## MIL-PRF-38534 CERTIFIED



# WIDE BANDWIDTH, VERY HIGH VOLTAGE CRT VIDEO AMPLIFIER

(315) 701-6751

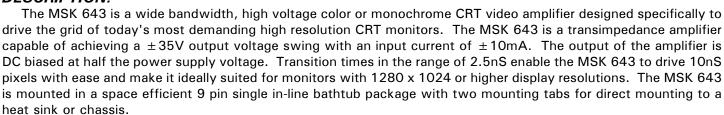
## FEATURES:

Negative Output Voltage for Grid Drive

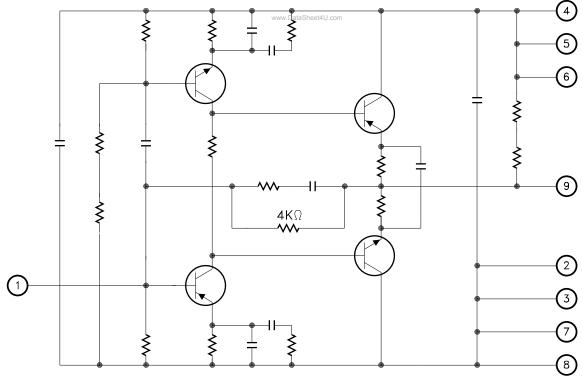
4707 Dey Road Liverpool, N.Y. 13088

- 2.5nS Transition Times
- Drives 8.5pF Capacitive Load With Ease
- · DC Coupled for Output Level Adjust
- 175MHz Bandwidth
- 70Vpp Output Swing
- · Replacement for CR3424R
- Contact MSK for MIL-PRF-38534 for Qualification Status

#### **DESCRIPTION:**



## EQUIVALENT SCHEMATIC



### **TYPICAL APPLICATIONS**

- CRT Driver for Color and Monochrome Monitors
- High Voltage Transimpedance Amplifier
- Ultra High Speed Amplifier for
- Test Equipment

## **PIN-OUT INFORMATION**

1	Inverting	Input
0	<b>O</b>	

- 2 Ground
- 3 Ground
- 4 -Vee 5 -Vee

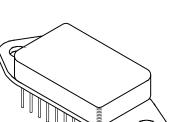
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6 -Vee

7 Ground

8 Ground

9 Output



## **ABSOLUTE MAXIMUM RATINGS**

-V <sub>EE</sub> θJC	Supply Voltage	
	(Junction to Case)	
Ιουτ	Peak Output Current	Tc

 $\bigcirc$ 

Storage Temperature Range -65°C to +150°C	
Lead Temperature Range	
(10 Seconds)	
Case Operating Temperature	
MSK643	
MSK643G	
1750C	

ТJ 

## **ELECTRICAL SPECIFICATIONS**

-Vee = -80V Unless Otherwise Specified

Parameter	Test Conditions (1)	Group A	MSK 643G			MSK 643			Units
Farameter		Subgroup	Min.	n. Typ. Max.		Min. Typ.		Max.	Units
STATIC									
Power Supply Current	$V_{IN} = N/C$	1	-	-40	-45	-	-40	-50	mA
		2	-	-55	-65	-	-55	-	mA
		3	-	-35	-45	-	-35	-	mA
Input Bias Voltage	VIN = N/C	1	-1.4	-1.55	-1.7	-1.3	-1.55	-1.8	V
		2,3	-1.35	-	-1.8	-	-	-	V
Output Offset Voltage	VIN = N/C	1	-38	-40	-42	-37	-40	-43	V
		2,3	-36	-40	-44	-	-	-	V
Input Capacitance 🗵	VIN = 0.7V	-	-	10	-	-	10	-	pF
Power Supply Range	Derated Performance	-	-60	-80	-85	-60	-80	-85	V
DYNAMIC CHARACTERISTICS									
Output Voltage High	f = 10KHz	4	-74	-76	-	-74	-76	-	V
Output Voltage Low	f = 10KHz	4	-	-4	-6	-	-4	-6	V
Voltage Gain	$V_{IN} = 2V_{PP}; f = 10KHz$	4	10.5	12.5	14.5	10	12.5	15	V/V
Rise Time	Vout = 40Vpp	4	-	2.5	3.4	-	2.5	3.5	nS
Fall Time	Vout = 40Vpp	4	-	2.5	3.4	-	2.5	3.5	nS
Overshoot (Adjustable) $2$	Vout = 20Vpp	-	-	25	-	-	25	-	%
-3dB Bandwidth ②	Vout = 20Vpp	-	125	175	-	120	175	-	MHz
Low Frequency Tilt Voltage $^{(\!2\!)}$	f=1KHz	-	-	-	1.5	-	-	1.5	V
Linearity Error	f = 10KHz; 5VPP≤Vout≤50Vpp	4	-	0.5	5	-	0.5	5	%

## NOTES:

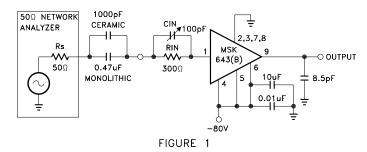
- $\begin{array}{l} \textcircled{1}{1} R_{\text{IN}} = 300\Omega, \ C_{\text{IN}} = 100 \text{pF}, \ C_{\text{LOAD}} = 8.5 \text{pF}, \ R_{\text{L}} = \infty, \ \text{unless otherwise specified (See Figure 1)}. \\ \textcircled{2}{2} \ Guaranteed \ by \ design \ but \ not \ tested. \ Typical \ parameters \ are \ representative \ of \ actual \ device \ performance \ but \ are \ for \ reference \ only. \\ \textcircled{3}{3} \ Industrial \ grade \ devices \ shall \ be \ tested \ to \ subgroups \ 1 \ and \ 4 \ unless \ otherwise \ specified. \\ \textcircled{4}{3} \ Military \ grade \ devices \ ('G' \ suffix) \ shall \ be \ 100\% \ tested \ to \ subgroups \ 1,2,3 \ and \ 4. \end{array}$

- (5) Subgroup 5 and 6 testing available upon request.
- 6 Subgroup 1,4  $T_A = T_C = +25 \circ C$
- $T_A = T_C = +85 \,^{\circ}C$ Subgroup 2,5
- Subgroup 3,6  $T_A = T_C = -55 \circ C$

🗇 Continuous operation at or above absolute maximum ratings may adversely effect the device performance and/or life cycle.

#### TYPICAL TEST CIRCUIT

The signal source in Figure 1 can be either a fast pulse generator or a network analyzer as long as the output impedance is 50 ohms. The DC level of the input should be -1.55V and all cables should be kept as short as possible. Since total load capacitance should be kept below 8.5pF, a FET probe should be used on the ouput.

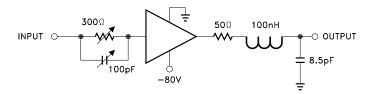


#### USING THE MSK 643

The output of the amplifier is biased at one half of the power supply voltage. An output voltage swing of  $\pm$  35 volts is typical with a power supply voltage of -80 volts. With an 8.5pF capacitive load, transistion times are in the 2.5nS range. If a spark gap current limiting resistor is used on the output of the amplifier and the transistion times are degraded, a peaking coil may be used to preserve system performance. The optimum value for this coil will be in the range of 100 to 200nH and can best be determined by trial and error. The output of the MSK 643 is not short circuit protected, therefore, purely resistive loads should be no less than 800 ohms at any time to avoid damaging the output.

#### **OPERATION CONSIDERATIONS**

The input of the MSK 643 rests at a -1.55VDC level with the input terminal open. In this state, the output rests at one half of the power supply voltage. When connecting a pulse generator to the input of the amplifier, the DC level should be offset so that the signal is centered around -1.55V. During characterization, the input should be coupled to the MSK 643 through a parallel combination of a variable resistor and variable capacitor peaking circuit. Optimum values for the peaking circuit can be determined experimentally. The optimum value of load capacitance is 8.5pF. Viewing the output with a normal oscilloscope probe would seriously degrade performance. A FET probe fitted with a 100:1 voltage divider will add only approximately 1.5pF of capacitance to the load and is highly recommended. An experimental circuit along with recommended values can be found in Figure 2.



#### **OUTPUT ISSUES**

The output of the MSK 643 is a pair of bipolar emitter followers configured in a complimentary push pull configuration. This configuration eliminates the need for a pull up load resistor and makes the amplifier less susceptible to load capacitance variations. Connecting a wire or cable from the output of the amplifier to the CRT grid can create a resonant circuit which can cause unwanted oscillations or overshoot at its resonant frequency. A damping resistor in series with the lead inductance will alleviate this condition. The optimum value of this resistor can be determined using the following formula:

 $R = 2* \sqrt{L/C}$ 

This resistor also doubles as an arcing protector. In the breadboarding stage, the value of this resistor should be determined experimentally. Resistance in the range of 50 to 100 ohms is usually sufficient. If a quick, simple peaking network is desired, a 300 ohm cable terminated by a capacitor will act like an inductor in the frequency range involved.

#### TRANSIMPEDANCE AMPLIFICATION

Transimpedance amplifiers relate input current to output voltage. The MSK 643 contains an internal  $4K\Omega$  feedback resistor. This resistor converts input current to output voltage in the following manner (See Figure 1):

 $\pm$  1.43V (referenced to -1.55Vdc) across the 300 $\Omega$  input resistor results in an input current of  $\pm$ 4.77mA. This current flows through the 4K $\Omega$  feedback resistor and results approximately in a  $\pm$  20V swing at the output. The actual voltage gain of the typical MSK 643 circuit may be slightly less due to transistor losses. The following formula approximates voltage gain including potential losses:

Voltage Gain (V/V) =  $4K\Omega/(Rin + L)$   $L \approx 25\Omega$ 

#### HEAT SINKING

The MSK 643 requires heat sinking in most applications. The following formula may be applied to determine if a heat sink is necessary and what size and type to use.

$$R_{\theta}sa = ((T_j-T_a)/Pd) - (R_{\theta}c) - (R_{\theta}cs)$$

WHERE

- Tj = Junction Temperature
- Pd = Total power dissipation

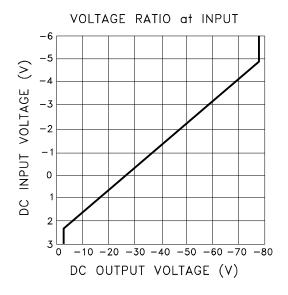
 $R_{\theta}jc =$  Junction to case thermal resistance

- $R_{\theta}cs = Case$  to heat sink thermal resistance
- Resa = Heat sink to ambient thermal resistance
- Tc = Case temperature
- Ta = Ambient temperature
- Ts = Sink temperature

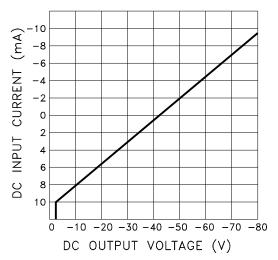
Tj = 150 °C Ta = 85 °C Pd = 1.5W  $R_{\theta j c} = 27 °C/W$   $R_{\theta c s} = 0.15 °C/W$ 

Solving the above equation for Resa (heat sink thermal conductivity) shows that the heat sink for this application must have a thermal resistance of no more than  $16^{\circ}$ C/W to maintain a junction temperature of no more than  $150^{\circ}$ C.

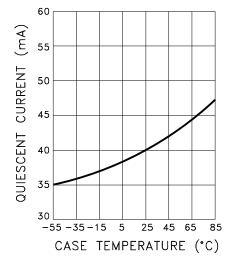
## **TYPICAL PERFORMANCE CURVES**

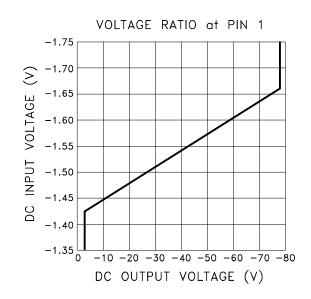


OUTPUT VOLTAGE vs INPUT CURRENT

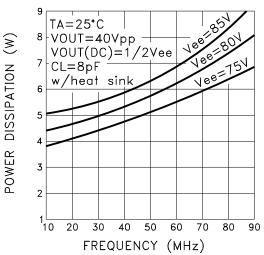


QUIESCENT CURRENT vs TEMPERATURE

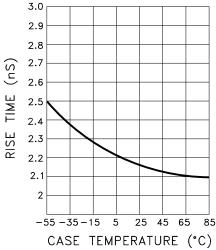




POWER DISSIPATION vs FREQUENCY



RISE TIME vs TEMPERATURE



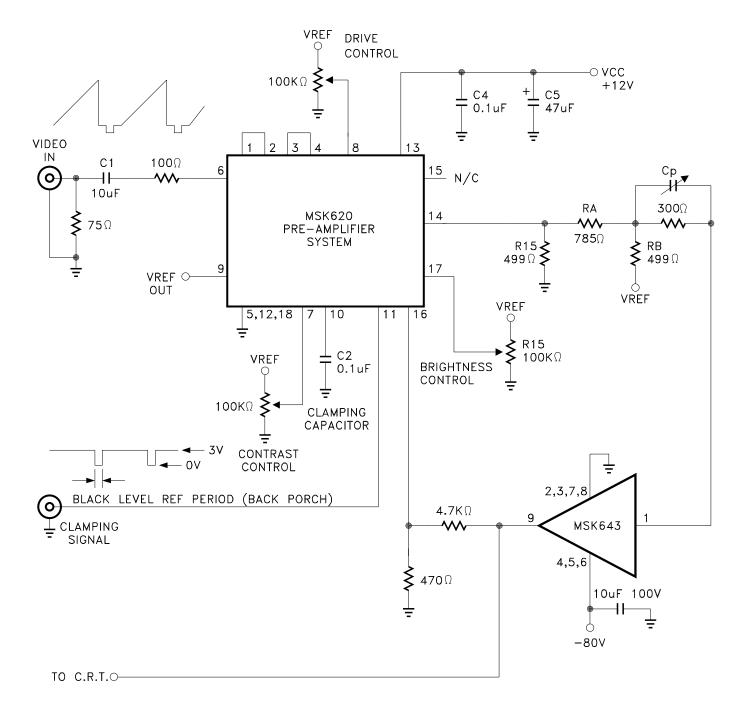
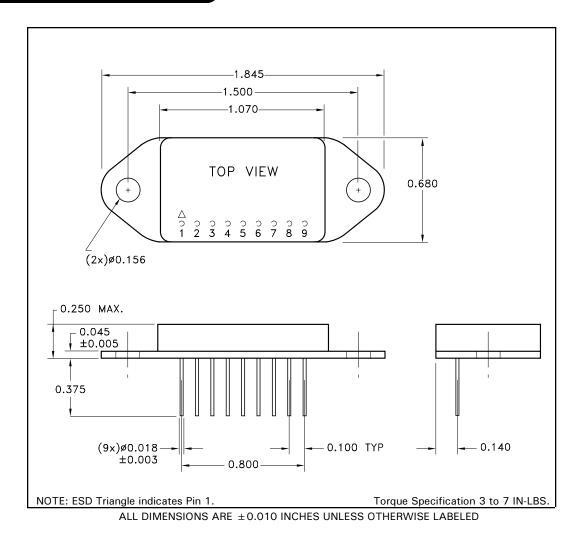


FIGURE 3

Figure 3 above illustrates how an MSK 620 and MSK 643 can be used to build a compete video system for high voltage grid drive. RA and RB act as a level shift stage to match the +3.9Vdc level at the output of the MSK 620 with the -1.55Vdc level at the input of the MSK 643. The output of the MSK 643 is sampled and fed back to the MSK 620. This scheme provides black level control superior to sampling the signal at pin 14 of the MSK 620. The general rule of thumb for transition times for a video driver is that rising and falling edges should be no more than one third the pixel time of the monitor. To improve rise and fall time in the system, the peaking capacitor Cp was added across the input resistor of the MSK 643. At high frequencies Cp increases the gain of the amplifier there by causing peaking. Cp should be a variable capacitor so that the response of the amplifier can be fine tuned for minimum transition time with minimum overshoot.



# **ORDERING INFORMATION**

Part Number	Screening Level				
MSK643	Industrial				
MSK643G	Mil-PRF-38534 Class G				

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Contact MSK for MIL-PRF-38534 qualification status.