

**RICOH****2CH PWM DC/DC CONTROLLER****R1282D002A SERIES**

NO. EA-086-0502

**OUTLINE**

The R1282D002A is a CMOS-based 2-channel PWM Step-up (as Channel 1)/Step-down (as Channel 2) DC/DC converter controller.

The R1282D002A consists of an oscillator, a PWM control circuit, a reference voltage unit, an error amplifier, a reference current unit, a protection circuit, and an under voltage lockout (UVLO) circuit. A high efficiency Step-up/Step-down DC/DC converter can be composed of this IC with inductors, diodes, power MOSFETs, resistors, and capacitors. Each output voltage and maximum duty cycle can be adjustable with external resistors, while soft-start time can be adjustable with external capacitors and resistors.

As for a protection circuit, if Maximum duty cycle of either Step-up DC/DC converter side or Step-down DC/DC converter side is continued for a certain time, the R1282D002A latches both external drivers with their off state by its Latch-type protection circuit. Delay time for protection is internally fixed typically at 100ms. To release the protection circuit, restart with power-on (Voltage supplier is equal or less than UVLO detector threshold level).

**FEATURES**

- Input Voltage Range .....2.5V to 5.5V
- Built-in Latch-type Protection Function by monitoring duty cycle (Fixed Delay Time Typ. 100ms)
- Oscillator Frequency .....700kHz
- High Accuracy Voltage Reference ..... $\pm 1.5\%$
- U.V.L.O. Threshold.....Typ. 2.2V (Hysteresis: Typ. 0.2V)
- Small Package .....thin SON-10 (package thickness Max. 0.9mm)

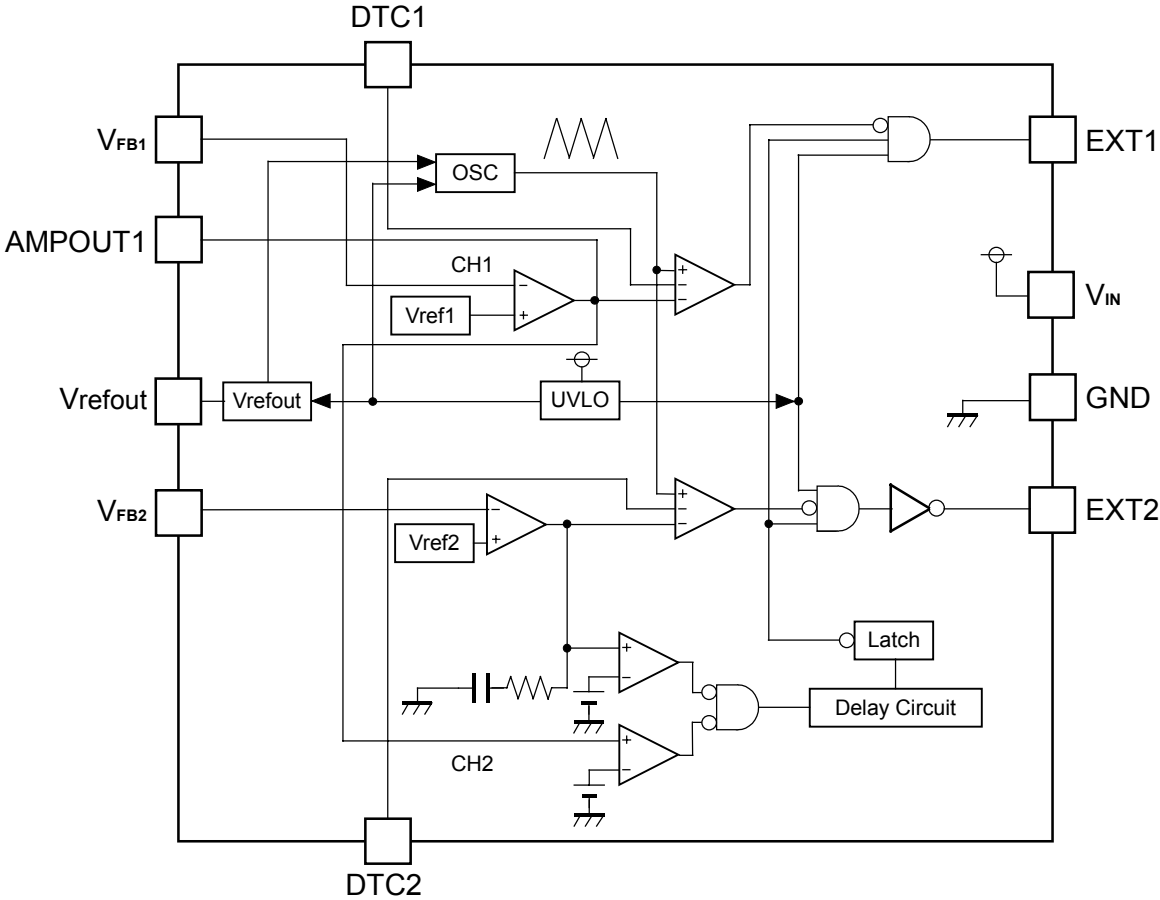
**APPLICATIONS**

- Constant Voltage Power Source for Portable Equipment.
- Constant Voltage Power Source for LCD and CCD.

**RICOH**

**R1282D002A**

**BLOCK DIAGRAM**



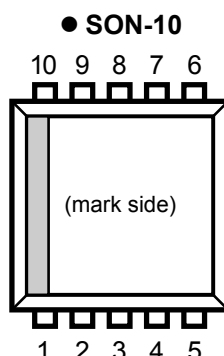
**SELECTION GUIDE**

The selection can be made with designating the part number as shown below;

R1282D002A-TR ←Part Number  
 ↑  
 a

Code	Contents
a	Designation of Taping Type : (Refer to Taping Specifications.)

## PIN CONFIGURATION



## PIN DESCRIPTION

Pin No	Symbol	Description
1	EXT1	External Transistor of Channel 1 Drive Pin (CMOS Output)
2	GND	Ground Pin
3	AMPOUT1	Amplifier Output Pin of Channel 1
4	DTC1	Maximum Duty Cycle of Channel 1 Setting Pin
5	V <sub>FB1</sub>	Feedback pin of Channel 1
6	V <sub>FB2</sub>	Feedback pin of Channel 2
7	DTC2	Maximum Duty Cycle of Channel 2 Setting Pin
8	V <sub>refout</sub>	Reference Output Pin
9	V <sub>IN</sub>	Voltage Supply Pin of the IC
10	EXT2	External Transistor of Channel 2 Drive Pin (CMOS Output)

## ABSOLUTE MAXIMUM RATINGS

Symbol	Item	Rating	Unit
V <sub>IN</sub>	V <sub>IN</sub> Pin Voltage	6.5	V
V <sub>EXT1,2</sub>	V <sub>EXT1,2</sub> Pin Output Voltage	-0.3~V <sub>IN</sub> +0.3	V
V <sub>AMPOUT1</sub>	AMPOUT1 Pin Voltage	-0.3~V <sub>IN</sub> +0.3	V
V <sub>DTC1,2</sub>	DTC1,2 Pin Voltage	-0.3~V <sub>IN</sub> +0.3	V
V <sub>refout</sub>	V <sub>REFOUT</sub> Pin Voltage	-0.3~V <sub>IN</sub> +0.3	V
V <sub>FB1,2</sub>	V <sub>FB1</sub> , V <sub>FB2</sub> Pin Voltage	-0.3~V <sub>IN</sub> +0.3	V
I <sub>EXT1,2</sub>	EXT1,2 Pin Output Current	±50	mA
P <sub>D</sub>	Power Dissipation	250	mW
T <sub>opt</sub>	Operating Temperature Range	-40 to +85	°C
T <sub>stg</sub>	Storage Temperature Range	-55 to +125	°C

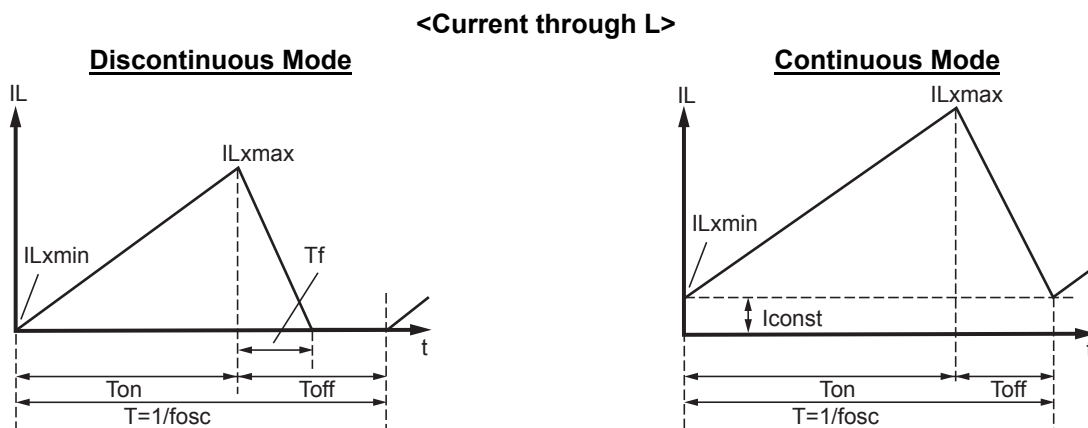
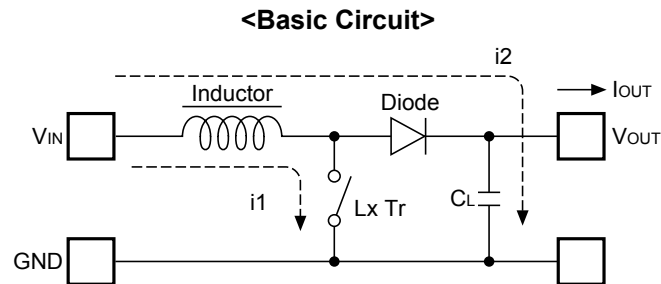
**R1282D002A****ELECTRICAL CHARACTERISTICS**

Topt=25°C

Symbol	Item	Conditions	Min.	Typ.	Max.	Unit
V <sub>IN</sub>	Operating Input Voltage		2.5		5.5	V
V <sub>REFOUT</sub>	V <sub>REFOUT</sub> Voltage Tolerance	V <sub>IN</sub> =3.3V, I <sub>OUT</sub> =1mA	1.478	1.500	1.522	V
I <sub>ROUT</sub>	V <sub>REFOUT</sub> Output Current	V <sub>IN</sub> =3.3V	20			mA
ΔV <sub>REFOUT</sub> /ΔV <sub>IN</sub>	V <sub>REFOUT</sub> Line Regulation	2.5V ≤ V <sub>IN</sub> ≤ 5.5V		2	6	mV
ΔV <sub>REFOUT</sub> /ΔI <sub>OUT</sub>	V <sub>REFOUT</sub> Load Regulation	1mA ≤ I <sub>ROUT</sub> ≤ 10mA V <sub>IN</sub> =3.3V		6	12	mV
I <sub>LIM</sub>	V <sub>REFOUT</sub> Short Current Limit	V <sub>IN</sub> =3.3V, V <sub>REFOUT</sub> =0V		25		mA
ΔV <sub>REFOUT</sub> /ΔT	V <sub>REFOUT</sub> Voltage Temperature Coefficient	-40°C ≤ Topt ≤ 85°C		±150		ppm/°C
V <sub>FB1</sub>	V <sub>FB1</sub> Voltage	V <sub>IN</sub> =3.3V	0.985	1.000	1.015	V
ΔV <sub>FB1</sub> /ΔT	V <sub>FB1</sub> Voltage Temperature Coefficient	-40°C ≤ Topt ≤ 85°C		±150		ppm/°C
ΔV <sub>FB2</sub> /ΔT	V <sub>FB2</sub> Voltage Temperature Coefficient	-40°C ≤ Topt ≤ 85°C		±150		ppm/°C
I <sub>VFB1,2</sub>	V <sub>FB1,2</sub> Input Current	V <sub>IN</sub> =5.5V, V <sub>FB1</sub> or V <sub>FB2</sub> =0V or 5.5V	-0.1		0.1	μA
f <sub>OSC</sub>	Oscillator Frequency	EXT1,2 Pins at no load, V <sub>IN</sub> =3.3V	595	700	805	kHz
I <sub>DD1</sub>	Supply Current	V <sub>IN</sub> =5.5V, EXT1,2 pins at no load		1.4	3.0	mA
R <sub>EXTH1</sub>	EXT1 "H" ON Resistance	V <sub>IN</sub> =3.3V, I <sub>EXT</sub> =-20mA		4.0	8.0	Ω
R <sub>EXTL1</sub>	EXT1 "L" ON Resistance	V <sub>IN</sub> =3.3V, I <sub>EXT</sub> =20mA		2.7	5.0	Ω
R <sub>EXTH2</sub>	EXT2 "H" ON Resistance	V <sub>IN</sub> =3.3V, I <sub>EXT</sub> =-20mA		4.0	8.0	Ω
R <sub>EXTL2</sub>	EXT2 "L" ON Resistance	V <sub>IN</sub> =3.3V, I <sub>EXT</sub> =20mA		3.7	8.0	Ω
T <sub>DLY</sub>	Delay Time for Protection	V <sub>IN</sub> =3.3V, V <sub>FB1</sub> =1.1V→0V	60	100	140	ms
V <sub>UVLOD</sub>	UVLO Detector Threshold		2.10	2.20	2.35	V
V <sub>UVLO</sub>	UVLO Released Voltage			V <sub>UVLOD</sub> +0.20	2.48	V
V <sub>DTC10</sub>	CH1 Duty=0%	V <sub>IN</sub> =3.3V	0.1	0.2	0.3	V
V <sub>DTC1100</sub>	CH1 Duty=100%	V <sub>IN</sub> =3.3V	1.1	1.2	1.3	V
V <sub>DTC20</sub>	CH2 Duty=0%	V <sub>IN</sub> =3.3V	0.1	0.2	0.3	V
V <sub>DTC2100</sub>	CH2 Duty=100%	V <sub>IN</sub> =3.3V	1.1	1.2	1.3	V
A <sub>V1</sub>	CH1 Open Loop Gain	V <sub>IN</sub> =3.3V		110		dB
F <sub>T1</sub>	CH1 Single Gain Frequency Band	V <sub>IN</sub> =3.3V, A <sub>V1</sub> =0dB		1.9		MHz
V <sub>ICR1</sub>	CH1 Input Voltage Range	V <sub>IN</sub> =3.3V		0.7 to V <sub>IN</sub>		V
I <sub>AMPL</sub>	CH1 Sink Current	V <sub>IN</sub> =3.3V, V <sub>AMPOUT1</sub> =1.0V, V <sub>FB1</sub> =V <sub>FB1</sub> + 0.1V	70	115		μA
I <sub>AMPH</sub>	CH1 Source Current	V <sub>IN</sub> =3.3V, V <sub>AMPOUT1</sub> =1.0V, V <sub>FB1</sub> =V <sub>FB1</sub> - 0.1V		-1.4	-0.7	mA
A <sub>V2</sub>	CH2 Open Loop Gain	V <sub>IN</sub> =3.3V		60		dB
F <sub>T2</sub>	CH2 Single Gain Frequency Band	V <sub>IN</sub> =3.3V, A <sub>V2</sub> =0dB		600		kHz
V <sub>ICR2</sub>	CH2 Input Voltage Range	V <sub>IN</sub> =3.3V		-0.2 to V <sub>IN</sub> -1.3		V
V <sub>FB2</sub>	CH2 Reference Voltage	V <sub>IN</sub> =3.3V	0.985	1.000	1.015	V

## Operation of Step-up DC/DC Converter and Output Current

Step-up DC/DC Converter makes higher output voltage than input voltage by releasing the energy accumulated during on time of  $L_x$  Transistor on input voltage.



Step 1.  $L_x$  Tr. is on, then the current  $I_L=i_1$  flows, and the energy is charged in L. In proportion to the on time of  $L_x$  Tr. ( $T_{on}$ ),  $I_L=i_1$  increases from  $I_L=I_{Lxmin}=0$  and reaches  $I_{Lxmax}$ .

Step 2. When the  $L_x$  Tr. is off, L turns on Schottky Diode (SD), and  $I_L=i_2$  flows to maintain  $I_L=I_{Lxmax}$ .

Step 3.  $I_L=i_2$  gradually decreases, and after  $T_f$  passes,  $I_L=I_{Lxmin}=0$  is true, then SD turns off. Note that in the case of the continuous mode, before  $I_L=I_{Lxmin}=0$  is true,  $T_{off}$  passes, and the next cycle starts, then  $L_x$  Tr. turns on again.

In this case,  $I_{Lxmin}>0$ , therefore  $I_L=I_{Lxmin}>0$  is another starting point and  $I_{Lx max}$  increases.

With the PWM controller, switching times during the time unit are fixed. By controlling  $T_{on}$ , output voltage is maintained.

**R1282D002A****Output Current and Selection of External Components**

## Output Current of Step-up Circuit and External Components

There are two modes, or discontinuous mode and continuous mode for the PWM step-up switching regulator depending on the continuous characteristic of inductor current.

During on time of the transistor, when the voltage added on to the inductor is described as  $V_{IN}$ , the current is  $V_{IN} \times t/L$ .

Therefore, the electric power,  $P_{ON}$ , which is supplied with input side, can be described as in next formula.

$$P_{ON} = \int_0^{T_{on}} V_{IN}^2 \times t/L dt \dots\dots\dots \text{Formula 1}$$

With the step-up circuit, electric power is supplied from power source also during off time. In this case, input current is described as  $(V_{OUT}-V_{IN}) \times t/L$ , therefore electric power,  $P_{OFF}$  is described as in next formula.

$$P_{OFF} = \int_0^{T_f} V_{IN} \times (V_{OUT} - V_{IN})t/L dt \dots\dots\dots \text{Formula 2}$$

In this formula,  $T_f$  means the time of which the energy saved in the inductance is being emitted. Thus average electric power,  $P_{AV}$  is described as in the next formula.

$$P_{AV} = 1/(T_{on} + T_{off}) \times \left\{ \int_0^{T_{on}} V_{IN}^2 \times t/L dt + \int_0^{T_f} V_{IN} \times (V_{OUT} - V_{IN})t/L dt \right\} \dots\dots\dots \text{Formula 3}$$

In PWM control, when  $T_f = T_{off}$  is true, the inductor current becomes continuous, then the operation of switching regulator becomes continuous mode.

In the continuous mode, the deviation of the current is equal between on time and off time.

$$V_{IN} \times T_{on}/L = (V_{OUT} - V_{IN}) \times T_{off}/L \dots\dots\dots \text{Formula 4}$$

Further, the electric power,  $P_{AV}$  is equal to output electric power,  $V_{OUT} \times I_{OUT}$ , thus,

$$I_{OUT} = f_{OSC} \times V_{IN}^2 \times T_{on}^2 / \{2 \times L \times (V_{OUT} - V_{IN})\} = V_{IN}^2 \times T_{on} / (2 \times L \times V_{OUT}) \dots\dots\dots \text{Formula 5}$$

When  $I_{OUT}$  becomes more than  $V_{IN} \times T_{on} \times T_{off} / (2 \times L \times (T_{on} + T_{off}))$ , the current flows through the inductor, then the mode becomes continuous. The continuous current through the inductor is described as

$I_{const}$ , then,

$$I_{OUT} = f_{OSC} \times V_{IN}^2 \times T_{on}^2 / (2 \times L \times (V_{OUT} - V_{IN})) + V_{IN} \times I_{const} / V_{OUT} \dots\dots\dots \text{Formula 6}$$

In this moment, the peak current,  $I_{Lxmax}$  flowing through the inductor and the driver  $T_r$  is described as follows:

$$I_{Lxmax} = I_{const} + V_{IN} \times T_{on} / L \dots \dots \dots \text{Formula 7}$$

With the formula 4,6, and  $I_{Lxmax}$  is,

$$I_{Lxmax} = V_{OUT} / V_{IN} \times I_{OUT} + V_{IN} \times T_{on} / (2 \times L) \dots \dots \dots \text{Formula 8}$$

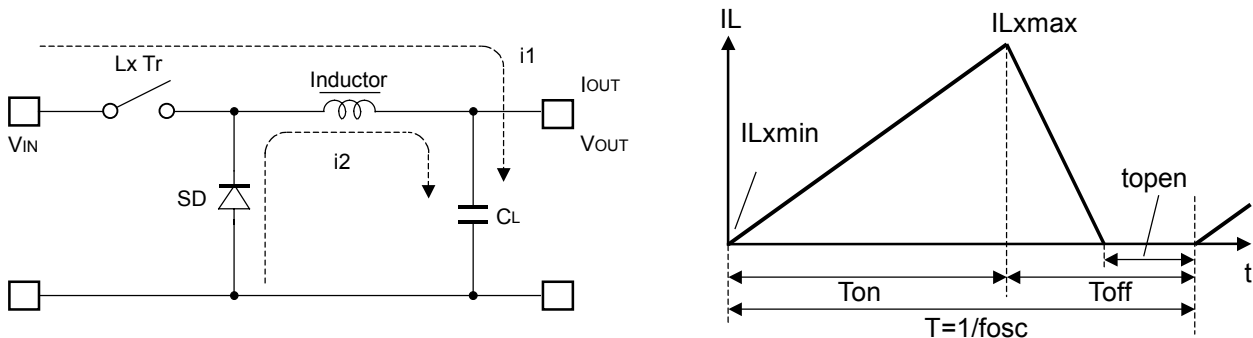
Therefore, peak current is more than  $I_{OUT}$ . Considering the value of  $I_{Lxmax}$ , the condition of input and output, and external components should be selected.

In the formula 7, peak current  $I_{Lxmax}$  at discontinuous mode can be calculated. Put  $I_{const}=0$  in the formula.

The explanation above is based on the ideal calculation, and the loss caused by  $L_x$  switch and external components is not included. The actual maximum output current is between 50% and 80% of the calculation. Especially, when the  $I_{Lx}$  is large, or  $V_{IN}$  is low, the loss of  $V_{IN}$  is generated with the on resistance of the switch. As for  $V_{OUT}$ ,  $V_f$  (as much as 0.3V) of the diode should be considered.

**R1282D002A****Operation of Inverting DC/DC converter and Output Current**

The step-down DC/DC converter charges energy in the inductor when Lx transistor is ON, and discharges the energy from the inductor when Lx transistor is OFF and controls with less energy loss, so that a lower output voltage than the input voltage is obtained. The operation will be explained with reference to the following diagrams:

**<Basic Circuits>**

Step 1. Lx Tr. turns on and current  $I_L (=i_1)$  flows, and energy is charged into CL. At this moment,  $I_L$  increases from  $I_{Lmin}$ . ( $=0$ ) to reach  $I_{Lmax}$ . in proportion to the on-time period( $ton$ ) of LX Tr.

Step 2. When Lx Tr. turns off, Schottky diode (SD) turns on in order that L maintains  $I_L$  at  $I_{Lmax}$ , and current  $I_L (=i_2)$  flows.

Step 3.  $I_L$  decreases gradually and reaches  $I_{Lmin}$ . after a time period of  $topen$ , and SD turns off, provided that in the continuous mode, next cycle starts before  $I_L$  becomes to 0 because  $toff$  time is not enough. In this case,  $I_L$  value is from this  $I_{Lmin}$  ( $>0$ ).

In the case of PWM control system, the output voltage is maintained by controlling the on-time period ( $ton$ ), with the oscillator frequency ( $fosc$ ) being maintained constant.

**Discontinuous Conduction Mode and Continuous Conduction Mode**

The maximum value ( $I_{Lmax}$ ) and the minimum value ( $I_{Lmin}$ ) current which flow through the inductor is the same as those when Lx Tr. is ON and when it is OFF.

The difference between  $I_{Lmax}$  and  $I_{Lmin}$ , which is represented by  $\Delta I$ ;

$$\Delta I = I_{Lmax} - I_{Lmin} = V_{OUT} \times topen / L = (V_{IN} - V_{OUT}) \times ton / L \dots \text{Equation A}$$

wherein,  $T = 1/fosc = ton + toff$

$$\text{duty (\%)} = ton / T \times 100 = ton \times fosc \times 100$$

$$topen \leq toff$$

In Equation A,  $V_{OUT} \times topen / L$  and  $(V_{IN} - V_{OUT}) \times ton / L$  are respectively shown the change of the current at ON, and the change of the current at OFF.

When the output current ( $I_{OUT}$ ) is relatively small,  $topen < toff$  as illustrated in the above diagram. In this case, the energy is charged in the inductor during the time period of  $ton$  and is discharged in its entirely during the time period of  $toff$ , therefore  $I_{Lmin}$  becomes to zero ( $I_{Lmin} = 0$ ). When  $I_{OUT}$  is gradually increased, eventually,  $topen$  becomes to  $toff$  ( $topen = toff$ ), and when  $I_{OUT}$  is further increased,  $I_{Lmin}$  becomes larger than zero ( $I_{Lmin} > 0$ ). The former mode is referred to as the discontinuous mode and the latter mode is referred to as continuous mode.

In the continuous mode, when Equation A is solved for  $ton$  and assumed that the solution is  $tonc$ ,

$$tonc = T \times V_{OUT} / V_{IN} \dots \text{Equation B}$$

When  $ton < tonc$ , the mode is the discontinuous mode, and when  $ton = tonc$ , the mode is the continuous mode.



## Output Current and Selection of External Components

There are also two modes, or discontinuous mode and continuous mode for the PWM step-down switching regulator depending on the continuous characteristic of inductor current.

During on time of the transistor, when the voltage added on to the inductor is described as  $V_{IN} - V_{OUT}$  the current is  $(V_{IN} - V_{OUT}) \times t/L$ .

Therefore, the electric power, P, which is supplied from the input side, can be described as in next formula.

$$P = \int_0^{T_{on}} V_{IN} \cdot (V_{IN} - V_{OUT}) \cdot t/L dt \dots\dots\dots \text{Formula 9}$$

Thus average electric power in one cycle,  $P_{AV}$  is described as in the next formula.

$$P_{AV} = 1/(T_{on} + T_{off}) \int_0^{T_{on}} V_{IN} \cdot (V_{IN} - V_{OUT}) \cdot t/L dt = V_{IN} \cdot (V_{IN} - V_{OUT}) \cdot T_{on}^2 / (2 \cdot L (T_{on} + T_{off})) \dots\dots \text{Formula 10}$$

This electric power  $P_{AV}$  equals to output electric power  $V_{OUT} \times I_{OUT}$ , thus,

$$I_{OUT} = V_{IN} / V_{OUT} \times (V_{IN} - V_{OUT}) \cdot T_{on}^2 / (2 \times L \times (T_{on} + T_{off})) \dots\dots\dots \text{Formula 11}$$

When  $I_{OUT}$  increases and the current flows through the inductor continuously, then the mode becomes continuous. In the continuous mode, the deviation of the current equals between  $T_{on}$  and  $T_{off}$ , therefore,

$$(V_{IN} - V_{OUT}) \times T_{on}/L = V_{OUT} \times T_{off}/L \dots\dots\dots \text{Formula 12}$$

In this moment, the current flowing continuously through L, is assumed as  $I_{const}$ ,  $I_{OUT}$  is described as in the next formula:

$$I_{OUT} = I_{CONST} + V_{OUT} \times T_{off} / (2 \times L) \dots\dots\dots \text{Formula 13}$$

In this moment, the peak current,  $I_{Lxmax}$  flowing through the inductor and the driver  $T_r$  is described as follows:

$$I_{Lxmax} = I_{OUT} + V_{OUT} \times T_{off} / (2 \times L) \dots\dots\dots \text{Formula 14}$$

With the formula 12,13,  $I_{Lxmax}$  is,

$$T_{off} = (1 - V_{OUT}/V_{IN}) / f_{osc} \dots\dots\dots \text{Formula 15}$$

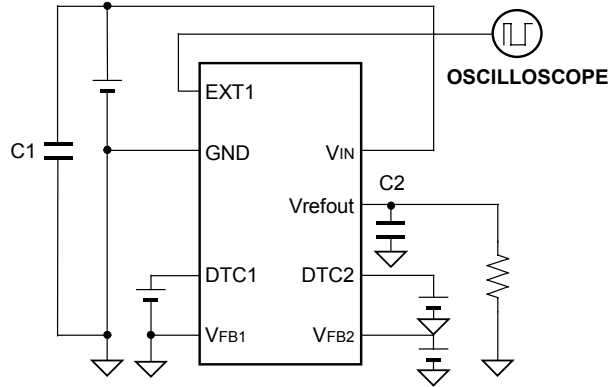
Therefore, peak current is more than  $I_{OUT}$ . Considering the value of  $I_{Lxmax}$ , the condition of input and output, and external components should be selected.

In the formula 14, peak current  $I_{Lxmax}$  at discontinuous mode can be calculated. Put  $I_{const}=0$  in the formula.

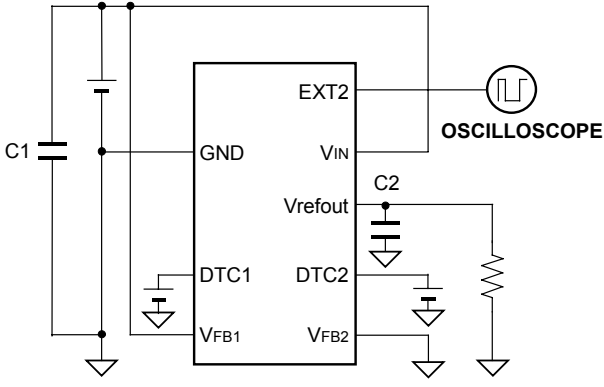
The explanation above is based on the ideal calculation, and the loss caused by  $L_x$  switch and external components is not included.

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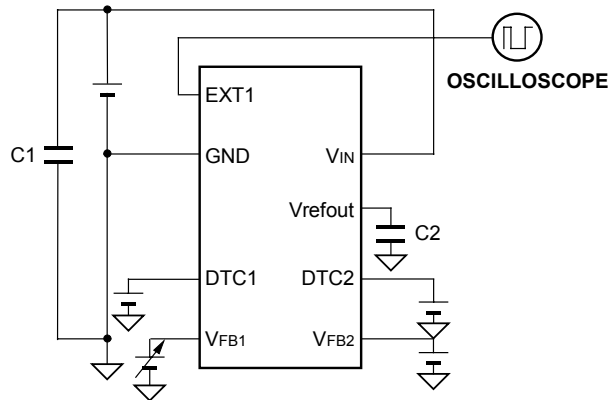
TEST CIRCUITS



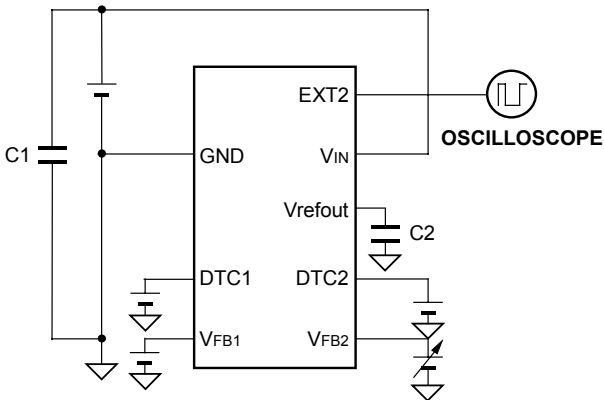
Test Circuit 1



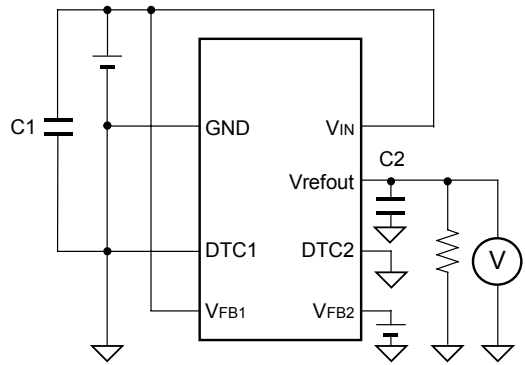
Test Circuit 2



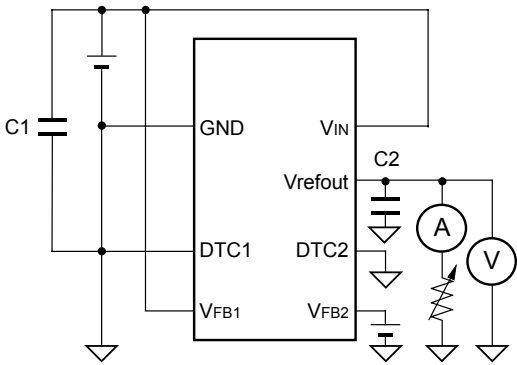
Test Circuit 3



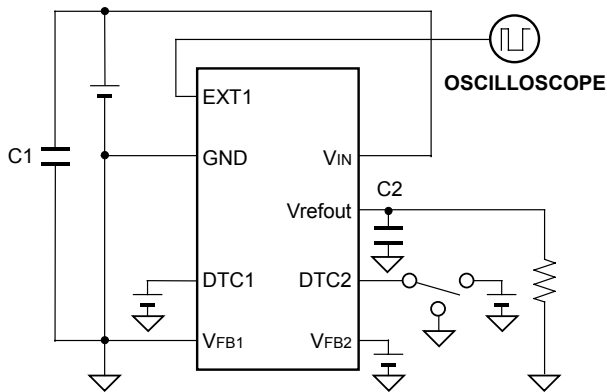
Test Circuit 4



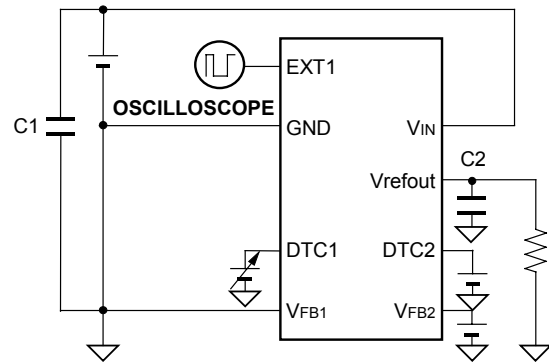
Test Circuit 5



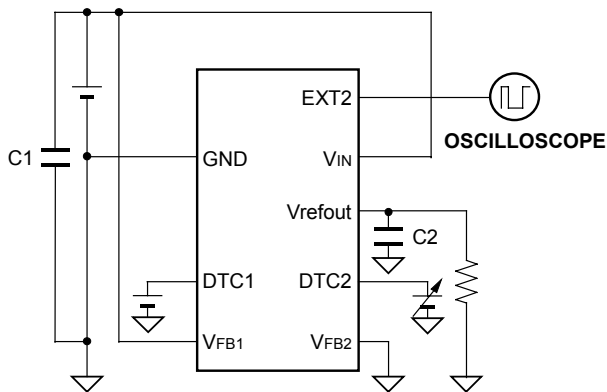
Test Circuit 6



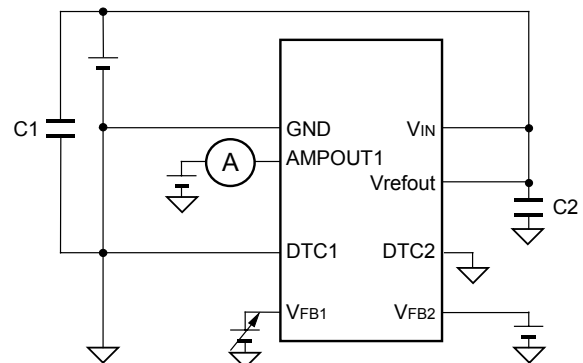
Test Circuit 7



Test Circuit 8



Test Circuit 9



Test Circuit 10

Typical Characteristics shown in the following pages are obtained with test circuits shown above.

- Test Circuit 1,2 : Typical Characteristic 4)
- Test Circuit 3 : Typical Characteristic 5)
- Test Circuit 4 : Typical Characteristic 5)
- Test Circuit 5 : Typical Characteristic 6)
- Test Circuit 6 : Typical Characteristics 7) 8)
- Test Circuit 7 : Typical Characteristic 9)
- Test Circuit 8 : Typical Characteristic 10)
- Test Circuit 9 : Typical Characteristics 10)
- Test Circuit 10 : Typical Characteristics 11) 12)

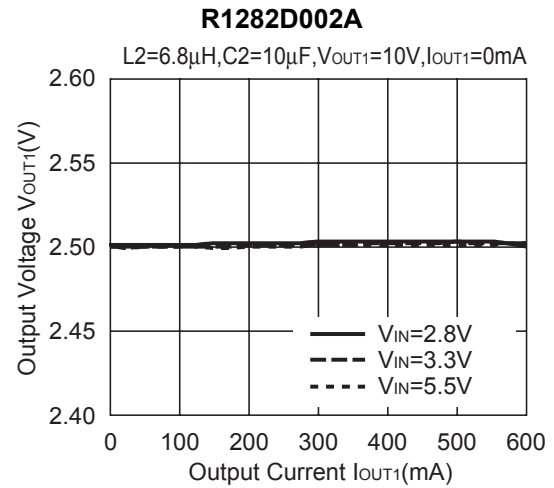
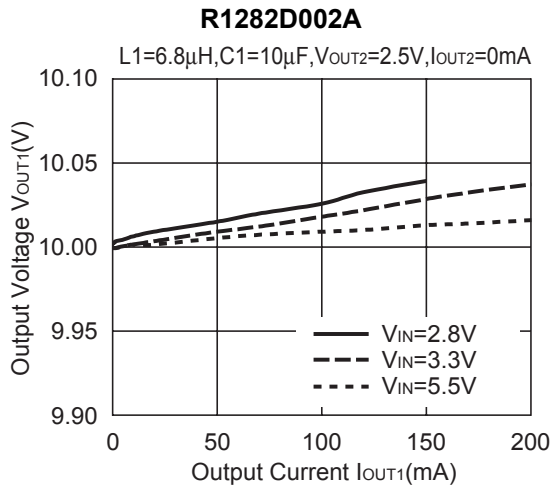
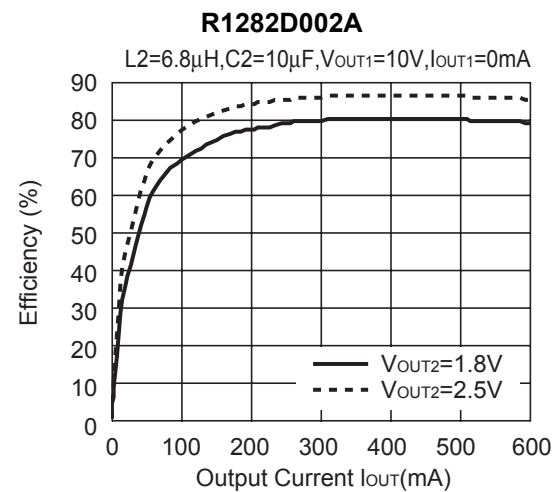
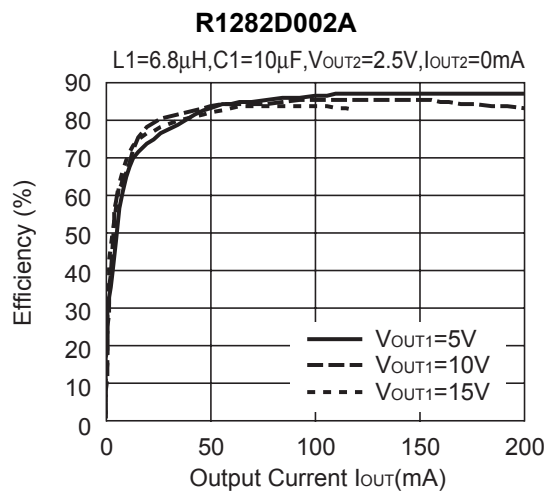
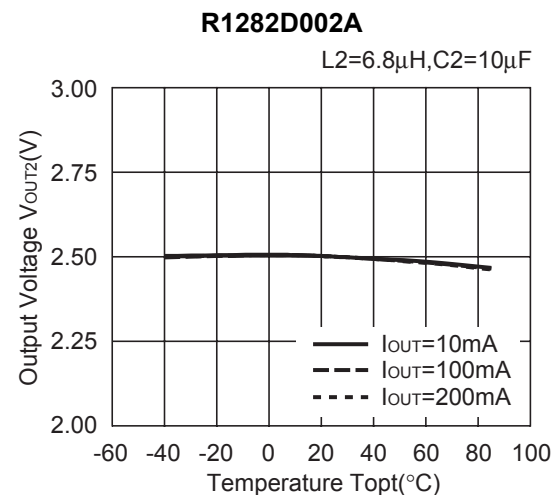
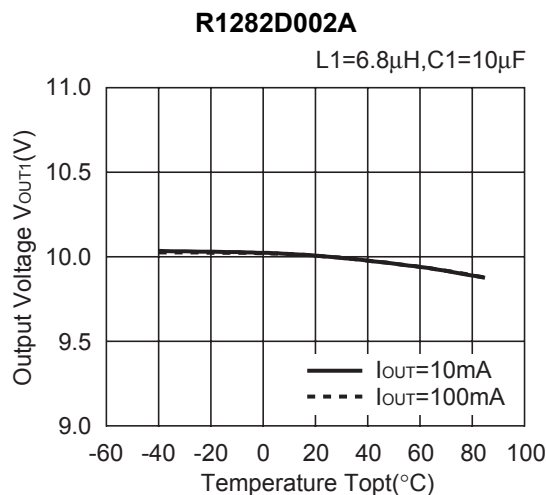
Note) Capacitors' values of test circuits

Capacitors: Ceramic Type:

C1=4.7 $\mu$ F, C2=1.0 $\mu$ F

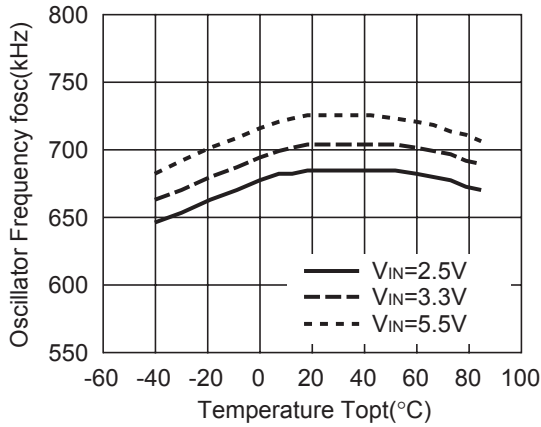
Efficiency  $\eta$ (%) can be calculated with the next formula:

$$\eta = (V_{OUT1} \times I_{OUT1} + V_{OUT2} \times I_{OUT2}) / (V_{IN} \times I_{IN}) \times 100$$

**R1282D002A****TYPICAL CHARACTERISTICS****1) Output Voltage vs. Output Current (Topt=25°C)****2) Efficiency vs. Output Current (VIN=3.3V, Topt=25°C)****3) Output Voltage vs. Temperature (VIN=3.3V)**

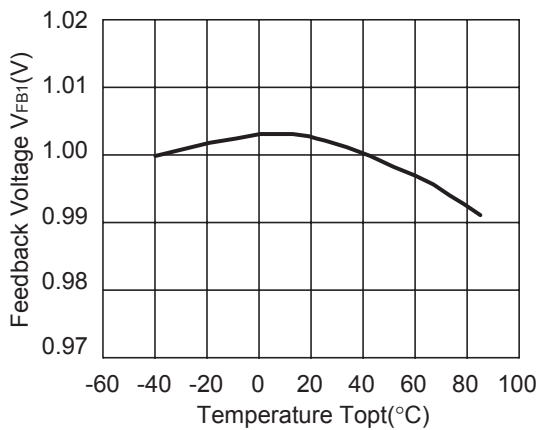
**4) Frequency vs. Temperature**

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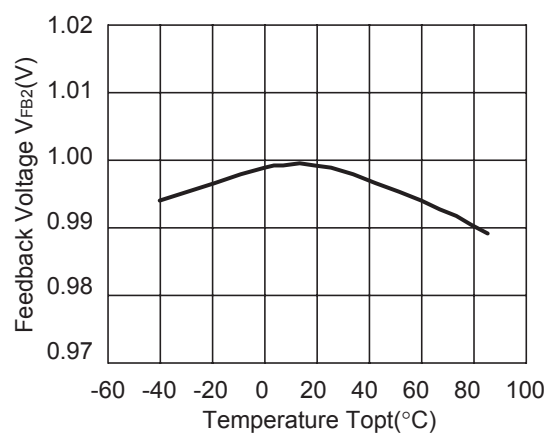


**5) Feedback Voltage vs. Temperature (V<sub>IN</sub>=3.3V)**

**R1282D002A**

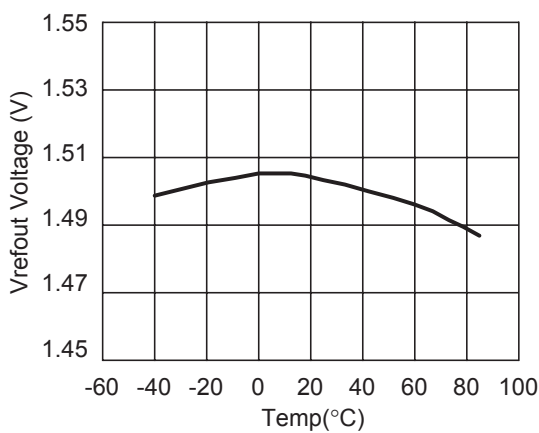


**R1282D002A**



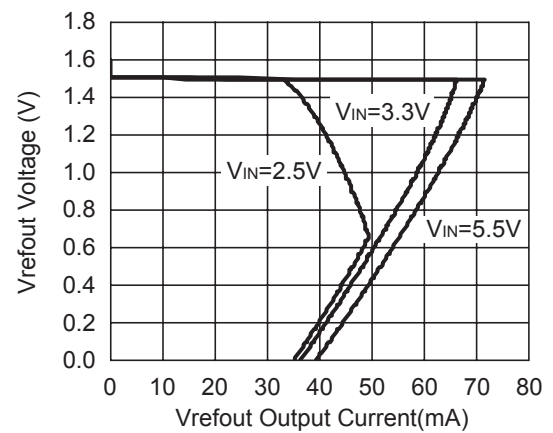
**6) V<sub>refout</sub> Voltage vs. Temperature (V<sub>IN</sub>=3.3V)**

**R1282D002A**



**7) V<sub>refout</sub> Output Voltage vs. Output Current**

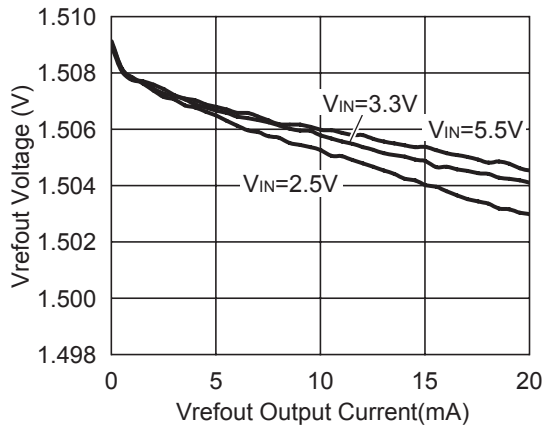
**R1282D002A**



**R1282D002A**

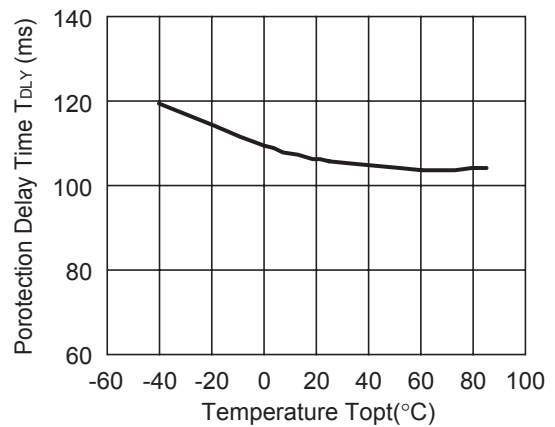
**8) Vrefout Output Voltage vs. Output Current**

**R1282D002A**



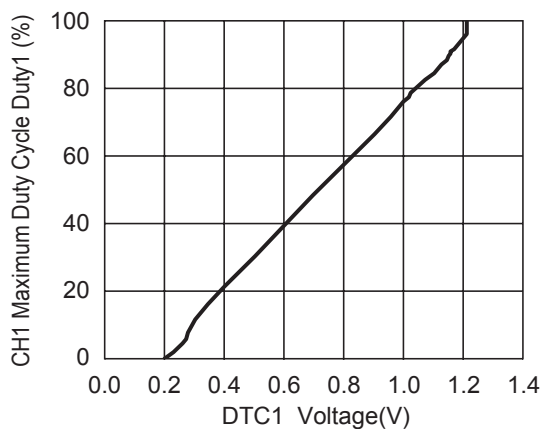
**9) Protection Delay Time vs. Temperature (V<sub>IN</sub>=3.3V)**

**R1282D002A**

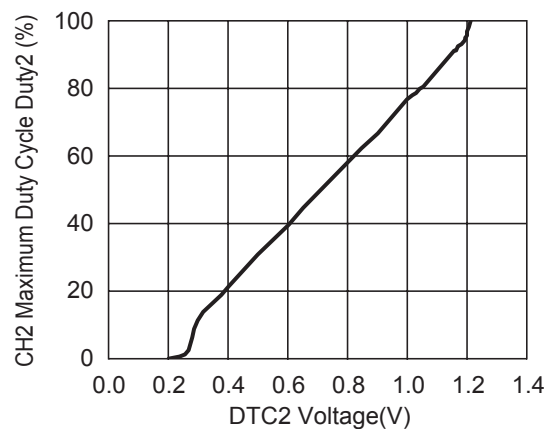


**10) Maximum Duty Cycle vs. DTC Voltage (V<sub>IN</sub>=3.3V)**

**R1282D002A**

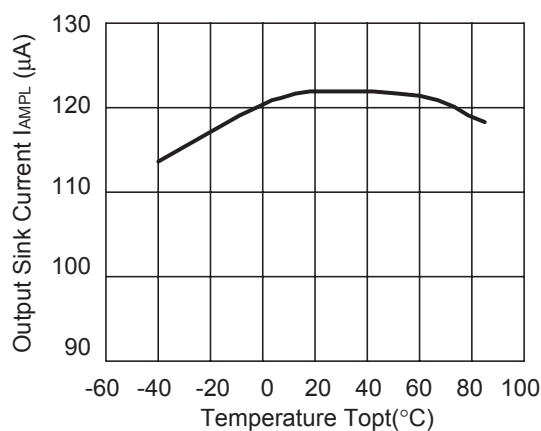


**R1282D002A**



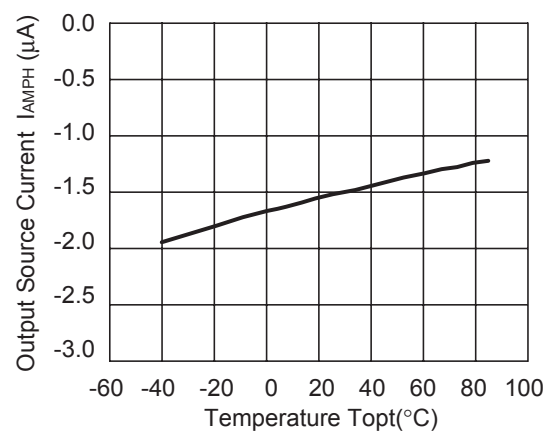
**11) Output Sink Current vs. Temperature (V<sub>IN</sub>=3.3V)**

**R1282D002A**

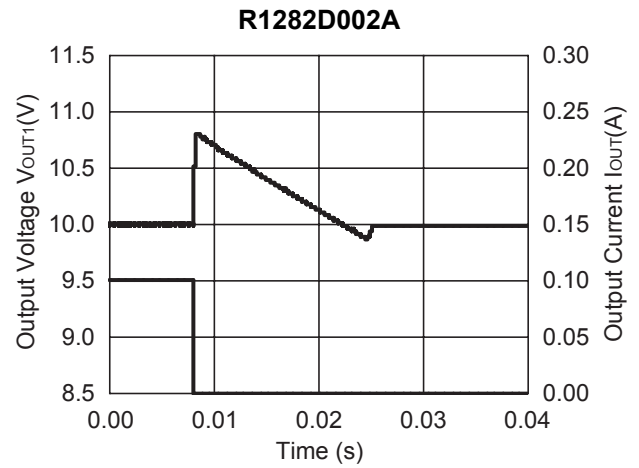
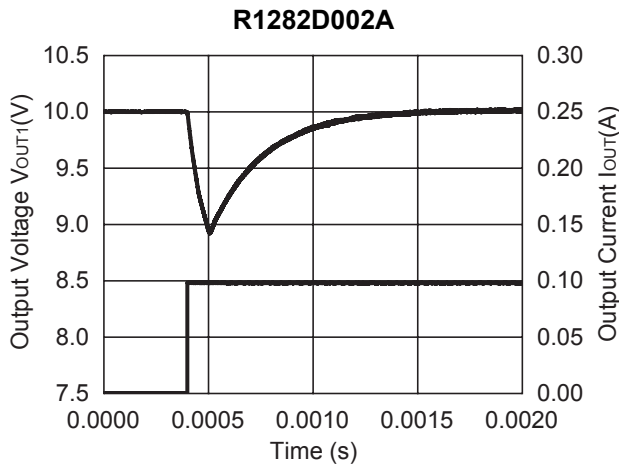


**12) Output Source Current vs. Temperature**

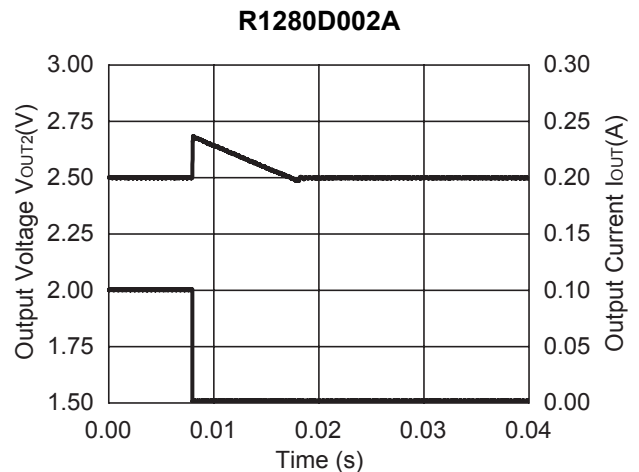
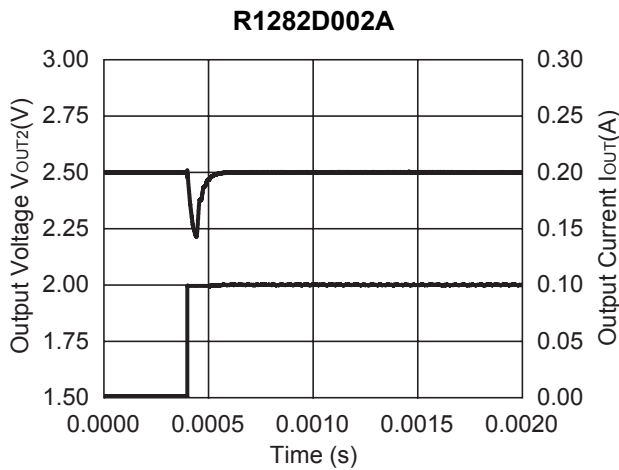
**R1282D002A**

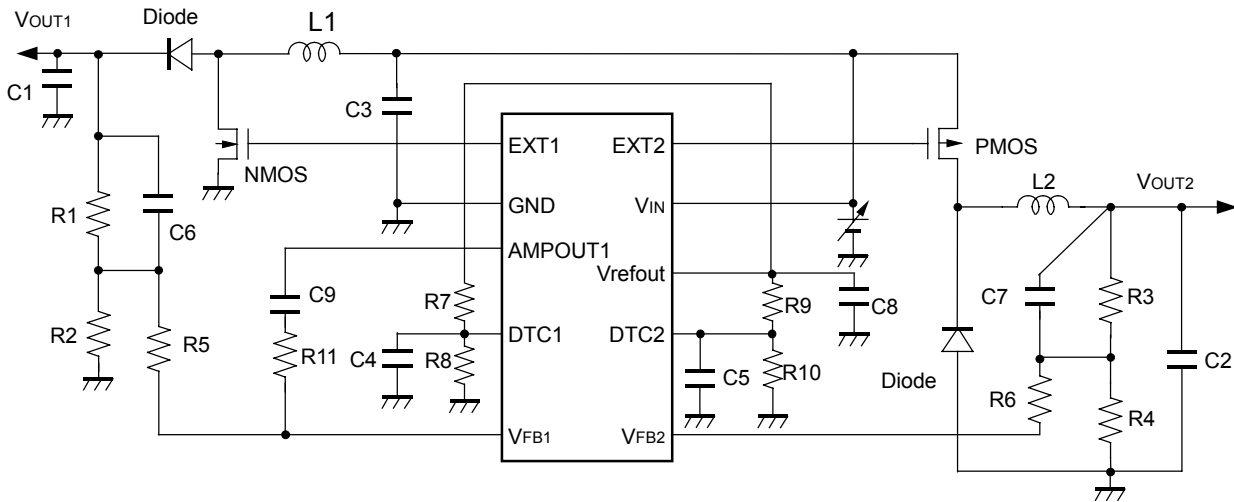


**13) Load Transient Response (Step-up Side)  $V_{IN}=3.3V$ ,  $L1=6.8\mu H$**



**14) Load Transient Response (Step-down Side)  $V_{IN}=3.3V$ ,  $L2=6.8\mu H$**



**R1282D002A****TYPICAL APPLICATION AND TECHNICAL NOTES****Components examples**

Inductor L1,2	6.8 $\mu$ H LDR655312T (TDK)
Diode	FS1J3 (Origin Electronics)
PMOS	Si3443DV (Siliconix)
NMOS	IRF7601 (International Rectifier)

Resistance As setting resistors total value for the output voltage, R1+R2, R3+R4 recommendation value is 100k $\Omega$  or less.

R1=47k $\Omega$	R2=5.1k $\Omega$	R3=30k $\Omega$	R4=20k $\Omega$
R5=43k $\Omega$	R6=10k $\Omega$		
R7=R9=22k $\Omega$	R8=R10=43k $\Omega$	R11=220k $\Omega$	

**Capacitors Ceramic Type**

C1=C2=10 $\mu$ F	C3=4.7 $\mu$ F	C4=0.22 $\mu$ F	C5=0.47 $\mu$ F	C6=120pF
C7=50pF	C8=1 $\mu$ F	C9=1000pF		

Note) Consider the ratings of external components including voltage tolerance. With the transistor in the circuit above, V<sub>OUT</sub>=15V is the voltage setting limit.



## EXTERNAL COMPONENTS

### 1. How to set the output voltages

As for step-up side, feedback ( $V_{FB1}$ ) pin voltage is controlled to maintain 1V, therefore,

$$V_{OUT1}: R1+R2=V_{FB1}: R2$$

Thus,  $V_{OUT1}=V_{FB1}\times(R1+R2)/R2$

Output Voltage is adjustable with R1 and R2.

As for Step-down side, Feedback ( $V_{FB2}$ ) pin voltage follows the next formula,

$$V_{OUT2}: R3+R4=V_{FB2} : R4$$

Thus,  $V_{OUT2}=V_{FB2}\times(R3+R4)/R4$

Output Voltage is adjustable with R3 and R4.

### 2. How to set Soft-Start Time and Maximum Duty Cycle

Soft-start time is adjustable with connecting resistors and a capacitor to DTC pin.

Soft starting time,  $T_{SS1}$  and  $T_{SS2}$  are adjustable. Soft-start time can be set with the time constant of RC.

Soft-start time can be described as in next formula.

$$T_{SS1}\cong R01\times C4$$

If  $R10=0\Omega$ , then,

$$T_{SS2}\cong R9\times C5\times\ln((V_{refout}-V_{DTC2})/V_{refout})$$

Maximum Duty Cycle is set with the voltage to DTC1 and DTC2.

Maximum duty cycle is described as follows;

CH1 (Step-up side)

$$\text{Maxduty1}\cong (R8/(R7+R8) \times V_{refout}-0.2)/(1.2-0.2) \times 100 (\%)$$

Step-up side maximum duty cycle should be set equal or less than 90%. If the maximum duty cycle is set at high percentage, operation will be unstable.

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**R1282D002A**

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**TECHNICAL NOTES on EXTERNAL COMPONENTS**

- External components should be set as close to this IC as possible. Especially, wiring of the capacitor connected to  $V_{IN}$  pin should be as short as possible.
- Enforce the ground wire. Large current caused by switching operation flows through GND pin. If the impedance of ground wire is high, internal voltage level of this IC might fluctuate and operation could be unstable.
- Recommended capacitance value of C3 is equal or more than  $4.7\mu\text{F}$ .
- If the spike noise of  $V_{OUT1}$  is too large, the noise is feedback from  $V_{FB1}$  pin and operation might be unstable. In that case, use the resistor ranging from  $10\text{k}\Omega$  to  $50\text{k}\Omega$  as R5 and try to reduce the noise level. In the case of  $V_{OUT2}$ , use the resistor as much as  $10\text{k}\Omega$  as R6.
- Select an inductor with low D.C. current, large permissible current, and uneasy to cause magnetic saturation. If the inductance value is too small,  $I_{Lx}$  might be beyond the absolute maximum rating at the maximum load.
- Select a Schottky diode with fast switching speed and large enough permissible current.
- Recommended capacitance value of C1 and C2 is as much as Ceramic  $10\mu\text{F}$ . In case that the operation with the system of DC/DC converter would be unstable, add a series resistor less than  $0.5\Omega$  to each output capacitor or use tantalum capacitors with appropriate ESR. If you choose too large ESR, ripple noise may be forced to  $V_{FB1}$  and  $V_{FB2}$ , and unstable operation may result. Use a capacitor with fully large voltage tolerance of the capacitor.
- this IC, for the test efficiency, latch release function is included. By forcing  $(V_{IN}-0.3)\text{V}$  or more voltage to DTC1 pin or DTC2 pin, Latch release function works.
- Performance of the power controller with using this IC depends on external components. Each component, layout should not be beyond each absolute maximum rating such as voltage, current, and power dissipation.