



## 1. Features

### GaNSense™ Power FET

- Loss-less current sensing
- Low 260 mΩ power FET
- Zero reverse recovery charge
- Low output charge
- 800 V Transient Voltage Rating
- 700 V Continuous Voltage Rating

### High Frequency QR Controller

- Wide VDD range up to 77V
- QR valley switching and optional CCM operating modes
- High frequency operation up to 225kHz
- High voltage start-up
- Frequency hopping for low EMI
- OVP, UVP, OTP, CSSP, SSSP, SD protection functions
- LPS function
- Ultra-low standby current consumption (<20mW)

### Small, low-profile SMT QFN

- 5 x 6 mm footprint, 0.85 mm profile
- Minimized package inductance
- Large cooling pad

### High Power Density

- > 1W/cc achievable power density
- Small transformer size
- Low component count

### Sustainability

- RoHS, Pb-free, REACH-compliant
- Up to 40% energy savings vs Si solutions
- System level 4kg CO<sub>2</sub> Carbon Footprint reduction

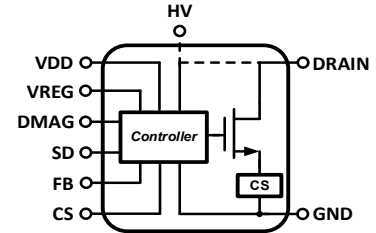
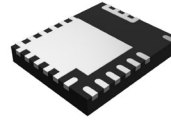
### Product Reliability

- 20-year limited product warranty  
(see Section 14 for details)

## 2. Topologies / Applications

- High efficiency AC-DC power adapters
- USB PD/QC battery charger

## GaNSense™ HFQR Controller



**QFN 5x6 Super**

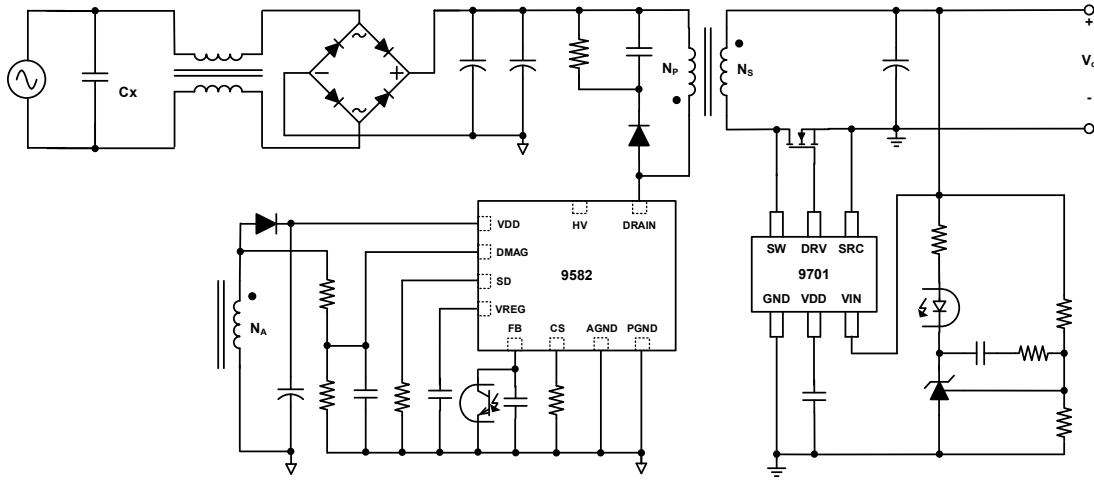
**Simplified schematic**

- Mobile chargers, adapters, aux power

## 3. Description

This GaNSense™ HFQR controller integrates a high performance eMode GaNSense Power FET together with an HFQR Flyback controller to achieve unprecedented high-frequency and high-efficiency operation for smallest size mobile charger and adapter solutions. The GaNSense Power FET includes loss-less current sensing, ultra-low gate charge, low output charge, and 700V continuous and 800V transient voltage ratings to provide excellent performance and robustness. The HFQR Flyback controller enables high frequency operation, wide VDD range, high-voltage start-up, and multi-mode operation. The HFQR Flyback controller also includes abnormal component short-circuit, over-temperature and LPS protection features to increase system robustness, while ultra-low standby current consumption increases light, tiny & no-load efficiency. Low-profile, low-inductance, and small footprint SMT QFN 5x6 packaging enables designers to achieve simple, quick and reliable solutions. Navitas' GaN IC technology enables high frequencies, high efficiencies and low EMI to achieve unprecedented power densities at a very attractive cost structure.

#### 4. Typical Application Circuit



HFQR Flyback

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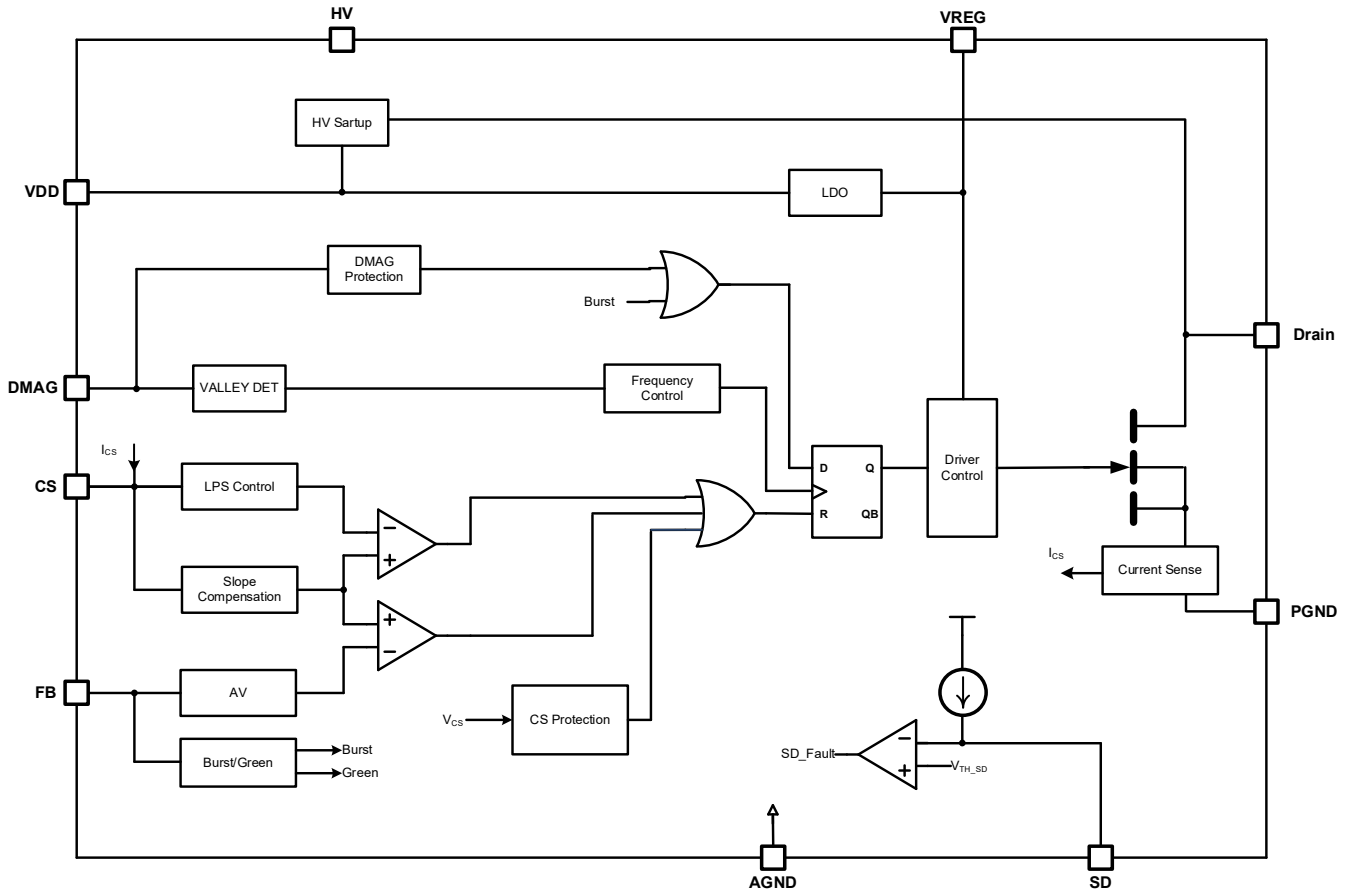
## 6. Ordering Information

Part Number	Maximum Frequency	Function	Protection Mode	R <sub>DS(ON)</sub>	Operating Temperature Range	Package	Packing Method
NV9582F1P1	129kHz/100kHz	PL+CC, OLP	AR	260mΩ	-40°C to +125°C	QFN 5x6	5,000 13" Tape & Reel
NV9582F2P1	225kHz/164kHz	PL+CC, OLP	AR				
NV9582F1P3	129kHz/100kHz	PL+CC, No OLP	AR				
NV9582F111	129kHz/100kHz	CCM, CC, OLP	AR				

\*PL=Power Limit, CC=Constant Current

\*Those protection functions not mentioned in **Protection Mode** column, they are all AR (auto restart) mode.

## 7. Internal Functional Block Diagram



## 8. Specifications

### 8.1. Absolute Maximum Ratings<sup>(1)</sup>

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol	Parameter	Min.	Max.	Unit	
$V_{DS(CONT)}$	GaN Power FET Drain-to-Source Voltage	-7	700	V	
$V_{DS(TRAN)}$	GaN Power FET Transient Drain-to-Source Voltage <sup>(2)</sup>	-	800	V	
$V_{VDD}$	VDD DC Supply Voltage	-0.3	80	V	
$V_{CS}$	CS Pin Input Voltage	-0.3	6	V	
$V_{FB}$	FB Pin Input Voltage	-0.3	6	V	
$V_{DMAG}$	DMAG Pin Input Voltage	-0.3	6	V	
$V_{SD}$	SD Pin Input Voltage	-0.3	6	V	
$V_{REG}$	VREG Pin Output Voltage	-0.3	7.5	V	
$I_D$	GaN Power FET Continuous Drain Current (@ $T_C = 100^\circ\text{C}$ )	-	5	A	
$I_D$ PULSE	GaN Power FET Pulsed Drain Current (10 $\mu\text{s}$ @ $T_J = 25^\circ\text{C}$ )	-	10	A	
$\theta_{JA}$	Thermal Resistance (Junction-to-Ambient) QFN 5x6 <sup>(3)</sup>	-	77.8	$^\circ\text{C}/\text{W}$	
$\theta_{JC}$	Thermal Resistance (Junction-to-Case) QFN 5x6 <sup>(3)</sup>	-	4.5	$^\circ\text{C}/\text{W}$	
$T_J$	Operating Junction Temperature	-40	150	$^\circ\text{C}$	
$T_{STG}$	Storage Temperature Range	-40	150	$^\circ\text{C}$	
$T_L$	Lead Temperature (Soldering) 10 Seconds	-	260	$^\circ\text{C}$	
ESD	Electrostatic Discharge Capability	Human Body Mode, ANSI/ESDA/JEDEC JS-001-2017	-	2.0	kV
		Charge Device Mode, ANSI/ESDA/JEDEC JS-001-2018	-	2.0	kV

Note (1): Absolute maximum ratings are stress ratings; devices subjected to stresses beyond these ratings may cause permanent damage.

Note (2):  $V_{DS(TRAN)}$  rating allows for surge ratings during non-repetitive events that are <100us (for example start-up, line interruption).  $V_{DS(TRAN)}$  rating allows for repetitive events that are <400ns, with 80% derating required (for example repetitive leakage inductance spikes). Refer to Section "GaN Power FET Drain-to-Source Voltage Considerations" for detailed recommended design guidelines.

Note (3): Measured on DUT mounted on 1 square inch 2 oz Cu (FR4 PCB)

## 8.2. Recommended Operating Conditions<sup>(4)</sup>

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance. Navitas does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Min.	Typ.	Max.	Unit
V <sub>VDD</sub>	VDD Pin Supply Voltage	-0.3		75	V
V <sub>CS</sub>	CS Pin Supply Voltage	-0.3		5.5	V
V <sub>FB</sub>	FB Pin Supply Voltage	-0.3		5.5	V
V <sub>DMAG</sub>	DMAG Pin Supply Voltage	-0.3		5.5	V
V <sub>SD</sub>	SD Pin Supply Voltage	-0.3		5.5	V
V <sub>REG</sub>	VREG Pin Output Voltage	-0.3		7	V

*Note (4): Functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied, exposure to absolute maximum rated conditions of extended periods may affect device reliability. All voltage values are with respect to the normal operation ambient temperature range is from -40°C to +125°C unless otherwise noted.*

### 8.3. Electrical Specifications

$V_{DD}$  (Typ.) = 12V,  $T_A$  = -40°C to 125°C, and  $T_A$  (Typ.) = 25°C, unless otherwise specified.

Parameter	Test Conditions	Min.	Typ.	Max.	Unit	
<b>HV Startup Section</b>						
$I_{HV}$	Startup Current Drawn from Drain Pin	$V_{DRAIN}=50V, V_{DD}=0V$	2		20	mA
$I_{HV\_LC}$	Startup Leakage Current Drawn from Drain Pin	$V_{DRAIN}=700V, V_{DD}=V_{DD\_UVLO}+1V$			3	$\mu A$
<b>VDD Section</b>						
$V_{DD\_ON}$	$V_{DD}$ Turn-On Threshold Voltage	$V_{DD}$ Rising	12.5	13.5	14.5	V
$V_{DD\_UVLO}$	$V_{DD}$ UVLO Threshold Voltage		6.2	6.5	6.8	V
$V_{DD\_DLCH}^{(5)}$	$V_{DD}$ Threshold for Latch Release		1.2	1.8	2.2	V
$I_{DD\_ST}$	Startup Current		0.5	2	5	$\mu A$
$I_{DD\_OP}$	Operating Supply Current	No DRV Switching	0.6	0.75	0.9	mA
$I_{DD\_DPGN}$	Operating Supply Current in Deep Green-Mode		300	375	450	$\mu A$
$t_{D\_DPGN}$	Debounce Time to Enter Deep Green Mode		380	480	580	$\mu s$
$V_{DD\_OVP}$	$V_{DD}$ Over-Voltage-Protection Threshold		77	78.5		V
$t_{D\_UVLO}^{(5)}$	UVLO De-bounce Time			10		$\mu s$
$t_{D\_VDD\_OVP}^{(5)}$	$V_{DD}$ Over-Voltage-Protection De-bounce Time			15		$\mu s$
$t_{VDD\_LAR}$	Long Auto-Restart Mode Time	Trim Option	2.08	2.64	3.20	s
<b>VREG Section</b>						
$V_{REG}$	VREG output voltage		6.15	6.4	6.65	V
$V_{REG\_5mA}$	VREG with 5mA Load Current	$I_{OUT} = 5mA$	6.05	6.4	6.65	V
<b>Oscillator Section</b>						
$f_{S\_BNK\_MAX\_LL}$	Maximum Blanking Frequency at Low Line Input Voltage	129kHz/100kHz	121	129	137	kHz
		225kHz/164kHz	202.5	225	247.5	kHz
$f_{S\_BNK\_MAX\_HL}$	Maximum Blanking Frequency at High Line Input Voltage	129kHz/100kHz	93	100	107	kHz
		225kHz/164kHz	147.2	164	180	kHz
$f_{S\_BNK\_MAX\_CCM}$	Maximum Blanking Frequency in CCM	129kHz/100kHz	93	100	107	kHz
$f_{S\_TMO}$	Minimum Time-Out PWM Frequency		23	25	27	kHz
$t_{ON\_MAX}$	Maximum PWM ON Time	129kHz/100kHz	16.6	18	19.4	$\mu s$
		225kHz/164kHz	9.5	10.5	11.5	$\mu s$
$D_{MAX}$	Maximum Duty Cycle		72	75	78	%
$m_{slp}^{(5)}$	Slope Compensation			60		mv/ $\mu s$
$\Delta V_{JIT}^{(5)}$	Current Sense Jitter Range			10		%
$T_{JIT}^{(5)}$	Frequency Jitter Period			0.64		ms



## Electrical Specifications (cont.)

$V_{DD}$  (Typ.) = 12V,  $T_A$  = -40°C to 125°C, and  $T_A$  (Typ.) = 25°C, unless otherwise specified.

Parameter		Test Conditions	Min.	Typ.	Max.	Unit
<b>Feedback Section</b>						
$V_{FB\_OPEN}$	FB Open Voltage		4.7	5.2		V
$Z_{FB}$	FB Pull Up Resistor		36	42	48	k $\Omega$
$V_{FB\_OLP}$	FB Threshold for OLP		3.4	3.5	3.6	V
$T_{D\_OLP}^{(5)}$	OLP Protection De-bounce time			36		ms
$A_{V\_HV}^{(5)}$	FB Voltage Attenuation Factor at High Output Voltage	129kHz/100kHz ( $V_{DMAG} > 1.75V$ )		0.225		V/V
$A_{V\_LV}^{(5)}$	FB Voltage Attenuation Factor at Low Output Voltage	129kHz/100kHz ( $V_{DMAG} < 1.6V$ )		0.200		V/V
$A_V^{(5)}$	FB Voltage Attenuation Factor	225kHz/164kHz		0.175		V/V
$V_{FB\_BST\_ENT}$	FB Threshold for Burst Mode Entry		0.50	0.55	0.60	V
$V_{FB\_BST\_EXT}$	FB Threshold for Burst Mode Exit		0.55	0.60	0.65	V
$V_{FB\_BNK\_STR}$	Frequency Foldback Start Point	129kHz/100kHz	2.240	2.300	2.380	V
$V_{FB\_BNK\_STR\_L}$	Frequency Foldback Start Point at Low Line Input Voltage	225kHz/164kHz	2.592	2.692	2.792	V
$V_{FB\_BNK\_STR\_H}$	Frequency Foldback Start Point at High Line Input Voltage	225kHz/164kHz	3.058	3.158	3.258	V
$V_{FB\_BNK\_END\_L}$	Frequency Foldback End Point at Low Line Input Voltage	129kHz/100kHz	1.340	1.394	1.480	V
		225kHz/164kHz	1.054	1.154	1.254	V
$V_{FB\_BNK\_END\_H}$	Frequency Foldback End Point at High Line Input Voltage	129kHz/100kHz	1.390	1.456	1.530	V
		225kHz/164kHz	1.051	1.151	1.251	V
$V_{FB\_CSMIN\_H}^{(5)}$	$V_{CS\_MIN}$ Foldback High Threshold Voltage	225kHz/164kHz	1.450	1.500	1.550	V
$V_{FB\_CSMIN\_L}^{(5)}$	$V_{CS\_MIN}$ Foldback Low Threshold Voltage	225kHz/164kHz	0.725	0.750	0.775	V

## Electrical Specifications (cont.)

$V_{DD}$  (Typ.) = 12V,  $T_A$  = -40°C to 125°C, and  $T_A$  (Typ.) = 25°C, unless otherwise specified.

Parameter	Test Conditions	Min.	Typ.	Max.	Unit	
<b>DMAG Section</b>						
$I_{DMAG\_MAX}$	Maximum Guaranteed Operating Current Flow Out of DMAG Pin	1.94			mA	
$I_{DMAG\_BRI}$	Current Threshold for Brown-In	0.432	0.480	0.528	mA	
$N_{BRI}$	Debounce Cycle for Brown-In		4		Cycle	
$I_{DMAG\_BRO}$	Current Threshold for Brown-Out	0.324	0.360	0.396	mA	
$t_{D\_BRO}$	Debounce Cycle for Brown-Out	14.5	16.5	18.5	ms	
$I_{DMAG\_HL}$	Current Threshold for High Line	1.008	1.120	1.232	mA	
$N_{HL\_ENT}$	Debounce Cycle for High Line Entry		4		Cycle	
$I_{DMAG\_LL}$	Current Threshold for Low Line	0.936	1.040	1.144	mA	
$t_{D\_LL\_ENT}$	Debounce Cycle for Low Line Entry	14.5	16.5	18.5	ms	
$t_{DMAG\_BNK\_L}$	DMAG Sampling Blanking Time	( $V_{FB} < 1.5V$ )	0.85	1.00	1.15	$\mu s$
$t_{DMAG\_BNK\_M}$	DMAG Sampling Blanking Time	( $V_{FB} > 1.6V$ )	1.28	1.50	1.73	$\mu s$
$V_{DMAG\_HV}$	$V_{DMAG}$ Threshold for High Output	1.65	1.75	1.85	V	
$V_{DMAG\_LV\_HYS}^{(5)}$	$V_{DMAG}$ Hysteresis Threshold for Low Output		0.15		V	
$V_{DMAG\_UVP}$	$V_{DMAG}$ Under-Voltage-Protection Threshold	0.390	0.425	0.460	V	
$N_{DMAG\_UVP}^{(5)}$	Debounce Cycle for $V_{DMAG\_UVP}$		2		Cycle	
$t_{VDMAG\_UVP\_BNK}$	$V_{DMAG\_UVP}$ Blanking Time during Start-up	25	32	35	ms	
$V_{DMAG\_OVP}$	$V_{DMAG}$ Over-Voltage-Protection Threshold	3.45	3.55	3.65	V	
$N_{DMAG\_OVP}^{(5)}$	Debounce Cycle for $V_{DMAG\_OVP}$		2		Cycle	

## Electrical Specifications (cont.)

$V_{DD}$  (Typ.) = 12V,  $T_A$  = -40°C to 125°C, and  $T_A$  (Typ.) = 25°C, unless otherwise specified.

Parameter		Test Conditions	Min.	Typ.	Max.	Unit
<b>Current Sense Section</b>						
Gain <sub>CS</sub>	Current Sense Ratio $I_{DRAIN} / I_{CS}$	$T_A$ (Typ.) = 25°C	2041	2200	2359	A/A
$V_{CS\_LIM}$	Maximum Current Sense Limit		0.620	0.650	0.680	V
$V_{CS\_MIN\_H}$	Minimum Current Sense Limit at High Output Voltage		0.190	0.225	0.260	V
$V_{CS\_MIN\_L}$	Minimum Current Sense Limit at Low Output Voltage		0.140	0.175	0.210	V
$V_{CS\_MIN\_FB\_STR\_LL\_H}$	Feedback of $V_{CS\_MIN}$ Foldback Start Point at Low Line and High Output Voltage	225kHz/164kHz	0.380	0.425	0.470	V
$V_{CS\_MIN\_FB\_STR\_LL\_L}$	Feedback of $V_{CS\_MIN}$ Foldback Start Point at Low Line and Low Output Voltage	225kHz/164kHz	0.330	0.375	0.420	V
$V_{CS\_MIN\_FB\_STR\_HL\_H}$	Feedback of $V_{CS\_MIN}$ Foldback Start Point at High Line and High Output Voltage	225kHz/164kHz	0.480	0.525	0.570	V
$V_{CS\_MIN\_FB\_STR\_HL\_L}$	Feedback of $V_{CS\_MIN}$ Foldback Start Point at High Line and Low Output Voltage	225kHz/164kHz	0.430	0.475	0.510	V
$t_{LEB}$	Leading Edge Blanking Time		220	295	370	ns
$t_{PD}$	Propagation Delay			30	45	ns
$V_{CS\_SP}$	CS Threshold for CS Short Circuit Protection		0.095	0.125	0.155	V
$N_{CS\_CSSP}^{(5)}$	Debounce Cycle for CSSP Protection Trigger			2		Cycle
$V_{CS\_SSSP}$	CS Threshold for SSSP		0.95	1.0	1.05	V
$N_{CS\_SSSP}^{(5)}$	Debounce Cycle for SSSP Protection Trigger			2		Cycle
$t_{D\_SSSP}$	Debounce Time for SSSP Protection Trigger		90	125	200	ns

## Electrical Specifications (cont.)

$V_{DD}$  (Typ.) = 12V,  $T_A$  = -40°C to 125°C, and  $T_A$  (Typ.) = 25°C, unless otherwise specified.

Parameter	Test Conditions	Min.	Typ.	Max.	Unit	
<b>Over-Temperature Protection Section</b>						
$T_{OTP}^{(5)}$	Over-Temperature-Protection Threshold		125	140	°C	
$\Delta T_{OTP}^{(5)}$	Over-Temperature-Protection Hysteresis		20		°C	
<b>Shut-Down Section</b>						
$V_{TH\_SD}$	Threshold Voltage for Shut-Down Trigger		0.97	1.00	1.03	V
$V_{TH\_SD\_STR}$	Threshold Voltage for Shut-Down Trigger at Start-up		1.07	1.10	1.13	V
$I_{SD}$	SD Pin Source Current		47.5	50	52.5	μA
$t_{D\_SD}$	Debounce Time for Shut-Down Trigger		300	400	500	μs
<b>GaN Power FET Section</b>						
Typical conditions: $V_{DS} = 400V$ , $F_{SW} = 1MHz$ , $T_A = 25^\circ C$ , $I_D = 2.5A$ , unless otherwise specified						
$I_{BSS}$	Drain-Source Leakage Current	$V_{DS} = 700V$ , PWM off		0.2	25	μA
$R_{DS(ON)}$	Drain-Source Resistance	PWM on, $I_D = 2.5A$		260	364	mΩ
$V_{SD}$	Source-Drain Reverse Voltage	$V_{PWM} = 0V$ , $I_{SD} = 2.5A$		3.5	5	V
$Q_{OSS}$	Output Charge			8.8		nC
$Q_{RR}$	Reverse Recovery Charge			0		nC
$C_{OSS}$	Output Capacitance	$V_{DS} = 400V$ , $V_{PWM} = 0V$		13		pF
$C_{O(er)}^{(6)}$	Effective Output Capacitance, Energy Related	$V_{DS} = 400V$ , $V_{PWM} = 0V$		16		pF
$C_{O(tr)}^{(6)}$	Effective Output Capacitance, Time Related	$V_{DS} = 400V$ , $V_{PWM} = 0V$		22		pF

Note (5): Guaranteed by design

Note (6):  $C_{O(er)}$  is a fixed capacitance that gives the same stored energy as  $C_{OSS}$  while  $V_{DS}$  is rising from 0 to 400 V

Note (6):  $C_{O(tr)}$  is a fixed capacitance that gives the same charging time as  $C_{OSS}$  while  $V_{DS}$  is rising from 0 to 400 V

8.4.

**8.4. Characteristic Graphs**

( $T_C = -40$  to  $125$  °C unless otherwise specified)

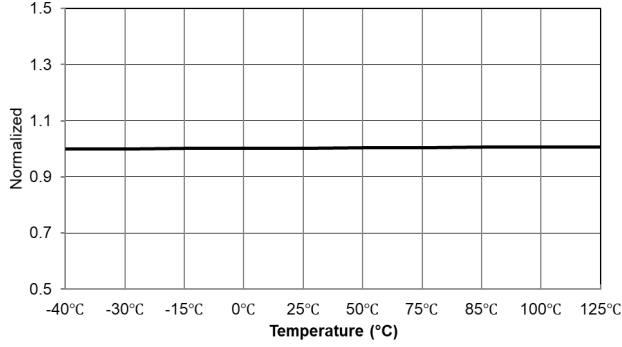


Fig. 1. V<sub>DD\_ON</sub>

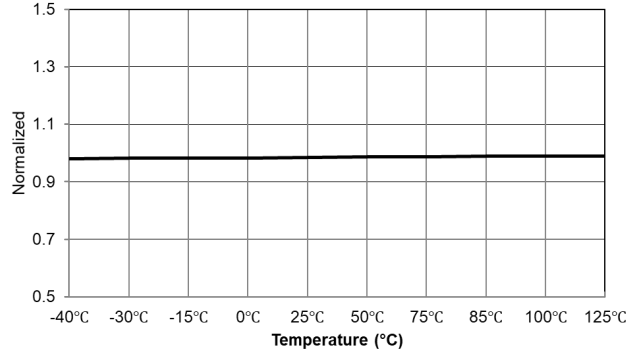


Fig. 2. V<sub>DD\_UVLO</sub>

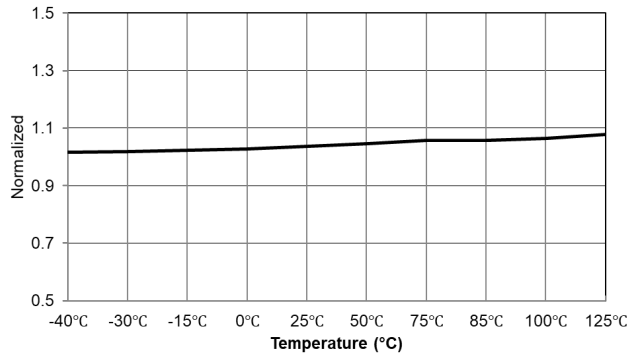


Fig. 3. V<sub>DD\_OVP</sub>

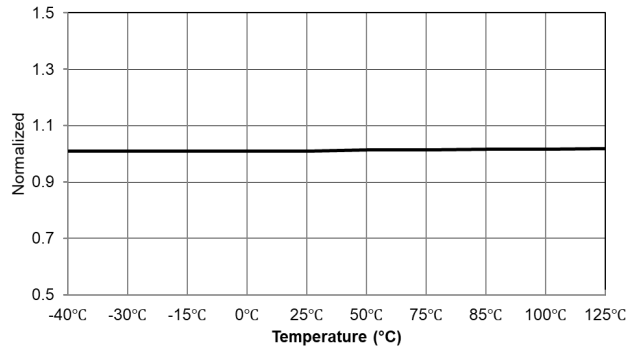


Fig. 4. f<sub>s\_TMO</sub>

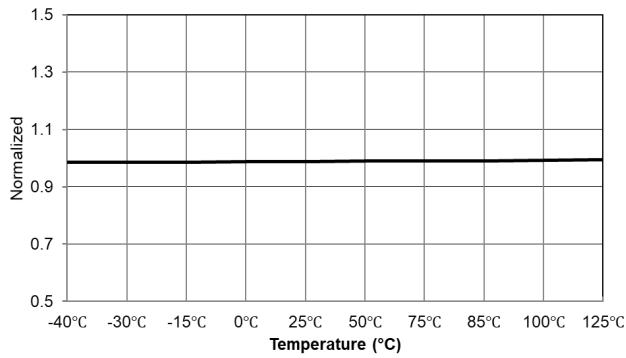


Fig. 5. V<sub>FB\_BST\_ENT</sub>

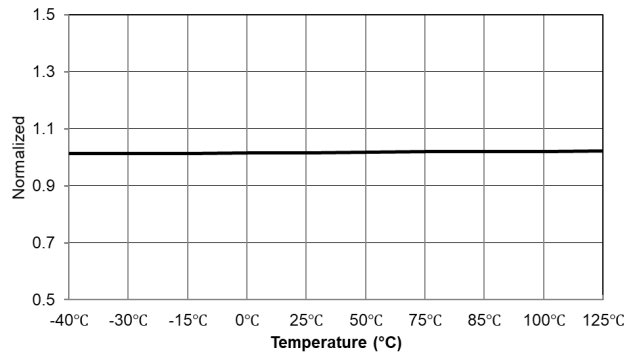


Fig. 6. V<sub>FB\_BST\_EXT</sub>

**Characteristic Graphs (cont.)**

( $T_C = -40$  to  $125$  °C unless otherwise specified)

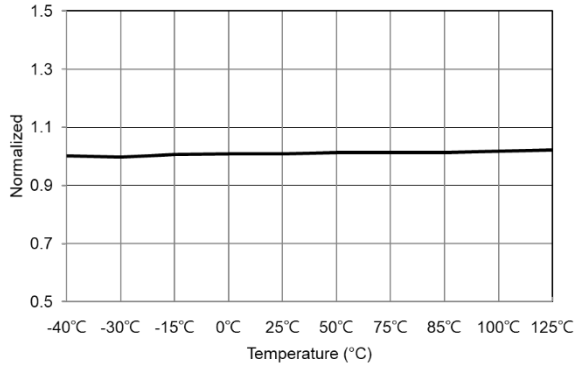


Fig. 7. IdMAG\_BRI

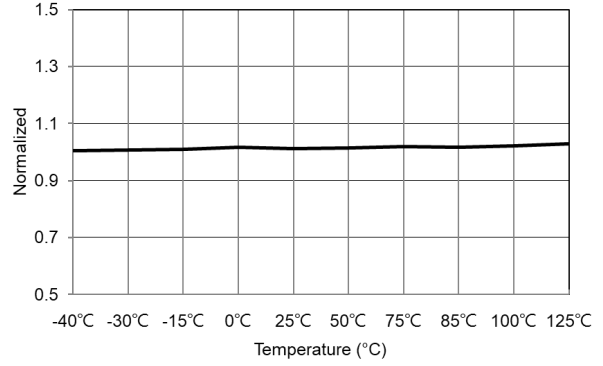


Fig. 8. IdMAG BRO

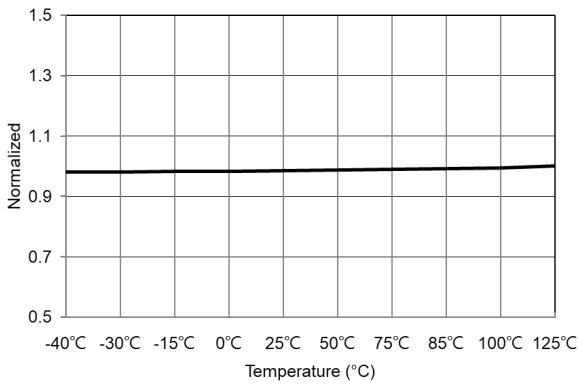


Fig. 9. VDMAG\_UVP

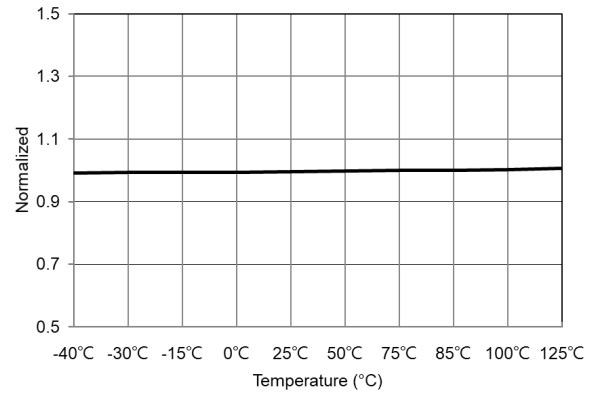


Fig. 10. VDMAG\_OVP

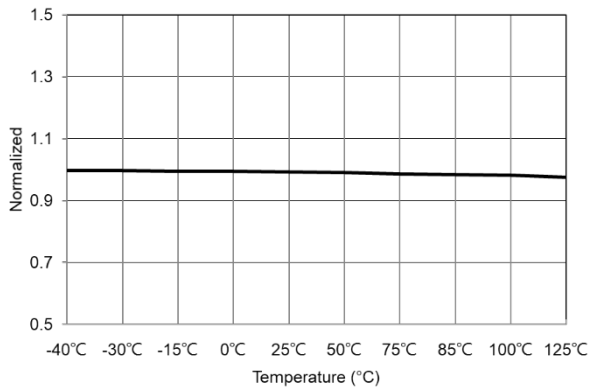


Fig. 11. Vcs\_LIM\_H

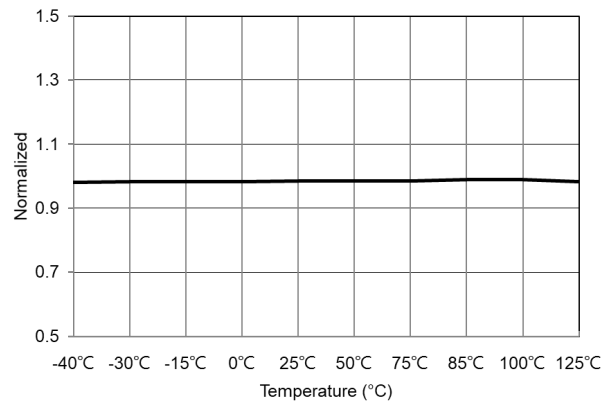


Fig. 12. VTH\_SD

**Characteristic Graphs (cont.)**

(GaN PowerFET,  $T_C = 25\text{ }^\circ\text{C}$  unless otherwise specified)

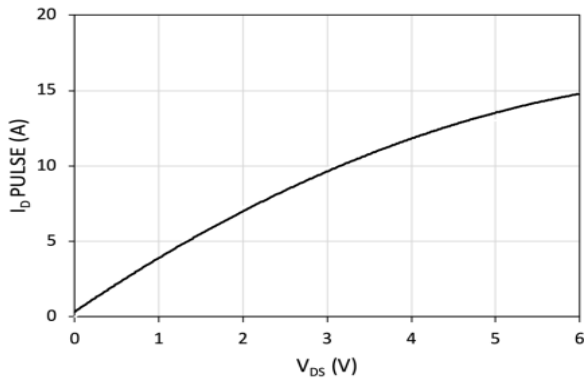


Fig. 13. Pulsed Drain current ( $I_D$  PULSE) vs. drain-to-source voltage ( $V_{DS}$ ) at  $T = 25\text{ }^\circ\text{C}$

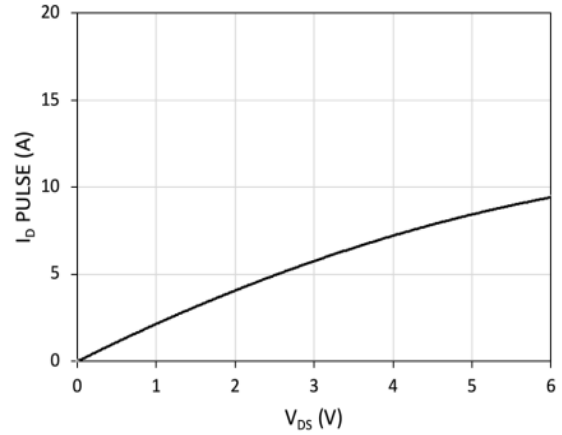


Fig. 14. Pulsed Drain current ( $I_D$  PULSE) vs. drain-to-source voltage ( $V_{DS}$ ) at  $T = 125\text{ }^\circ\text{C}$

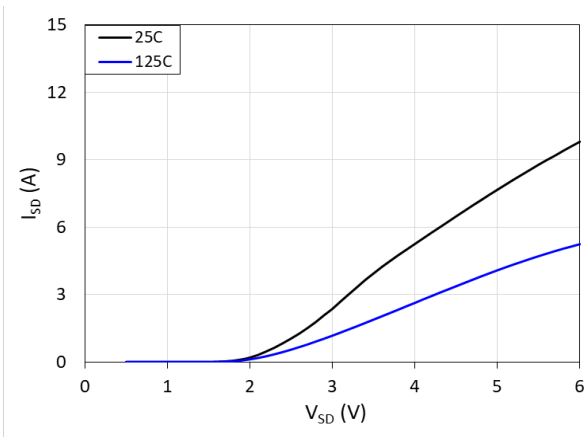


Fig.15. Source-to-drain reverse conduction voltage

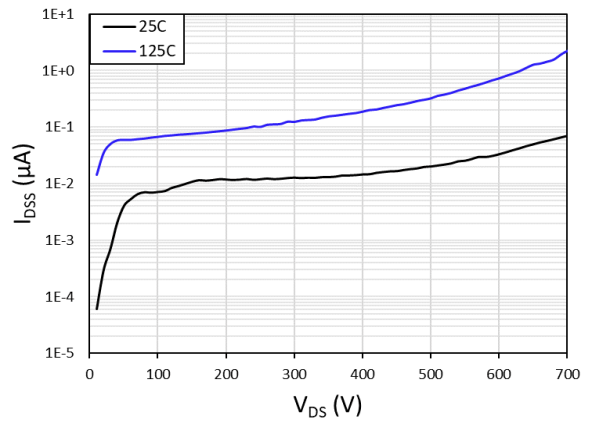


Fig.16. Drain-to-source leakage current ( $I_{DSS}$ ) vs. drain-to-source voltage ( $V_{DS}$ )

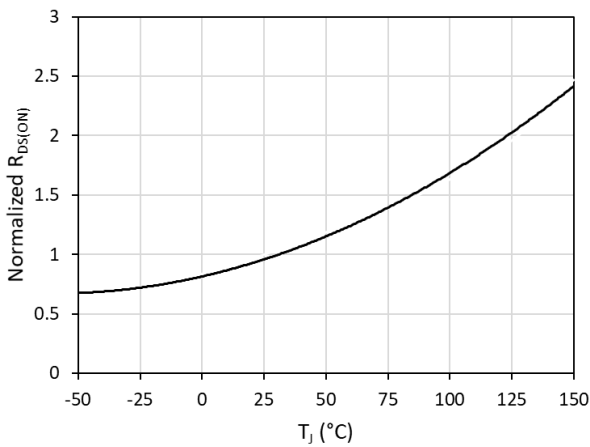


Fig.17. Normalized on-resistance ( $R_{DS(ON)}$ ) vs. junction temperature ( $T_J$ )

**Characteristic Graphs (Cont.)**

(GaN Power FET,  $T_C = 25\text{ }^\circ\text{C}$  unless otherwise specified)

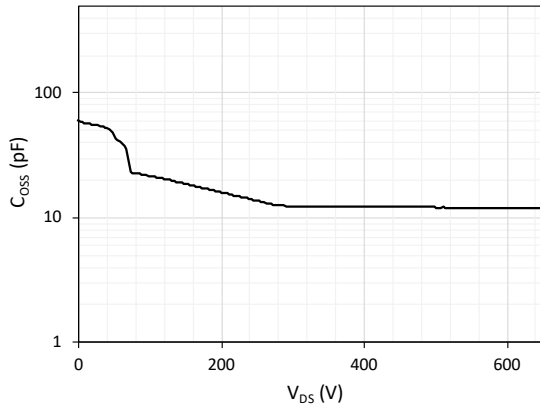


Fig.18. Output capacitance ( $C_{OSS}$ ) vs. drain-to-source voltage ( $V_{DS}$ )

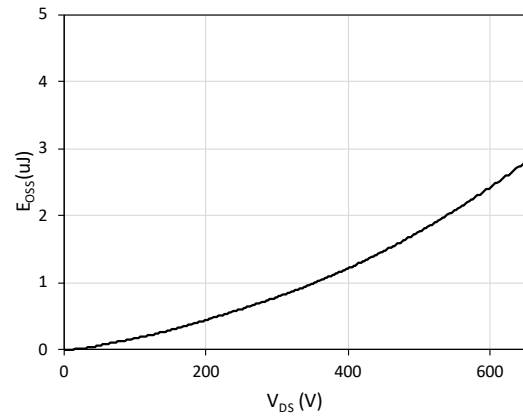


Fig.19. Energy stored in output capacitance ( $E_{OSS}$ ) vs. drain-to-source voltage ( $V_{DS}$ )

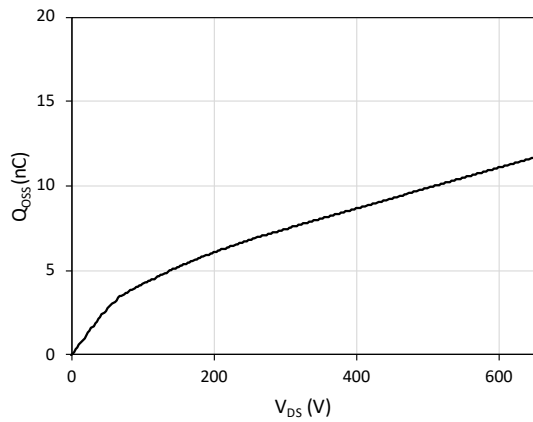


Fig.20. Charge stored in output capacitance ( $Q_{OSS}$ ) vs. drain-to-source voltage ( $V_{DS}$ )



9.

**9. Pin Configurations and Marking Diagram**

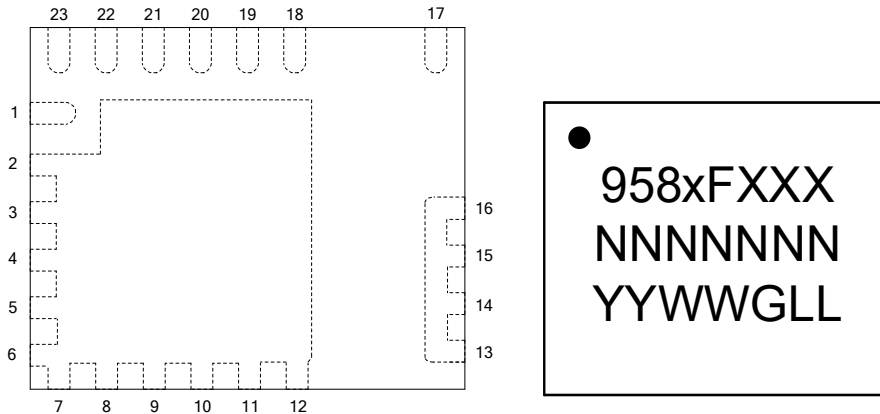


Fig. 21. Pin Configuration (Top View)

Symbol	Content
x	Device Code, 0=NV9582, 1=NV9581, 2=NV9582, 3=NV9583...etc.
F	Package Code, F=QFN
XXX	Trim Option Code
NNNNNN	Lot Number
YY	Year Code
WW	Week Code
G	Manufacture Code
LL	Trace Code

Pin No.	Name	Description
2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, PAD	PGND	<b>Power Ground.</b> Source of Power FET. Metal pad on bottom of package.
1	CS	<b>Current Sense.</b> This pin detects the integrated GaN sense FET current cycle by cycle when connected to a current-sense resistor. There is a current ratio between $I_{drain}$ and $I_{cs}$
13, 14, 15, 16	Drain	<b>Drain of GaN Power FET.</b> This pin is also connected internally to the high-voltage startup circuit for NV9580/82/84 devices.
17	HV	<b>High Voltage Startup.</b> This pin is the input for high voltage startup for NV9581/83 devices. This pin is open for NV9580/82/84 devices (see Drain pin description).
18	VREG	<b>LDO Output.</b> Typically, this pin is connected to an external capacitor with recommended value = 100nF to 1uF.
19	VDD	<b>Power Supply.</b> IC operation current and GaN FET driving current are supplied through this pin. Typically, this pin is connected to external $V_{DD}$ capacitor. The device starts to operate when $V_{DD}$ exceeds $V_{DD\_ON}$ .
20	FB	<b>Feedback.</b> Input for the internal PWM comparator.
21	SD	<b>Shut Down.</b> Typically, this pin is connected to a NTC thermistor. The device enters the fault mode if the voltage on this pin is pulled below the fault thresholds.
22	AGND	<b>Analog GND</b>
23	DMAG	<b>Demagnetization Sense.</b> This pin is used to detect resonant valleys for QR switching. It also detects the output voltage information, as well as the input voltage information for Brown-in & Brown-out protection.

## 10. Functional Description

The following functional description contains additional information regarding the IC operating modes and pin functionality.

### Basic Operation

NV958x family ICs are offline flyback regulator which operate in frequency limit quasi-resonant (QR) mode to reduce switching losses and EMI (electromagnetic interference). It regulates the output based on the load condition through feedback circuitry.

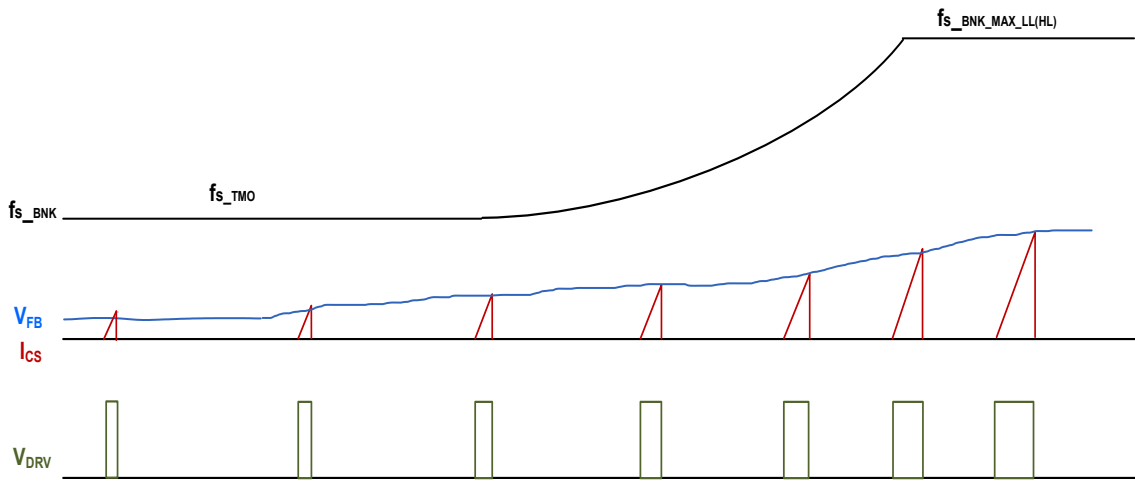
The QR resonant frequency is determined by the transformer primary inductance ( $L_p$ ) and the primary side GaN FET effective output capacitance ( $C_{oss-eff}$ ).

$$C_{oss-eff} = C_{oss-GaN FET} + C_{parasitic} + C_{transformer} \quad \text{(Equation 1)}$$

$$t_{resonance} = 2\pi \sqrt{L_p \times C_{oss-eff}} \quad \text{(Equation 2)}$$

In a general 958x design, at no load or light load condition, the frequency limit  $f_{S\_BNK}$  for the pulse to pulse operating frequency is  $f_{S\_TMO}$ . So operating frequency is between  $f_{S\_TMO}$  and  $1/(1/f_{S\_TMO} + t_{resonance})$ . At the medium load condition (e.g. 25%~50% of full load), the frequency limit  $f_{S\_BNK}$  is modulated as a function of load condition such that it varies between  $f_{S\_TMO}$  and  $f_{S\_BNK\_MAX\_LL(HL)}$  as load varies. At the heavy load condition (e.g. 50%~100% of full load),  $f_{S\_BNK}$  is fixed at  $f_{S\_BNK\_MAX\_LL(HL)}$  such that the switching frequency is not higher than  $f_{S\_BNK\_MAX\_LL(HL)}$  as shown in Figure 22.

NV958x family ICs also have option to operate in CCM at low line. When the device enters CCM, the maximum CCM frequency limit is  $f_{S\_BNK\_MAX\_CCM}$ .



**Figure 22 Frequency Fold-Back Operation**

### Burst Mode

As shown in Figure 23, when feedback voltage  $V_{FB}$  drops below  $V_{FB\_BST\_ENT}$  at light load, the PWM output shuts off and the output voltage drops at a rate depending on the load current level. Thereafter, feedback voltage  $V_{FB}$  rises. Once  $V_{FB}$  exceeds  $V_{FB\_BST\_EXT}$ , NV958x family products resume switching and the switch peak currents is limited by  $V_{CS\_MIN}$ . If more power is delivered to the load than required,  $V_{FB}$  voltage will decrease. Once  $V_{FB}$  voltage is pulled below  $V_{FB\_BST\_ENT}$ , switching stops again. In this manner, the burst mode operation alternately enables and disables switching of the GaN FET to regulate the output and in the meanwhile reduce the switching losses.

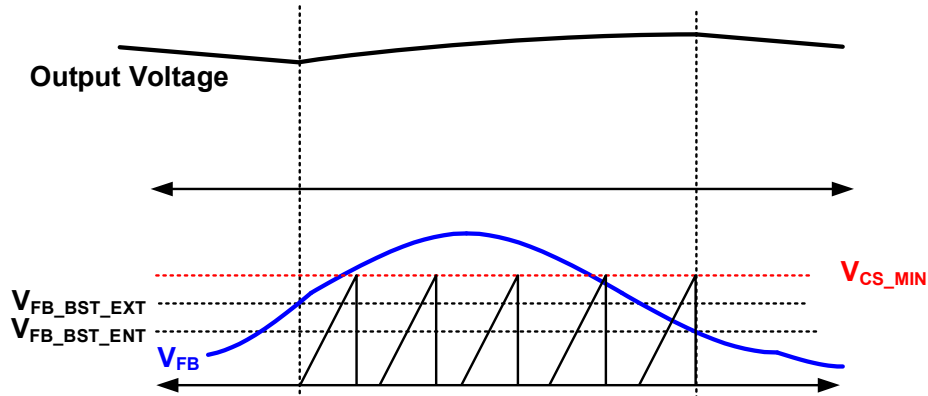


Figure 23 Burst Mode Operation

### Deep Green Mode

NV958x family ICs enter the deep green mode if  $V_{FB}$  voltage stays below  $V_{FB\_BST\_ENT}$  for more than  $t_{D\_DPGN}$ . In the deep green mode, the IC operating current is reduced to  $I_{DD\_DPGN}$  to minimize power consumption. IC resumes switching with normal operating current  $I_{DD\_OP}$  once  $V_{FB}$  voltage rises above  $V_{FB\_BST\_EXT}$ .

### Valley Detection

NV958x family valley detection is achieved by monitoring  $V_{DMAG}$  voltage, which is the divided auxiliary winding voltage by  $R_{DMAG1}$  and  $R_{DMAG2}$  as shown in Figure 24. One ceramic capacitor ( $C_{DMAG}$ ) with typical value 10pF (and not bigger than 22pF) is recommended to filter out the noise if there is PCB noise coupling concern.

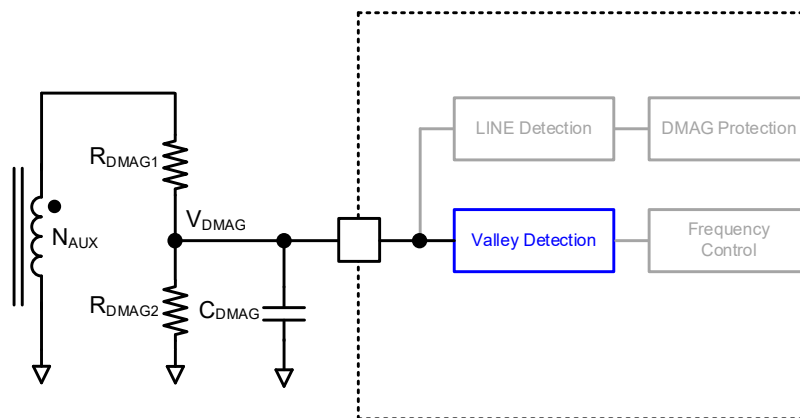


Figure 24 Valley Detection Circuit

### Inherent Frequency Jitter

In flyback application, the DC ripple ( $\Delta V_{DC}$ ) of bulk capacitor at the low line application is larger than at the high line application as shown in Figure 25. This large DC ripple will result in switching frequency variation for a valley switched converter. The frequency variation scatters EMI noise over the nearby frequency band, allowing compliance with EMI requirement easily. Therefore, the EMI performance at the low line application is easy to comply with EMI limitation naturally. However, at the high line application, the DC ripple is relatively small and consequently the EMI performance may suffer. To maintain good EMI performance across over the universal input, a frequency jitter is implemented in the NV958x family products.

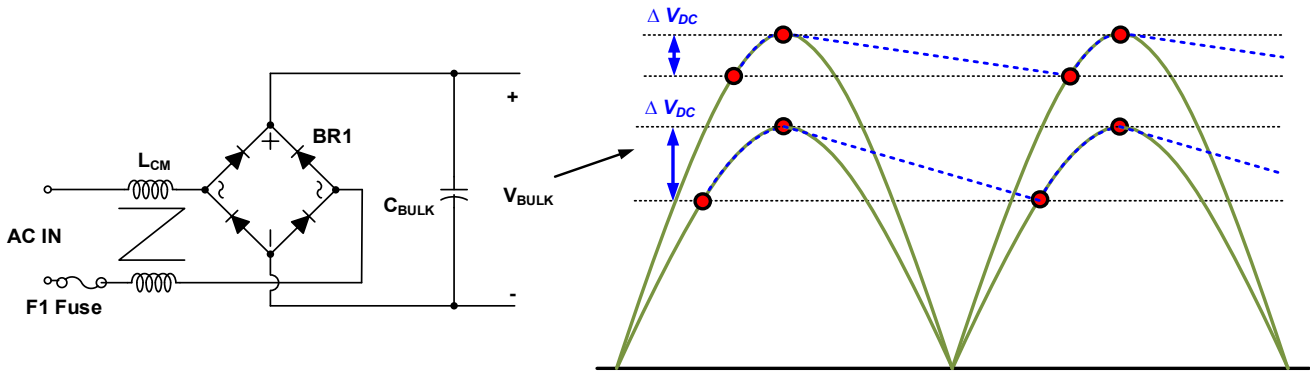


Figure 25 Inherent Frequency Jitter

### Output Voltage Detection

NV958x family products detect output voltage through DMAG voltage. Figure 26 shows the DMAG voltage ( $V_{DMAG-S/H}$ ) is sampled at the end of  $t_{DMAG\_BNK}$  to avoid sampling error. The DMAG voltage is set based on the transformer turn ratio, the voltage divider resistors  $R_{DMAG1}$  &  $R_{DMAG2}$ . The ratio ( $Ratio_{DMAG}$ ) between  $V_{DMAG-S/H}$  and  $V_o$  can be defined as :

$$Ratio_{DMAG} = \frac{V_{DMAG-S/H}}{V_o} = \frac{N_A}{N_S} \times \frac{R_{DMAG2}}{R_{DMAG1} + R_{DMAG2}} \quad (\text{Equation 3})$$

$Ratio_{DMAG}$  is required to be designed to guarantee  $V_o$  nominal operation will not hit protections, i.e.,  $V_{DMAG-S/H}$  will not hit either  $V_{DMAG-OVP}$  or  $V_{DMAG-UVP}$  described in protection section. For USB-PD/PPS application, a typical recommended  $Ratio_{DMAG}$  design is 0.16.

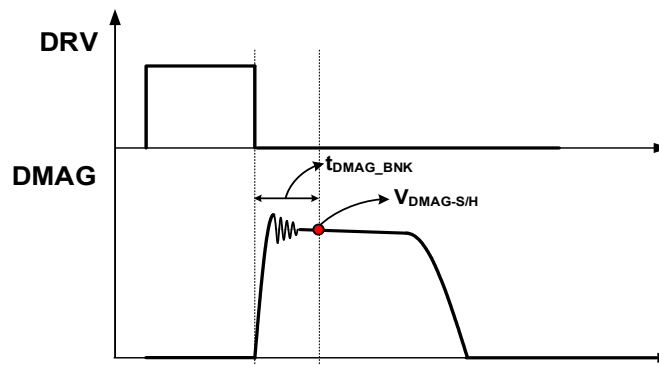


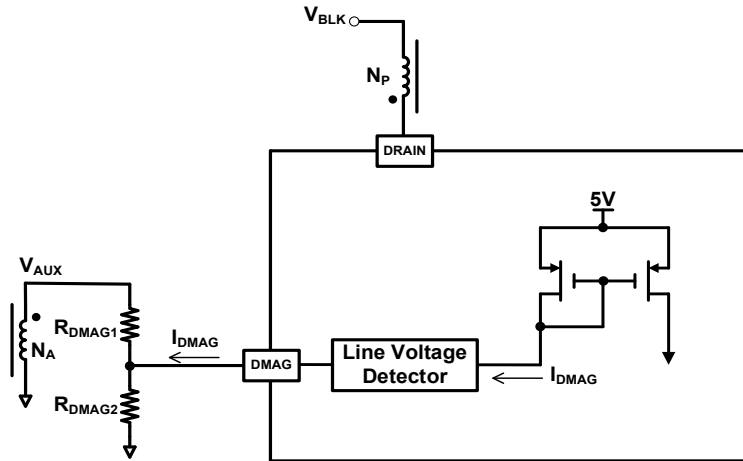
Figure 26 Output Voltage Detection

## Line Voltage Detection

As illustrated in Figure 27, NV958x family products indirectly sense the line voltage through DMAG pin during GaN FET turn-on period. During the GaN FET conduction time, the line voltage detector clamps DMAG pin voltage at 0V. The auxiliary winding voltage,  $V_{AUX}$ , is proportional to the input bulk capacitor voltage,  $V_{BLK}$ . So current  $I_{DMAG}$  flowing out of DMAG pin is expressed as:

$$I_{DMAG} = \frac{V_{BLK}}{R_{DMAG1}} \times \frac{N_A}{N_P} \quad (\text{Equation 4})$$

$I_{DMAG}$  current, reflecting the line voltage information, is used for the brown-in and brown-out protection.



**Figure 27 Line Voltage Detection Circuit**

## LPS Function

The NV958x family products incorporate built-in circuits to limit output power (PL) and limit output current (CC) in the event of the protocol IC becoming malfunction.

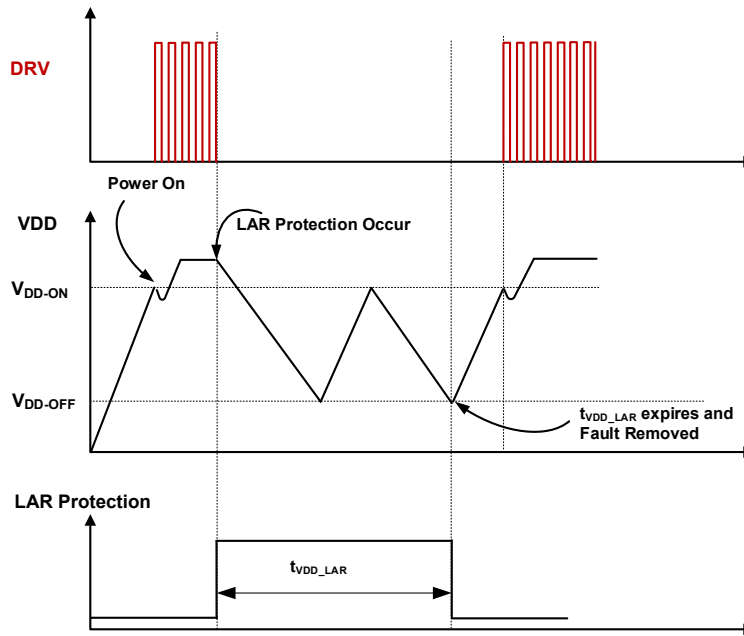
## HV Start-up

During startup, the internal HV startup circuit is enabled and the input voltage supplies the current,  $I_{HV}$ , to charge hold-up capacitor  $C_{VDD}$ . When  $V_{DD}$  voltage reaches  $V_{DD\_ON}$ , the HV startup circuit is disabled. The IC starts PWM switching and senses DMAG signal to check the brown-in condition. If the brown-in is not detected, the IC enters the auto-restart mode. For NV9582 devices, the HV startup circuit is connected to the Drain pin inside and the HV pin is no connection inside.

## Protection Description

NV958x family products protection functions include VDD over-voltage protection (VDD-OVP), Brown-in/out protection, DMAG over-voltage protection (DMAG-OVP), DMAG under-voltage protection (DMAG-UVP), Over load protection (OLP), IC internal over-temperature protection (OTP), IC external thermal shut-down (SD) etc. All protections have auto-restart mode option. The DMAG-OVP and external SD protection can be configured with auto-restart or latch mode. The DMAG-UVP can be configured with auto-restart or long auto-restart mode. The protection function information is provided on page 3.

When the long auto-restart mode protection is triggered, the integrated GaN FET is turned off for a time period of  $t_{VDD\_LAR}$ . After  $t_{VDD\_LAR}$ , if VDD rises above  $V_{DD\_ON}$ , NV958x family products resume normal operation as shown in Figure 28.



**Figure 28 Auto-Restart Long AR Mode**

### VDD-OVP

VDD-OVP prevents IC damage from over voltage stress when abnormal system conditions occur. When VDD voltage exceeds  $V_{DD\_OVP}$  for the debounce time  $t_{D\_VDD\_OVP}$ , the VDD-OVP protection is triggered, the device enters the auto-restart mode.

### Brown-in & Brown-out

The sensed line voltage information is used for the brown-in and brown-out protection. During GaN FET conduction time, when the current,  $I_{DMAG}$ , flowing out of DMAG pin is higher than  $I_{DMAG\_BRI}$  for  $N_{BRI}$  debounce cycles, the brown-in is enabled. The input bulk capacitor voltage level to enable the brown-in is given as

$$V_{BLK\_Brownin} = I_{DMAG\_BRI} \times \frac{R_{DMAG1}}{N_A/N_P} \quad \text{(Equation 5)}$$

When  $I_{DMAG}$  is lower than  $I_{DMAG\_BRO}$  for longer than  $t_{D\_BRO}$ , the brown-out is triggered. The input bulk capacitor voltage level to trigger the brown-out protection is given as

$$V_{BLK\_Brownout} = I_{DMAG\_BRO} \times \frac{R_{DMAG1}}{N_A/N_P} \quad \text{(Equation 6)}$$

### IC Internal OTP

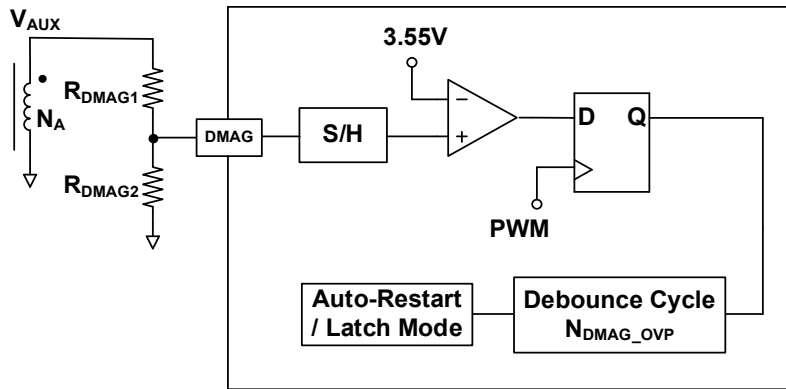
The internal temperature-sensing circuit disables the PWM output if the junction temperature exceeds  $T_{OTP}$ , and the IC enters protection mode.

### DMAG-OVP

DMAG-OVP prevents server system damage when abnormal system conditions occur and cause DMAG voltage rising abnormally. Usually, DMAG over voltage protection is caused by not working properly feedback network (FB) or a fault condition of the DMAG voltage divider resistors. Figure 29 shows the internal circuit of DMAG-OVP. When abnormal system conditions occur and cause DMAG voltage to exceed  $V_{DMAG\_OVP}$  for more than  $N_{DMAG\_OVP}$  consecutive switching cycles, PWM pulses are disabled and the IC enters the auto-restart mode or the latch mode.

For DMAG voltage divider design,  $R_{DMAG1}$  is obtained from Equation 5. With  $Ratio_{DMAG}$  setting or  $V_{O\_OVP}$  (output over voltage protection) setting,  $R_{DMAG2}$  is determined by Equation 3 or Equation 7.

$$V_{O\_OVP} = \frac{V_{DMAG_{OVP}}}{Ratio_{DMAG}} = \frac{N_S}{N_A} \times \left(1 + \frac{R_{DMAG1}}{R_{DMAG2}}\right) \times V_{DMAG_{OVP}} \quad (\text{Equation 7})$$



**Figure 29 DMAG Over Voltage Protection Circuit**

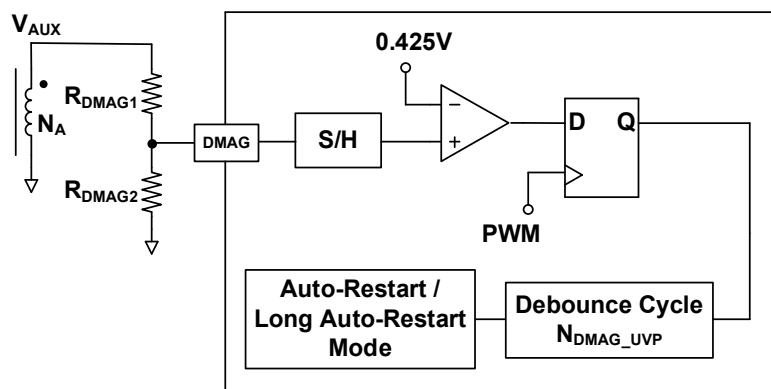
### DMAG-UVP

In the event with shorted output, the output voltage will drop and the primary peak current will increase. To prevent operation for a long time under this condition, NV958x family products incorporate the under voltage protection through DMAG pin (DMAG-UVP). Figure 30 shows the internal circuit for DMAG-UVP. When DMAG voltage is less than  $V_{DMAG\_UVP}$  and longer than de-bounce cycles  $N_{DMAG\_UVP}$ , DMAG UVP is triggered and the IC enters the auto-restart mode or the long auto-restart mode.

The output under voltage protection level,  $V_{O\_UVP}$ , can be determined by Equation 8.

$$V_{O\_UVP} = \frac{V_{DMAG_{UVP}}}{Ratio_{DMAG}} = \frac{N_S}{N_A} \times \left(1 + \frac{R_{DMAG1}}{R_{DMAG2}}\right) \times V_{DMAG_{UVP}} \quad (\text{Equation 8})$$

To avoid DMAG-UVP triggering during the startup sequence, startup blanking time  $t_{V_{DMAG\_UVP\_BNK}}$  is incorporated for system power on.



**Figure 30 DMAG Under Voltage Protection Circuit**



### External Thermal Shut-down

During the startup, when  $V_{DD}$  voltage reaches  $V_{DD\_ON}$ , the shut-down trigger level is set at  $V_{TH\_SD\_STR}$ . After startup, the trigger level is changed to  $V_{TH\_SD}$ . By pulling down SD pin voltage below threshold voltage  $V_{TH\_SD}$ , the shut-down can be triggered externally and the IC will enter the auto-restart or the latch mode as shown in Figure 31. There is an internal constant current source  $I_{SD}$  that is connected to SD pin. So an external OTP function can be implemented by connecting a NTC thermistor between SD pin and ground. The resistance of the NTC thermistor becomes smaller as the ambient temperature increases, therefore the voltage at SD pin will decrease. When the voltage is below the threshold voltage  $V_{TH\_SD}$ , for debounce time of  $t_{D\_SD}$ , the external OTP protection is triggered. A capacitor may also be placed in parallel with the NTC thermistor to further improve the noise immunity.

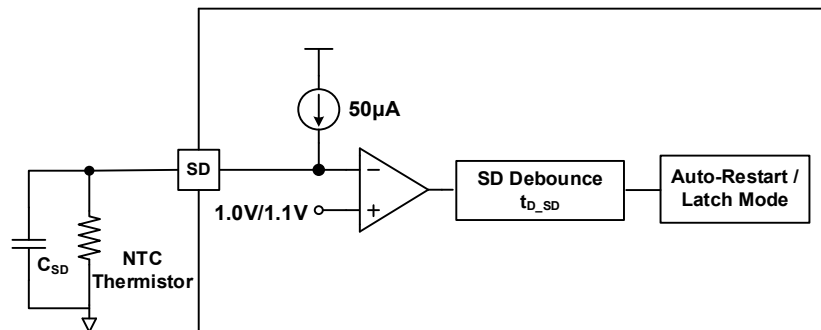


Figure 31 External OTP by SD Pin

### Current Sense Short Protection (CSSP)

NV958x family has CSSP function. When abnormal system conditions occur, in case after debounce time CS pin voltage is still lower than  $V_{CS_{SSP}}$ , the GaN switch turn on time will be limited to limit output power. If this status maintains consecutive  $N_{CS\_CSSP}$  switching cycles, The IC enters auto-restart mode.

### Secondary Side Short Protection (SSSP)

When the secondary-side rectifier is abnormally shorted, the primary-side switch current will increase dramatically within the leading-edge blanking time. To limit the switch current during such conditions, NV958x family products incorporate SSSP function which forces the GaN Switch to turn off when CS pin voltage reaches  $V_{CS\_SSSP}$  after blanking time  $t_{D\_SSSP}$ . If this status maintains consecutive  $N_{CS\_SSSP}$  switching cycle, the IC enters auto-restart mode.

### Over Load Protection (OLP)

NV958x implements overload protection by limiting the maximum duration for operation of overload conditions. The overload timer starts counting when  $V_{FB}$  voltage reaches  $V_{FB\_OLP}$ . If this time is over OLP debounce time  $T_{D\_OLP}$ , OLP protection will be triggered and device will shut down and turn to auto restart mode. If  $V_{FB}$  voltage drops to below  $V_{FB\_OLP}$  before  $T_{D\_OLP}$ , the overload timer will be reset.

### Cycle by Cycle Current Limit

Under certain operation condition, such as the startup or the overload condition, the feedback control loop can be saturated and is unable to control the primary peak current. To limit the current under such conditions, NV958x family products incorporate the cycle by cycle current limit function which forces the GaN switch turn off when CS pin voltage reaches the current limit threshold  $V_{CS\_LIM}$ .



### GaN Power FET Drain-to-Source Voltage Considerations

GaN Power ICs have been designed and tested to provide significant design margin to handle transient and continuous voltage conditions that are commonly seen in single-ended topologies, such as quasi-resonant (QR) flyback applications. The different voltage levels and recommended margins in a typical QR flyback can be analyzed using Fig. 32. When the device is switched off, the energy stored in the transformer leakage inductance will cause  $V_{DS}$  to overshoot to the level of  $V_{SPIKE}$ . The clamp circuit should be designed to control the magnitude of  $V_{SPIKE}$ . After dissipation of the leakage energy, the device  $V_{DS}$  will settle to the level of the bus voltage plus the reflected output voltage which is defined in Fig. 32 as  $V_{DS-OFF}$ .

- For repetitive events, 80% derating should be applied from  $V_{DS(TRAN)}$  rating (800V) to 640V max under the worst case operating conditions.
- It is recommended to design the system such that  $V_{DS-OFF}$  is derated 80% from the  $V_{DS(CONT)}$  (700V) max rating to 560V.
- For half-bridge based topologies, such as LLC,  $V_{DS}$  voltage is clamped to the bus voltage.  $V_{DS}$  should be designed such that it meets the  $V_{DS-OFF}$  derating guideline (560V).
- Non-repetitive events are infrequent, one-time conditions such as line surge, ESD, and lightning. No derating from the  $V_{DS(TRAN)}$  rating (800V) is needed for non-repetitive  $V_{SPIKE}$  durations  $< 100 \mu s$ . The  $V_{DS(TRAN)}$  rating (800V) allows for repetitive events that are  $< 400 ns$ , with 80% derating required (for example repetitive leakage inductance spikes).

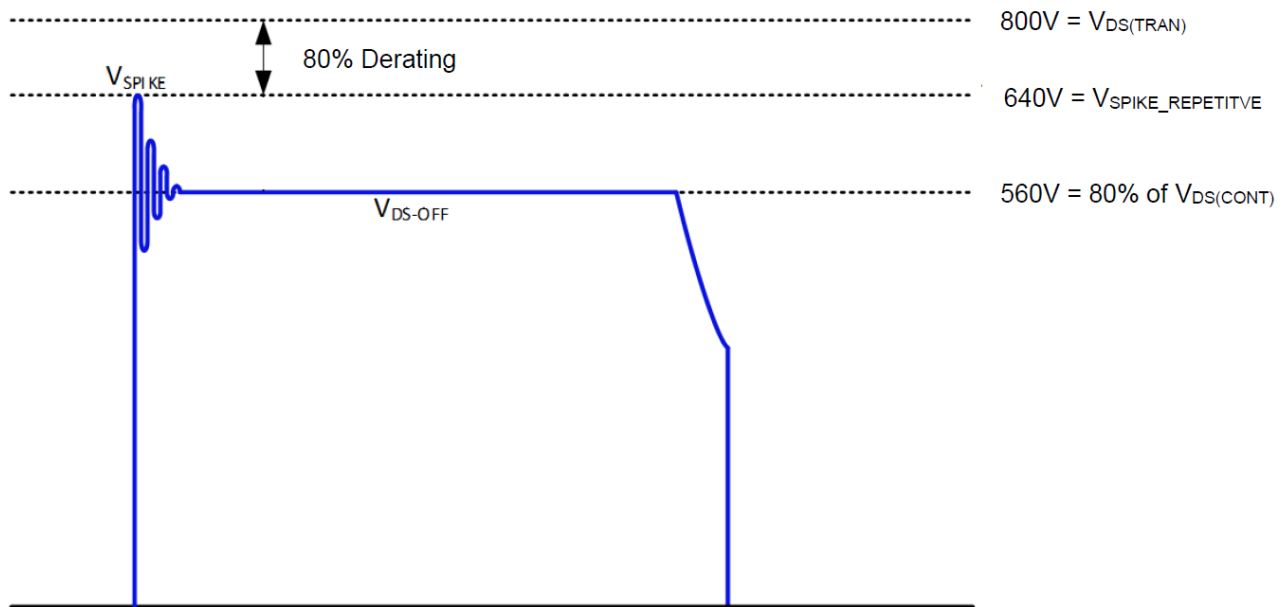
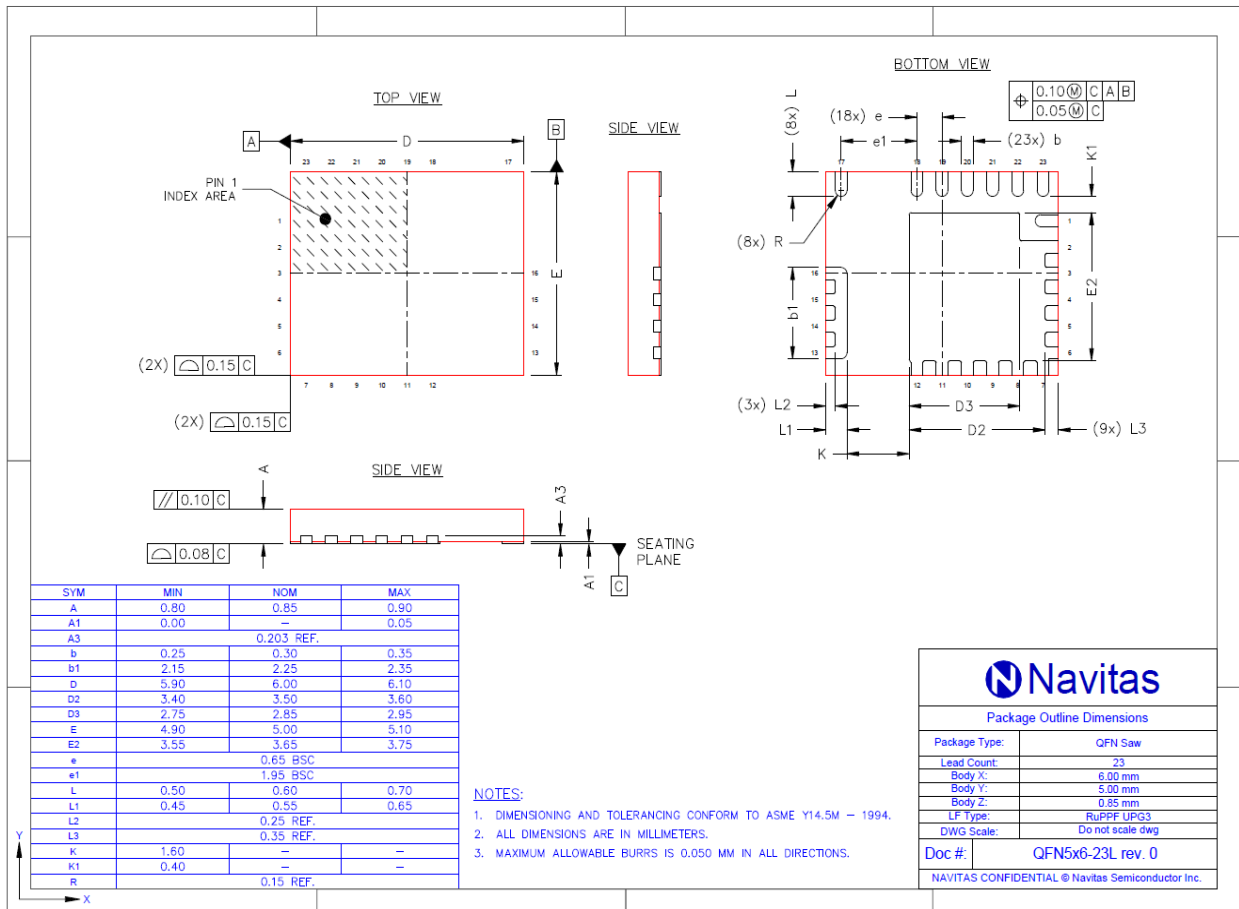


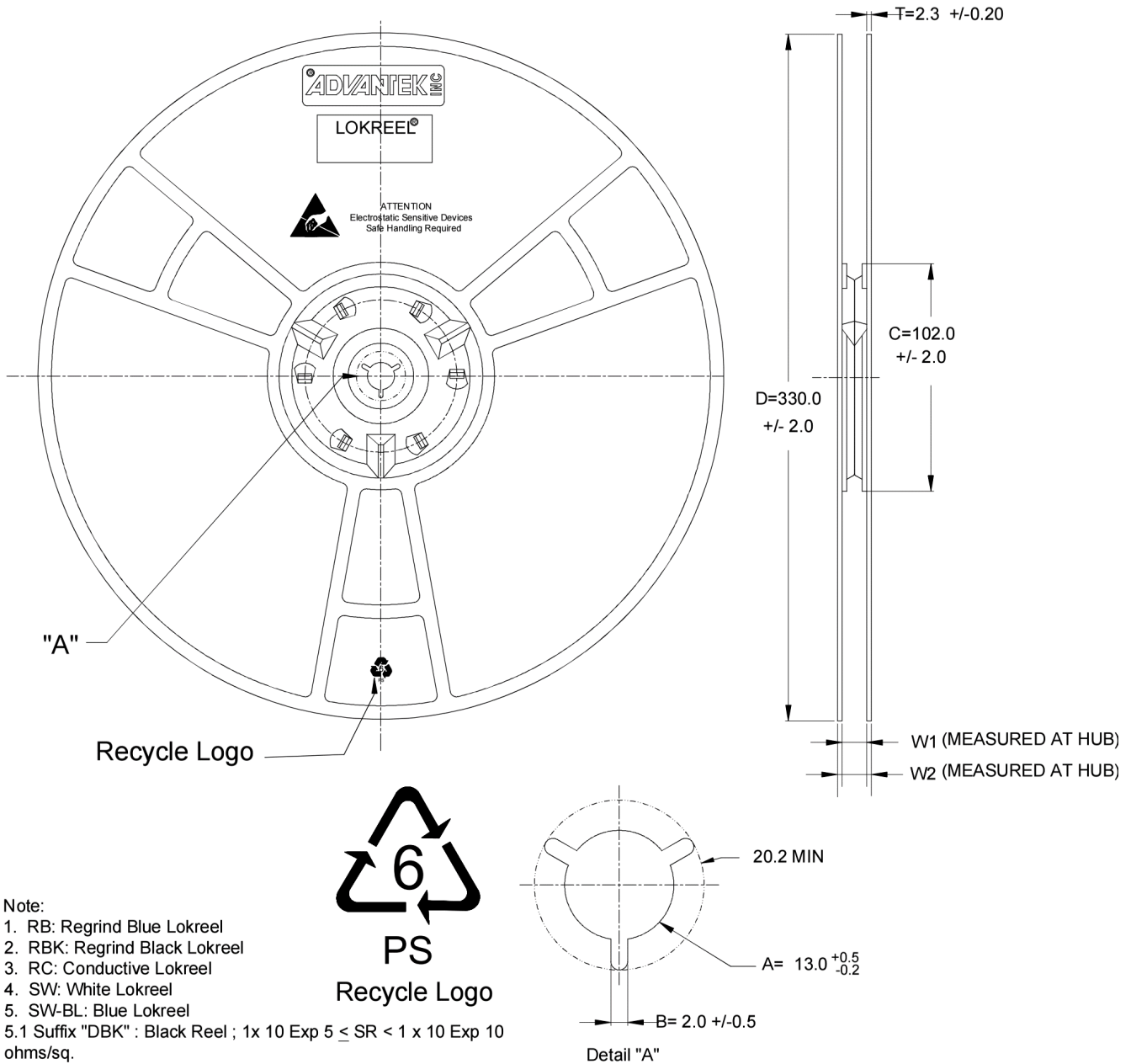
Figure 32 QR flyback drain-to-source voltage stress diagram

**11. Package Outline (Power QFN)**



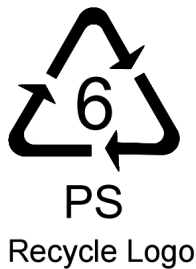
## 12. Tape and Reel Dimensions

-All Dimensions in Millimeters-



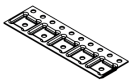
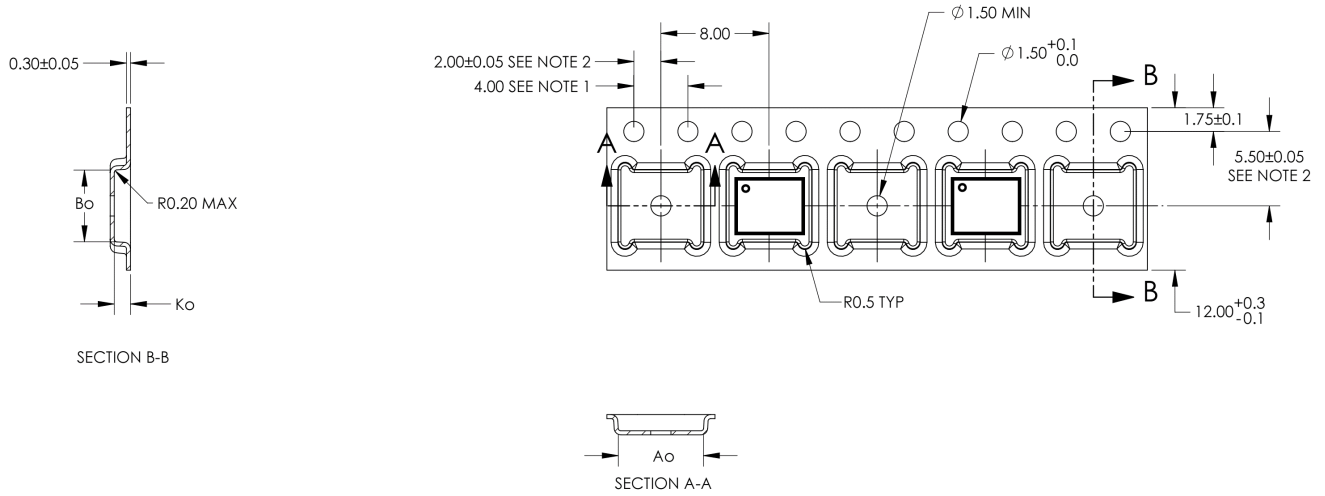
Note:

1. RB: Re grind Blue Lokreel
2. RBK: Re grind Black Lokreel
3. RC: Conductive Lokreel
4. SW: White Lokreel
5. SW-BL: Blue Lokreel
- 5.1 Suffix "DBK": Black Reel ;  $1 \times 10 \text{ Exp } 5 \leq SR < 1 \times 10 \text{ Exp } 10$  ohms/sq.
6. RD Series Lokreel:  $1 \times 10 \text{ Exp } 5 \leq SR < 1 \times 10 \text{ Exp } 12$  ohms/sq.
7. RC Series Lokreel:  $SR < 1 \times 10 \text{ Exp } 5$  ohms/sq.



Nominal Hub Width	W1	W2 MAX
12mm	12.8mm $+1.6 / -0.4$	18.4mm

**13. Tape and Reel Dimensions (Cont.)**



SCALE 1:1

	DIM	±
Ao	6.30	0.1
Bo	5.30	0.1
Ko	1.20	0.1

NOTES:

1. 10 SPROCKET HOLE PITCH CUMULATIVE TOLERANCE ±0.2
2. POCKET POSITION RELATIVE TO SPROCKET HOLE MEASURED AS TRUE POSITION OF POCKET, NOT POCKET HOLE.
3. Ao AND Bo ARE CALCULATED ON A PLANE AT A DISTANCE "R" ABOVE THE BOTTOM OF THE POCKET.

## 14. 20-Year Limited Product Warranty

The 20-year limited warranty applies to all packaged Navitas GaNFast Power ICs and GaNSense HFQR Controllers in mass production, subject to the terms and conditions of, Navitas' express limited product warranty, available at <https://navitassemi.com/terms-conditions>. The warranted specifications include only the MIN and MAX values only listed in Absolute Maximum Ratings and Electrical Characteristics sections of this datasheet. Typical (TYP) values or other specifications are not warranted.



## 15. Revision History

Date	Status	Notes
Oct. 16, 2023	Datasheet	First publication
Dec. 27, 2023	Datasheet	The min and max spec change of $V_{CS\_MIN\_H}$ , $V_{CS\_MIN\_L}$
Feb. 02, 2024	Datasheet	Add $I_{DMAG\_MAX}$ , $V_{DD\_DLCH}$ , $N_{CS\_CSSP}$ in EC table, Optimized the description of GaN Power FET Drain-to-Source Voltage Considerations and functional sections.
Apr. 18, 2024	Datasheet	1. The test current of $R_{DS(ON)}$ and $V_{SD}$ are 2.5A, no change the practical test condition just to correct typos. 2. W2 MAX of Tape and Reel Dimensions to 18.4mm. 3. Updated Abs Max & VDS considerations sections.
Sep.20.2024	Datasheet	Added Sustainability description

## Additional Information

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