Preferred Device

Power MOSFET 16 Amps, 400 Volts N-Channel TO-247

This high voltage MOSFET uses an advanced termination scheme to provide enhanced voltage-blocking capability without degrading performance over time. In addition, this advanced Power MOSFET is designed to withstand high energy in the avalanche and commutation modes. The new energy efficient design also offers a drain-to-source diode with a fast recovery time. Designed for high voltage, high speed switching applications in power supplies, converters and PWM motor controls, these devices are particularly well suited for bridge circuits where diode speed and commutating safe operating areas are critical and offer additional safety margin against unexpected voltage transients.

- Robust High Voltage Termination
- Avalanche Energy Specified
- Source-to-Drain Diode Recovery Time Comparable to a Discrete Fast Recovery Diode
- Diode is Characterized for Use in Bridge Circuits
- IDSS and VDS(on) Specified at Elevated Temperature
- Isolated Mounting Hole Reduces Mounting Hardware

MAXIMUM RATINGS ($T_{C} = 25^{\circ}C$ unless otherwise noted)

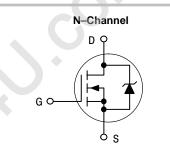
Symbol	Value	Unit		
VDSS	400	Vdc		
VDGR	400	Vdc		
V _{GS} V _{GSM}	± 20 ± 40	Vdc Vpk		
ID ID IDM	16 9.0 56	Adc Apk		
PD	180 1.4	Watts W/°C		
TJ, T _{stg}	–55 to 150	°C		
E _{AS}	870	mJ		
R _θ JC R _θ JA	0.70 40	°C/W		
т∟	260	°C		
	Symbol VDSS VDGR VGS VGSM ID ID ID ID ID ID ID ID ID ID	$\begin{array}{c c} \mbox{Symbol} & \mbox{Value} \\ \mbox{VDSS} & 400 \\ \mbox{VDGR} & 400 \\ \mbox{VGS} & \pm 20 \\ \mbox{± 40} \\ \mbox{VGSM} & \pm 40 \\ \mbox{ID} & 16 \\ \mbox{9.0} \\ \mbox{1.4} \\ \mbox{ID} & 56 \\ \mbox{PD} & 180 \\ \mbox{1.4} \\ \mbox{TJ, Tstg} & -55 \ to \\ \mbox{150} \\ \mbox{EAS} & 870 \\ \mbox{ReJA} & 40 \\ \end{array}$		



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16 AMPERES 400 VOLTS RDS(on) = 240 m Ω

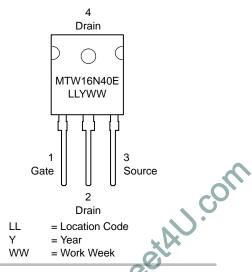






MARKING DIAGRAM **& PIN ASSIGNMENT**

2 3



ORDERING INFORMATION

Device	Package	Shipping
MTW16N40E	TO-247	30 Units/Rail

Preferred devices are recommended choices for future use and best overall value.

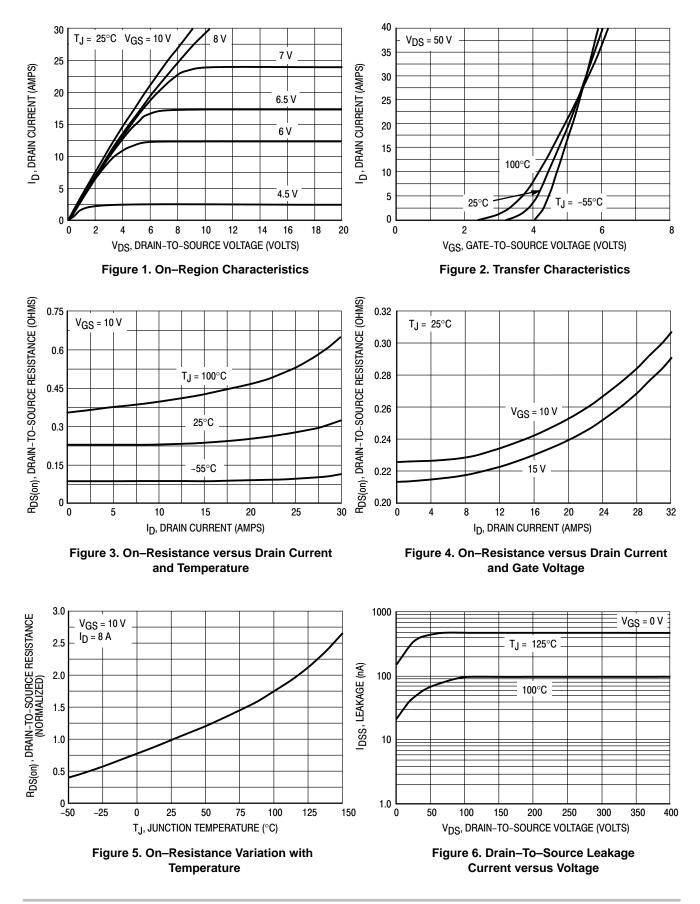
ELECTRICAL CHARACTERISTICS (T_J = 25° C unless otherwise noted)

Characteristic			Тур	Max	Unit
			1		
$\begin{tabular}{lllllllllllllllllllllllllllllllllll$			_ 420		Vdc mV/°C
Zero Gate Voltage Drain Current $(V_{DS} = 400 \text{ Vdc}, V_{GS} = 0 \text{ Vdc})$ $(V_{DS} = 320 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 125^{\circ}\text{C})$				0.25 1.0	mAdc
$s = \pm 20 \text{ Vdc}, \text{ V}_{\text{DS}} = 0)$	IGSS	-	-	100	nAdc
ON CHARACTERISTICS (Note 1.) Gate Threshold Voltage (V _{DS} = V _{GS} , I _D = 0.25 mAdc) Temperature Coefficient (Negative)			3.0 7.0	4.0 -	Vdc mV/°C
e (V _{GS} = 10 Vdc, I _D = 8.0 Adc)	R _{DS(on)}	-	0.225	0.24	Ohm
Drain–Source On–Voltage (V _{GS} = 10 Vdc) (I_D = 16 Adc) (I_D = 8.0 Adc, T _J = 125°C)				4.8 4.3	Vdc
= 15 Vdc, I _D = 8.0 Adc)	9FS	8.0	10	-	mhos
	C _{iss}	-	2570	3600	pF
$(V_{DS} = 25 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}, f = 1.0 \text{ MHz})$	C _{OSS}	-	330	460	
	C _{rss}	-	82	164	
Note 2.)					
	^t d(on)	-	29	50	ns
$(V_{DD} = 200 \text{ Vdc}, I_D = 16 \text{ Adc},$	tr	-	62	70	
$R_{\rm G} = 9.1 \ \Omega$	^t d(off)	-	76	170	
	t _f	-	57	95	
	QT	-	66	93	nC
$(V_{DS} = 320 \text{ Vdc}, I_{D} = 16 \text{ Adc},$	Q ₁	-	17	_	
VGS = 10 VdC)	Q ₂	-	31	-	
	Q ₃	-	30	-	
TERISTICS					
$(I_{S} = 16 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $(I_{S} = 16 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 125^{\circ}\text{C})$	V _{SD}	-	1.0 0.9	1.6 _	Vdc
	t _{rr}	-	340	_	ns
		_	228	_	-
		—	112	_	1
	Q _{RR}	_	4.3	_	μC
 ;E				•	
Internal Drain Inductance (Measured from the drain lead 0.25" from package to center of die)			5.0	-	nH
Internal Source Inductance (Measured from the source lead 0.25" from package to source bond pad)			13	_	nH
	ge e) $T_J = 125^{\circ}C)$ $S = \pm 20 \text{ Vdc}, \text{ V}_{DS} = 0)$ Ve) $Ve(V_{GS} = 10 \text{ Vdc}, \text{ I}_{D} = 8.0 \text{ Adc})$ 10 Vdc) $= 15 \text{ Vdc}, \text{ I}_{D} = 8.0 \text{ Adc})$ $(V_{DS} = 25 \text{ Vdc}, \text{ V}_{GS} = 0 \text{ Vdc}, \text{ f} = 1.0 \text{ MHz})$ Note 2.) $(V_{DD} = 200 \text{ Vdc}, \text{ I}_{D} = 16 \text{ Adc}, \text{ V}_{GS} = 10 \text{ Vdc}, \text{ R}_{G} = 9.1 \Omega)$ $(V_{DS} = 320 \text{ Vdc}, \text{ I}_{D} = 16 \text{ Adc}, \text{ V}_{GS} = 10 \text{ Vdc})$ $(V_{DS} = 320 \text{ Vdc}, \text{ I}_{D} = 16 \text{ Adc}, \text{ V}_{GS} = 10 \text{ Vdc})$ $(I_{S} = 16 \text{ Adc}, \text{ V}_{GS} = 0 \text{ Vdc})$ $(I_{S} = 16 \text{ Adc}, \text{ V}_{GS} = 0 \text{ Vdc}, \text{ I}_{J} = 125^{\circ}C)$ $(I_{S} = 16 \text{ Adc}, \text{ V}_{GS} = 0 \text{ Vdc}, \text{ dI}_{S}/\text{dt} = 100 \text{ A/}\mu\text{s})$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ge V(BR)DSS 400 e) IDSS - TJ = 125°C) IGSS - S = ± 20 Vdc, VDS = 0) IGSS - ve) VGS(th) 2.0 pe (VGS = 10 Vdc, ID = 8.0 Adc) RDS(on) - 10 Vdc) VDS(on) - 10 Vdc, ges 8.0 (VDS = 25 Vdc, VGS = 0 Vdc, f = 1.0 MHz) Ciss - (VDS = 25 Vdc, VGS = 0 Vdc, f = 16 Adc, VGS = 10 Vdc, RG = 9.1 \Omega) td(on) - (VDD = 200 Vdc, ID = 16 Adc, VGS = 10 Vdc, RG = 9.1 \Omega) tf - (VDS = 320 Vdc, ID = 16 Adc, VGS = 10 Vdc) QT - (VDS = 320 Vdc, ID = 16 Adc, VGS = 0 Vdc) Q1 - (VDS = 320 Vdc, ID = 16 Adc, VGS = 0 Vdc) Q1 - (VDS = 320 Vdc, ID = 16 Adc, VGS = 0 Vdc) VSD - (IS = 16 Adc, VGS = 0 Vdc, dIS/d = 100 A/µS) VSD - (IS = 16 Adc, VGS = 0 Vdc, dIS/d = 100 A/µS) VSD - (IS = 16 Adc, VGS = 0 Vdc, dIS/d = 100 A/µS) URR - 25" from package to center of die) LD -	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

1. Pulse Test: Pulse Width \leq 300 μ s, Duty Cycle \leq 2%.

2. Switching characteristics are independent of operating junction temperature.

TYPICAL ELECTRICAL CHARACTERISTICS



POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_G(AV)$) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$

During the rise and fall time interval when switching a resistive load, V_{GS} remains virtually constant at a level known as the plateau voltage, V_{SGP} . Therefore, rise and fall times may be approximated by the following:

$$\label{eq:tr} \begin{split} t_r &= Q_2 \; x \; R_G / (V_{GG} - V_{GSP}) \\ t_f &= Q_2 \; x \; R_G / V_{GSP} \end{split}$$

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_{G} = the gate drive resistance

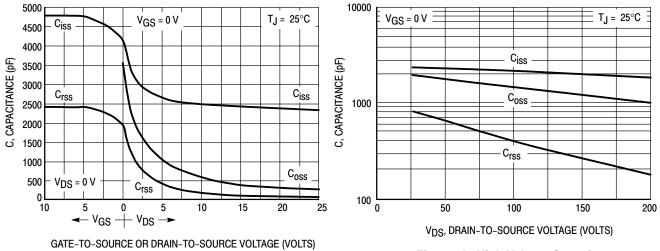
and Q_2 and V_{GSP} are read from the gate charge curve.

During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

 $t_{d(on)} = R_G C_{iss} In [V_{GG}/(V_{GG} - V_{GSP})]$ $t_{d(off)} = R_G C_{iss} In (V_{GG}/V_{GSP})$ The capacitance (C_{ISS}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



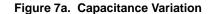
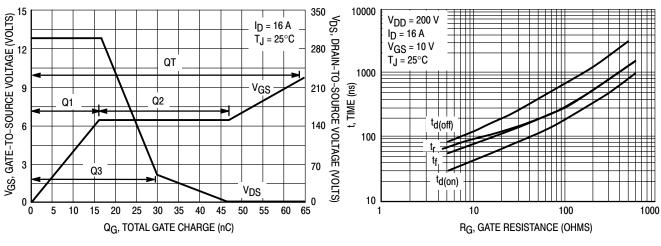


Figure 7b. High Voltage Capacitance Variation



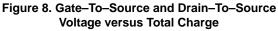


Figure 9. Resistive Switching Time Variation versus Gate Resistance



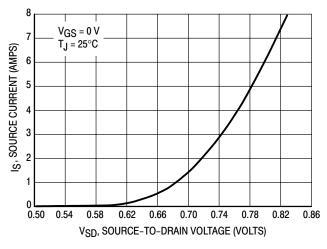


Figure 10. Diode Forward Voltage versus Current

SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain–to–source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance–General Data and Its Use."

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (VDSS) is exceeded and the transition time (t_r , t_f) do not exceed 10 μ s. In addition the total power averaged over a complete switching cycle must not exceed (T_{J(MAX)} – T_C)/(R θ JC).

A Power MOSFET designated E–FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature

Although many E–FETs can withstand the stress of drain–to–source avalanche at currents up to rated pulsed current (I_{DM}), the energy rating is specified at rated continuous current (I_D), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous I_D can safely be assumed to equal the values indicated.

SAFE OPERATING AREA

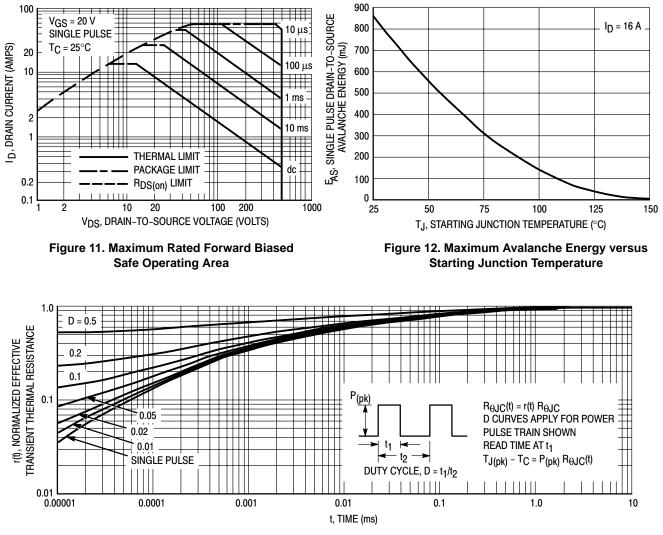


Figure 13. Thermal Response

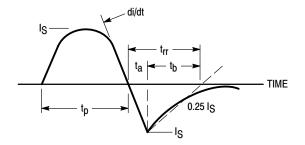
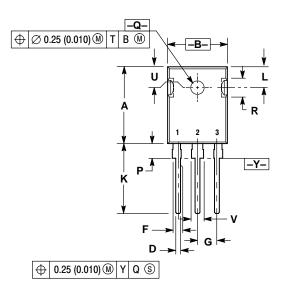
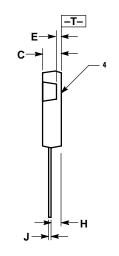


Figure 14. Diode Reverse Recovery Waveform

PACKAGE DIMENSIONS

TO-247 CASE 340K-01 ISSUE C





NOTES: 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982. 2. CONTROLLING DIMENSION: MILLIMETER.

	MILLIMETERS		TERS INCHES		
DIM	MIN	MAX	MIN	MAX	
Α	19.7	20.3	0.776	0.799	
В	15.3	15.9	0.602	0.626	
С	4.7	5.3	0.185	0.209	
D	1.0	1.4	0.039	0.055	
Е	1.27 REF		0.050 REF		
F	2.0	2.4	0.079	0.094	
G	5.5 BSC		0.216 BSC		
Η	2.2	2.6	0.087	0.102	
J	0.4	0.8	0.016	0.031	
K	14.2	14.8	0.559	0.583	
L	5.5 1	MON	0.217 NOM		
Ρ	3.7	4.3	0.146	0.169	
Q	3.55	3.65	0.140	0.144	
R	5.0 NOM		0.197 NOM		
U	5.5 BSC		0.217 BSC		
۷	3.0	3.4	0.118	0.134	

STYLE 1: PIN 1. GATE 2. DRAIN 3. SOURCE 4. DRAIN

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