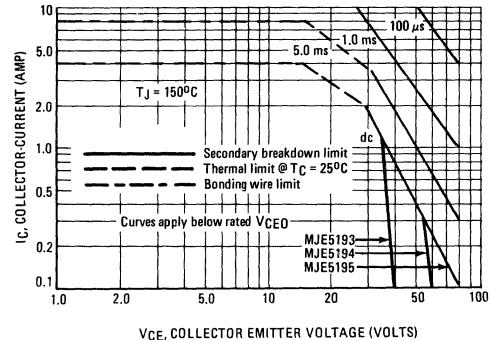
FIGURE 11 – 2N5193, 2N5194, 2N5195



Note 1:

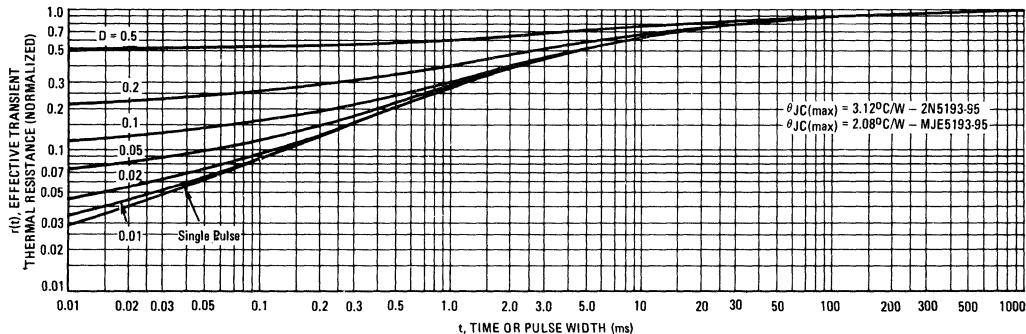
There are two limitations on the power handling ability of a transistor; average junction temperature and second breakdown. Safe operating area curves indicate I_C - V_{CE} limits of the transistor that must be observed for reliable operation; i.e., the transistor must not be subjected to greater dissipation than the curves indicate.

FIGURE 12 – MJE5193, MJE5194, MJE5195



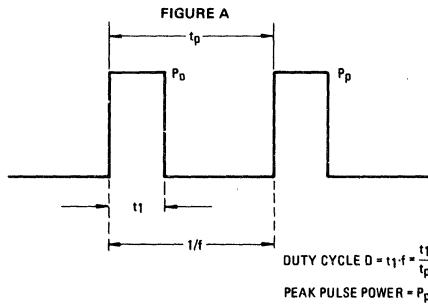
The data of Figures 11 and 12 is based on $T_J(pk) = 150^\circ\text{C}$; T_C is variable depending on conditions. Second breakdown pulse limits are valid for duty cycles to 10% provided $T_J(pk) \leq 150^\circ\text{C}$. At high case temperatures, thermal limitations will reduce the power that can be handled to values less than the limitations imposed by second breakdown. (See AN-415)

FIGURE 13 – THERMAL RESPONSE



DESIGN NOTE: USE OF TRANSIENT THERMAL RESISTANCE DATA

FIGURE A



A train of periodical power pulses can be represented by the model shown in Figure A. Using the model and the device thermal response, the normalized effective transient thermal resistance of Figure 13 was calculated for various duty cycles.

To find $\theta_{JC}(t)$, multiply the value obtained from Figure 13 by the steady state value θ_{JC} .

Example:

The 2N5193 is dissipating 50 watts under the following conditions: $t_1 = 0.1$ ms, $t_P = 0.5$ ms. ($D = 0.2$).

Using Figure 13, at a pulse width of 0.1 ms and $D = 0.2$, the reading of $r(t_1, D)$ is 0.27.

The peak rise in junction temperature is therefore:

$$\Delta T = r(t) \times P_p \times \theta_{JC} = 0.27 \times 50 \times 3.12 = 42.2^\circ\text{C}$$