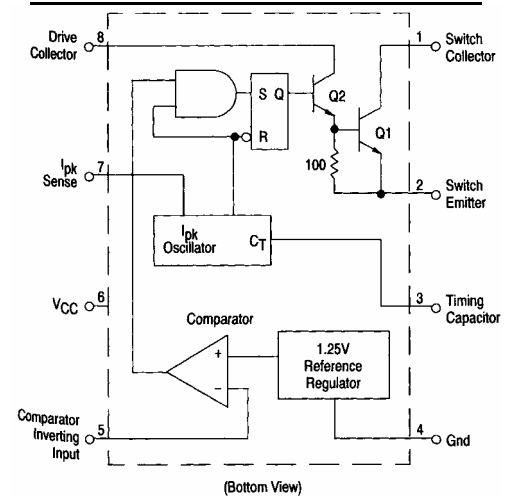


The 34063D is a monolithic control circuit containing the primary functions required for DC-to-DC converters. These devices consist of an internal temperature compensated reference, comparator, controlled duty cycle oscillator with an active current limit circuit, driver and high current output switch. This series was specifically designed to be incorporated in Step-Down and Step-Up and Voltage-Inverting applications with a minimum number of external components.

FEATURES

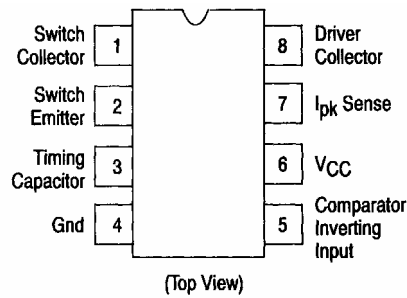
- Operation from 3.0 V to 40 V Input
- Low Standby Current
- Current Limiting
- Output Switch Current to 1.5 A
- Output Voltage Adjustable
- Frequency Operation to 100 kHz
- Precision 2% Reference

FUNCTIONAL BLOCK DIAGRAM



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Voltage	V_{CC}	40	Vdc
Comparator Input Voltage Range	V_{IR}	-0.3 to +40	Vdc
Switch Collector Voltage	$V_{C(\text{switch})}$	40	Vdc
Switch Emitter Voltage ($V_{pin 1} = 40\text{ V}$)	$V_{E(\text{switch})}$	40	Vdc
Switch Collector to Emitter Voltage	$V_{CE(\text{switch})}$	40	Vdc
Driver Collector Voltage	$V_{C(\text{driver})}$	40	Vdc
Driver Collector Current (Note 1)	$I_{C(\text{driver})}$	100	mA
Switch Current	I_{SW}	1.5	A
Power Dissipation and Thermal Characteristics			
Plastic Package, P Suffix $T_A = +25^\circ\text{C}$	P_D	1.25	W
Thermal Resistance	$R_{\theta JA}$	100	$^\circ\text{C/W}$
SOIC Package, D Suffix $T_A = +25^\circ\text{C}$	P_D	625	mW
Thermal Resistance	$R_{\theta JA}$	160	$^\circ\text{C/W}$
Operating Junction Temperature	T_J	+150	$^\circ\text{C}$
Operating Ambient Temperature Range	T_A	0 to +70	$^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65to+150	$^\circ\text{C}$



ELECTRICAL CHARACTERISTICS

($V_{CC} = 5.0\text{ V}$, $T_A = 0$ to $+70^\circ\text{C}$ unless otherwise specified.)

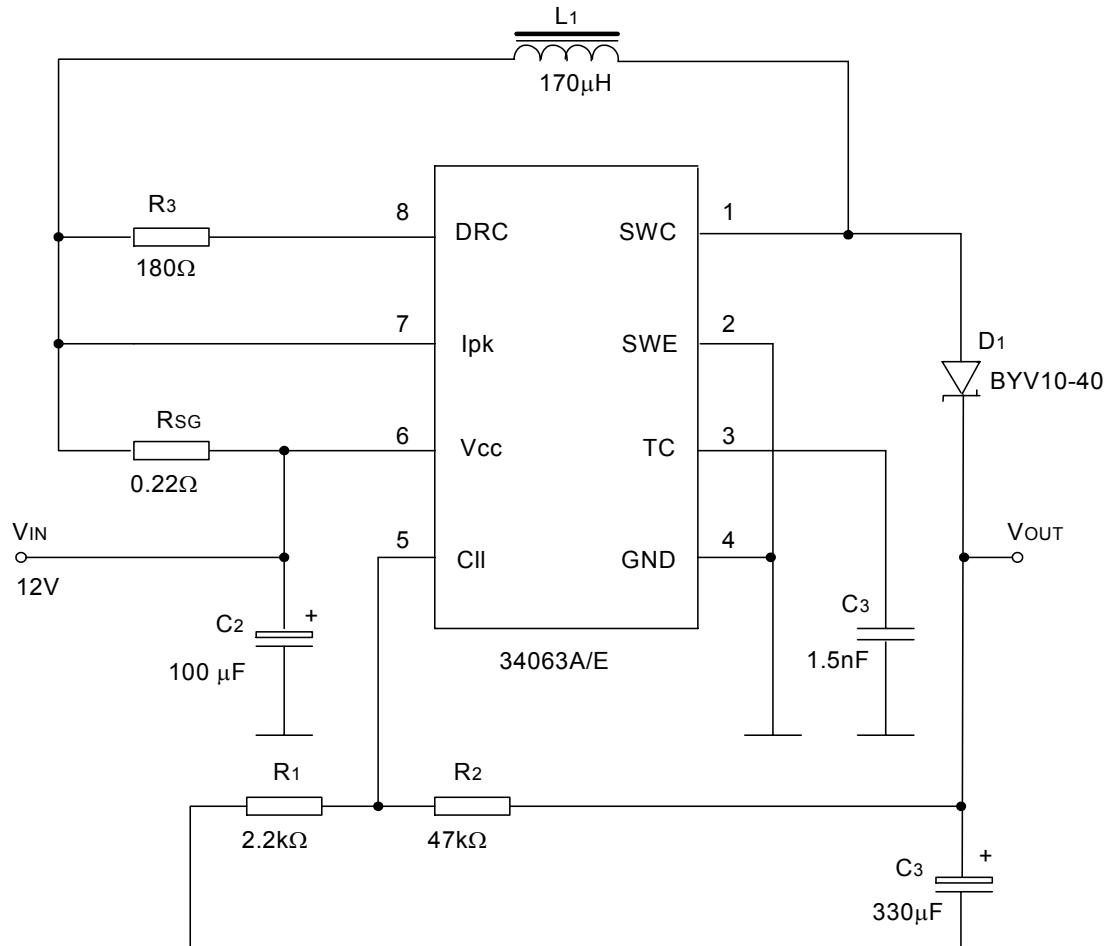
Characteristics	Symbol	Min	Max	Unit
OSCILLATOR				
Frequency ($V_{Pin5} = 0\text{ V}$, $C_T = 1.0\text{ nF}$, $T_A = 25^\circ\text{C}$)	fosc	24	42	kHz
Charge Current ($V_{CC} = 5.0\text{ V to }40\text{ V}$, $T_A = 25^\circ\text{C}$)	Ichg	24	42	μA
Discharge Current ($V_{CC} = 5.0\text{ V to }40\text{ V}$, $T_A = 25^\circ\text{C}$)	Idischg	140	260	μA
Discharge to Charge Current Ratio (Pin7 to Vcc, $T_A = 25^\circ\text{C}$)	Idischg/Ichg	5.2	7.5	—
Current Limit Sense Voltage (Ichg = Idischg, $T_A = 25^\circ\text{C}$)	Vlpk(sense)	250	350	mV
OUTPUT SWITCH (Note 3)				
Saturation Voltage, Darlington Connection ($I_{SW} = 1.0\text{ A}$, Pins 1, 8 connected)	$V_{CE(sat)}$	—	1.3	V
Saturation Voltage ($I_{SW} = 1.0\text{ A}$, $R_{Pin8} = 82\ \Omega$ to V_{CC} , Forced $\beta = 20$)	$V_{CE(sat)}$	—	0.7	V
DC Current Gain ($I_{SW} = 1.0\text{ A}$, $V_{CE} = 5.0\text{ V}$, $T_A = 25^\circ\text{C}$)	h_{FE}	50	—	—
Collector Off-State Current ($V_{CE} = 40\text{ V}$)	$I_C(off)$	—	100	μA
COMPARATOR				
Threshold Voltage ($T_A = 25^\circ\text{C}$) ($T_A = T_{LOW}$ to T_{HIGH})	Vth	1.225 1.21	1.275 1.29	V
Threshold Voltage Line Regulation ($V_{CC} = 3.0\text{ V to }40\text{ V}$)	Regline	—	5.0	mV
Input Bias Current ($V_{in}=0\text{ V}$)	I_{IB}	—	-400	nA
TOTAL DEVICE				
Supply Current ($V_{CC} = 5.0\text{ V to }40\text{ V}$, $C_T = 1.0\text{ nF}$, $V_{pin7} = V_{CC}$, $V_{pin5} > V_{th}$, Pin 2 = Gnd, Remaining pins open)	I_{CC}	—	4.0	mA

NOTES:

- Maximum package power dissipation limits must be observed.
- Low duty cycle pulse techniques are used during test to maintain Junction temperature as close to ambient temperature as possible
- If the output switch is driven into hard saturation (non Darlington configuration) at low switch currents (< 300 mA) and high driver currents (>30 mA), it may take up to 2.0 μs to come out of saturation This condition will shorten the off time at frequencies > 30 kHz, and is magnified at high temperatures This condition does not occur with a Darlington configuration, since the output switch cannot saturate If a non Darlington configuration is used, the following output drive condition is recommended
Forced β of output switch = $I_C, output / (I_C, driver - 7.0\text{ mA}^*) > 10$
*The 100 Ω . resistor in the emitter of the driver device requires about 7.0 mA before the output switch conducts

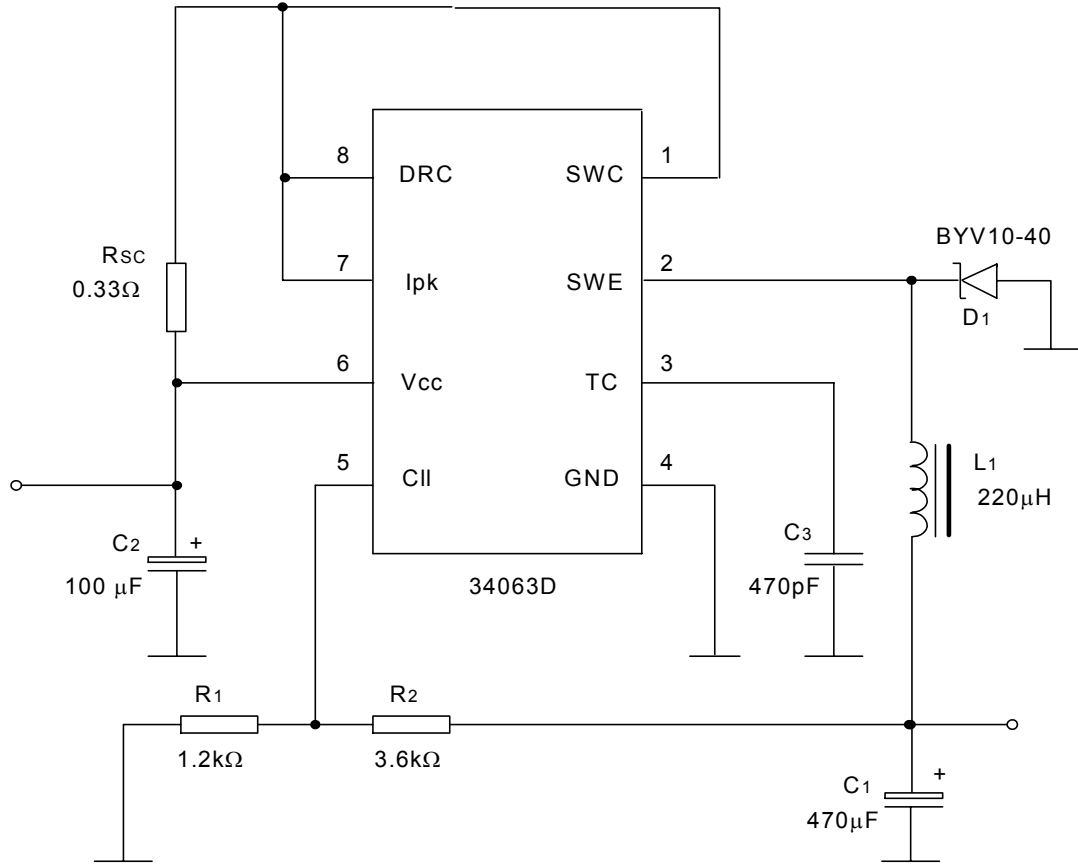
TYPICAL APPLICATION CIRCUIT

Step-Up Converter


 Test Condition ($V_{OUT} = 28\text{ V}$)

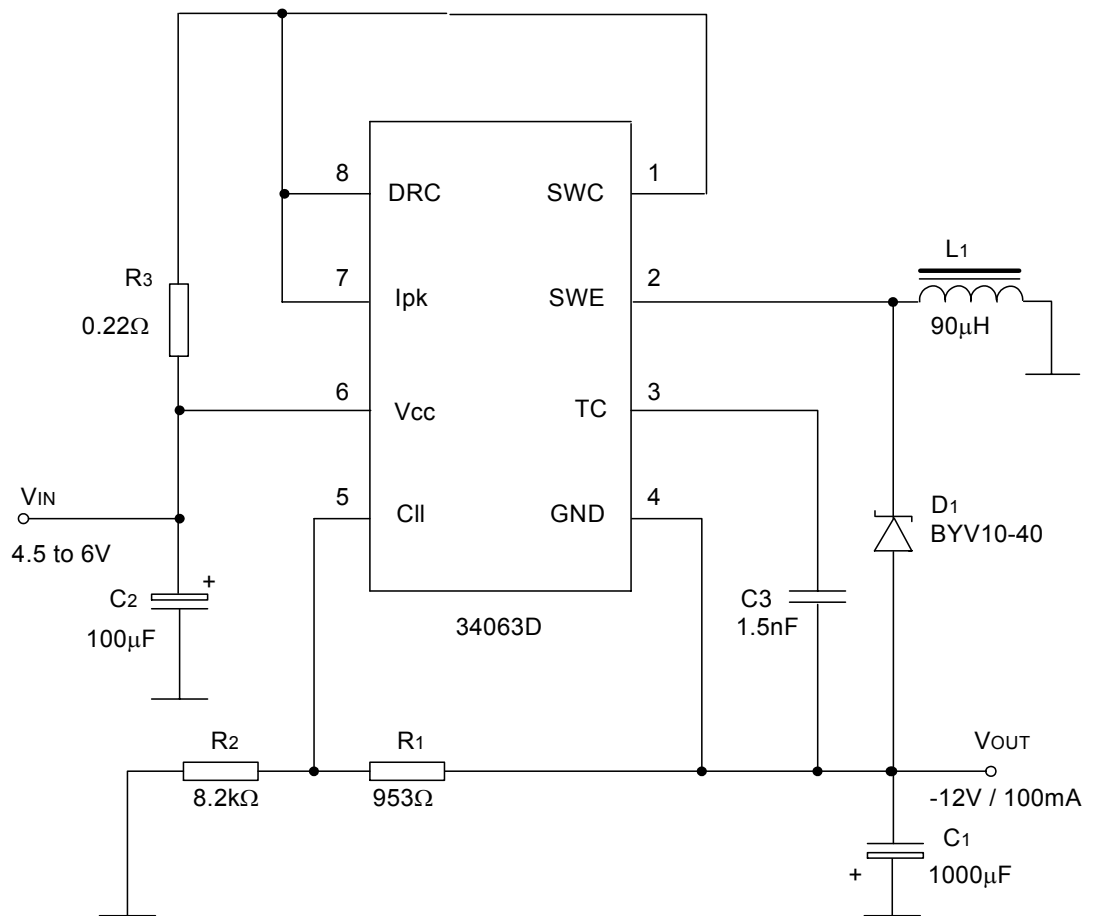
Test	Conditions	Value (Typ)	Unit
Line Regulation	$V_{IN} = 8\text{ to }16\text{ V}$, $I_O = 175\text{ mA}$	30	mV
Load Regulation	$V_{IN} = 12\text{ V}$, $I_O = 75\text{ to }175\text{ mA}$	10	mV
Output Ripple	$V_{IN} = 12\text{ V}$, $I_O = 175\text{ mA}$	400	mV
Efficiency	$V_{IN} = 12\text{ V}$, $I_O = 175\text{ mA}$	87.7	%

Step-Down Converter


 Test Condition ($V_{OUT} = 5V$)

Test	Conditions	Value (Typ)	Unit
Line Regulation	$V_{IN} = 15$ to $25V$, $I_O = 500mA$	12	mV
Load Regulation	$V_{IN} = 25V$, $I_O = 50$ to $500mA$	3	mV
Output Ripple	$V_{IN} = 25V$, $I_O = 500mA$	120	mV
Efficiency	$V_{IN} = 25V$, $I_O = 500mA$	83.7	%
ISC	$V_{IN} = 25V$, $R_{LOAD} = 0.1\Omega$	1.1	A

Voltage Inverting Converter


 Test Condition ($V_{OUT} = -12\text{ V}$)

Test	Conditions	Value (Typ)	Unit
Line Regulation	$V_{IN} = 4.5\text{ to }6\text{ V}$, $I_O = 100\text{ mA}$	3	mV
Load Regulation	$V_{IN} = 5\text{ V}$, $I_O = 10\text{ to }100\text{ mA}$	22	mV
Output Ripple	$V_{IN} = 5\text{ V}$, $I_O = 100\text{ mA}$	500	mV
Efficiency	$V_{IN} = 5\text{ V}$, $I_O = 100\text{ mA}$	62.2	%
ISC	$V_{IN} = 5\text{ V}$, $R_{LOAD} = 0.1\ \Omega$	0.91	A

Calculation

Parameter	Step-Up (Discontinuous mode)	Step-Down (Continuous mode)	Voltage Inverting (Discontinuous mode)
t_{on}/t_{off}	$\frac{V_{out} + V_F - V_{in(min)}}{V_{in(min)} - V_{sat}}$	$\frac{V_{out} + V_F}{V_{in(min)} - V_{sat} - V_{out}}$	$\frac{ V_{out} + V_F}{V_{in} - V_{sat}}$
$(t_{on} + t_{off})_{max}$	$\frac{1}{f_{min}}$	$\frac{1}{f_{min}}$	$\frac{1}{f_{min}}$
C_T	$4.5 \times 10^{-5} t_{on}$	$4.5 \times 10^{-5} t_{on}$	$4.5 \times 10^{-5} t_{on}$
$I_{PK(switch)}$	$2I_{out(max)}[(t_{on}/t_{off}) + 1]$	$2I_{out(max)}$	$2I_{out(max)}[(t_{on}/t_{off}) + 1]$
R_{SC}	$0.3/I_{PK(switch)}$	$0.3/I_{PK(switch)}$	$0.3/I_{PK(switch)}$
C_O	$\equiv \frac{I_{out} t_{on}}{V_{ripple(p-p)}}$	$\frac{I_{PK(switch)} (t_{on} + t_{off})}{8V_{ripple(p-p)}}$	$\equiv \frac{I_{out} t_{on}}{V_{ripple(p-p)}}$
$L(min)$	$\frac{V_{in(min)} - V_{sat}}{I_{PK(switch)}} t_{on(max)}$	$\frac{V_{in(min)} - V_{sat} - V_{out}}{I_{PK(switch)}} t_{on(max)}$	$\frac{V_{in(min)} - V_{sat}}{I_{PK(switch)}} t_{on(max)}$

NOTES:

V_{sat} = Saturation voltage of the output switch

V_F = Forward voltage drop of the output rectifier

THE FOLLOWING POWER SUPPLY CHARACTERISTICS MUST BE CHOSEN:

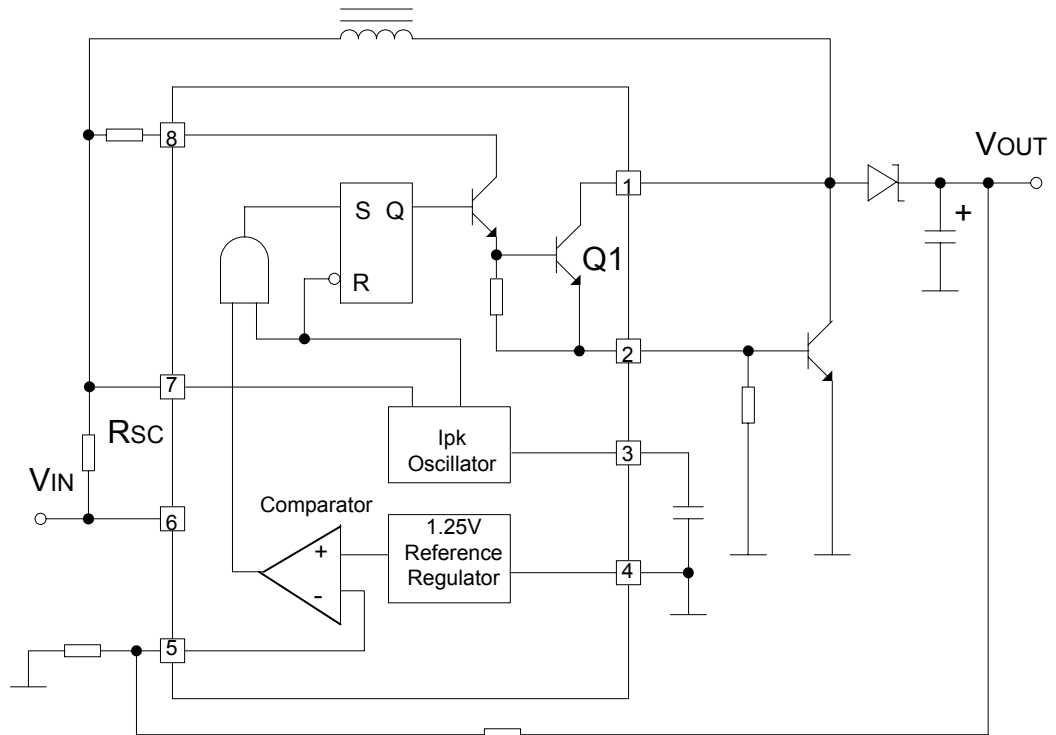
V_{in} = Nominal input voltage

V_{out} = Desired output voltage, $|V_{out}| = 1.25(1 + R_2/R_1)$

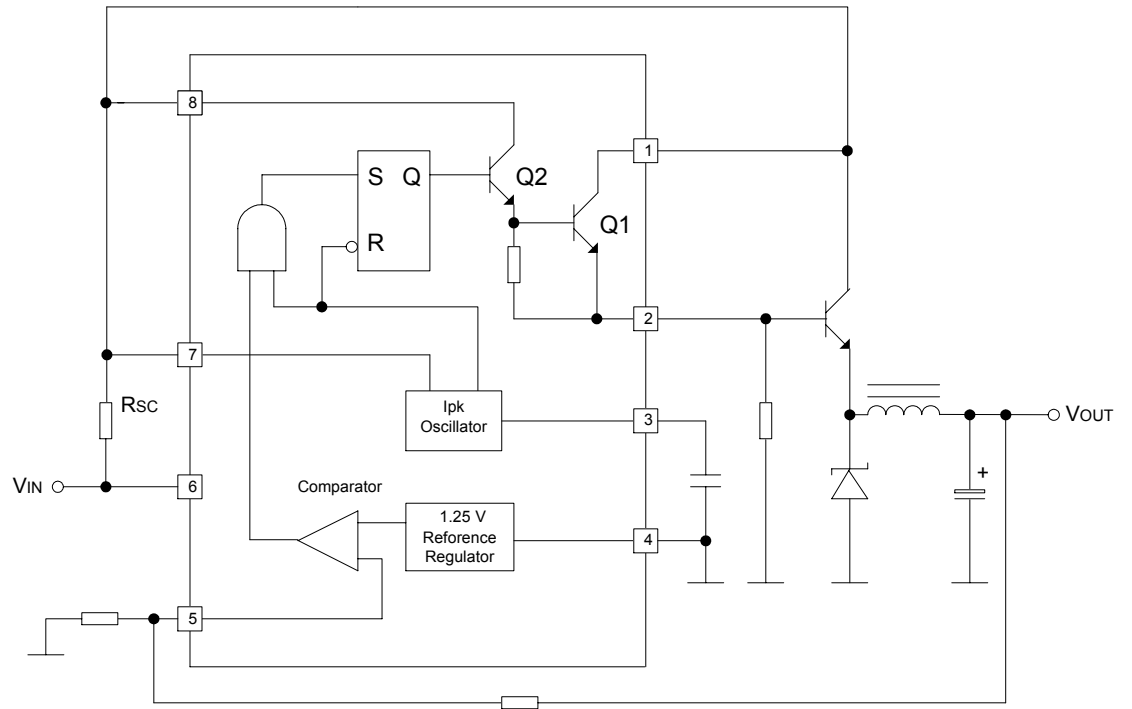
I_{out} = Desired output current

f_{min} = Minimum desired output switching frequency at the selected values of V_{in} and I_o

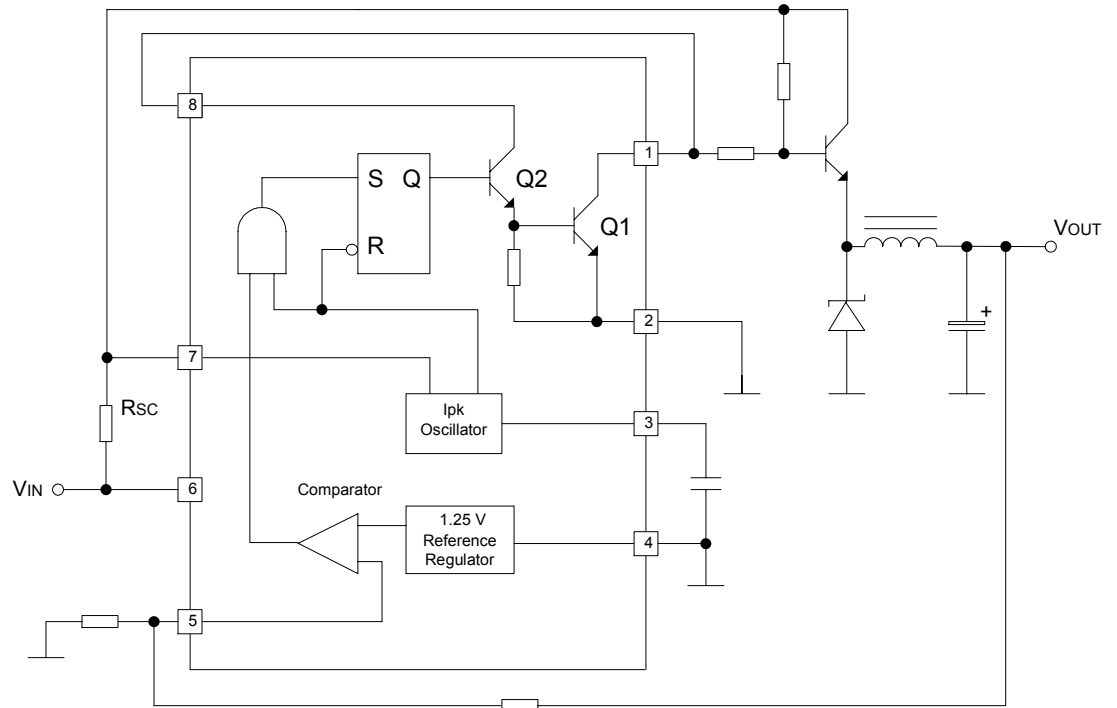
V_{ripple} = Desired peak to peak output ripple voltage. In practice, the calculated capacitor value will and to be increased due to its equivalent series resistance and board layout. The ripple voltage should be kept to a low value since it will directly affect the line and load regulation.

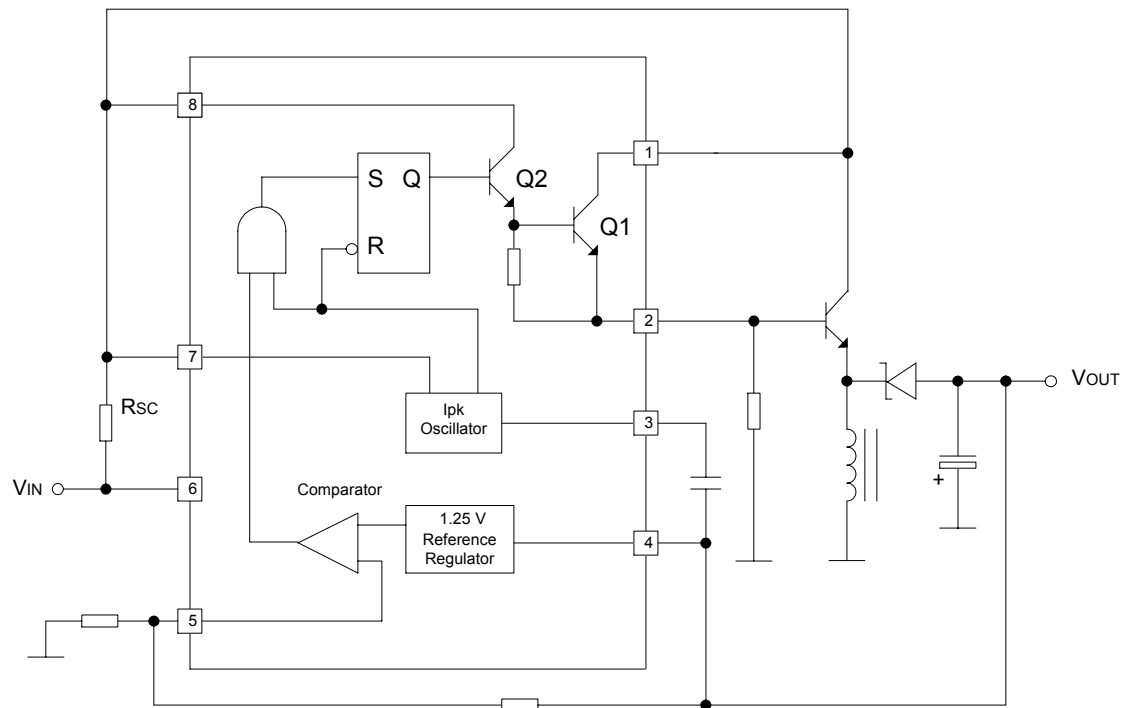
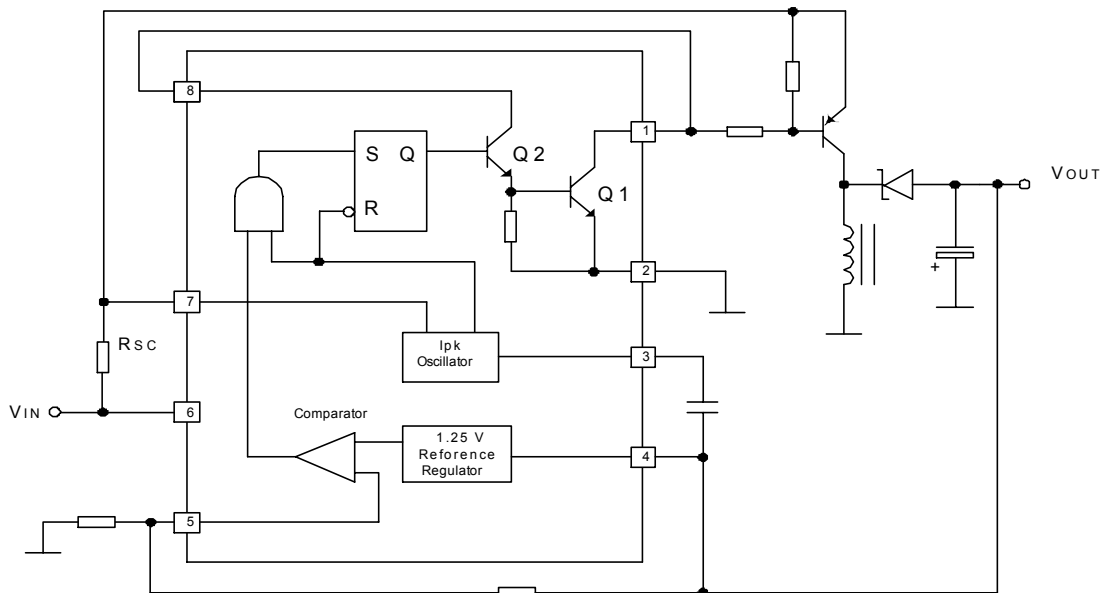
Step-up With External NPN Switch


Step-down With External NPN Switch

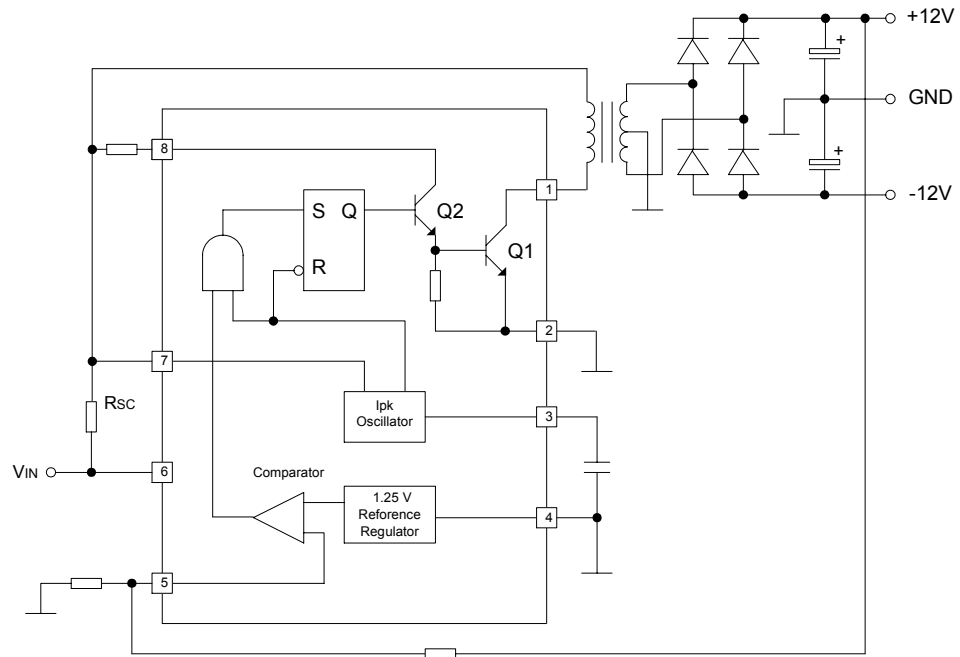


Step-down With External PNP Switch



Voltage Inverting With External NPN Switch

Voltage Inverting With External PNP Saturated Switch


Dual Output Voltage



Higher Output Power, Higher Input Voltage

