

# SA58671

## 1.2 W/channel stereo class-D audio amplifier

Rev. 01 — 21 December 2007

Product data sheet

## 1. General description

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The SA58671 is a stereo, filter-free class-D audio amplifier which is available in a 16 bump WLCSP (Wafer Level Chip-Size Package).

The SA58671 features independent shutdown controls for each channel. The gain can be set at 6 dB, 12 dB, 18 dB or 24 dB using G0 and G1 gain select pins. Improved immunity to noise and RF rectification is increased by high PSRR and differential circuit topology. Fast start-up time and very small WLCSP package makes it an ideal choice for both cellular handsets and PDAs.

The SA58671 delivers 1.3 W/channel at 5 V and 720 mW/channel at 3.6 V into 8  $\Omega$ . It delivers 1.2 W/channel at 5 V into 4  $\Omega$ . The maximum power efficiency is excellent at 70 % to 74 % into 4  $\Omega$  and 84 % to 88 % into 8  $\Omega$ . The SA58671 provides thermal and short-circuit shutdown protection.

## 2. Features

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- Output power:
  - ◆ 1.2 W/channel into 4  $\Omega$  at 5 V
  - ◆ 1.3 W/channel into 8  $\Omega$  at 5 V
  - ◆ 720 mW/channel into 8  $\Omega$  at 3.6 V
- Supply voltage: 2.5 V to 5.5 V
- Independent shutdown control for each channel
- Selectable gain: 6 dB, 12 dB, 18 dB and 24 dB
- High SVRR: -77 dB at 217 Hz
- Fast start-up time: 3.5 ms
- Low supply current
- Low shutdown current
- Short-circuit and thermal protection
- Space savings with 2.06 mm  $\times$  2.11 mm 16 bump WLCSP package
- Low junction to ambient thermal resistance of 110 K/W with adequate heat sinking of WLCSP

## 3. Applications

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- Wireless and cellular handsets and PDA
- Portable DVD player
- USB speaker
- Notebook PC

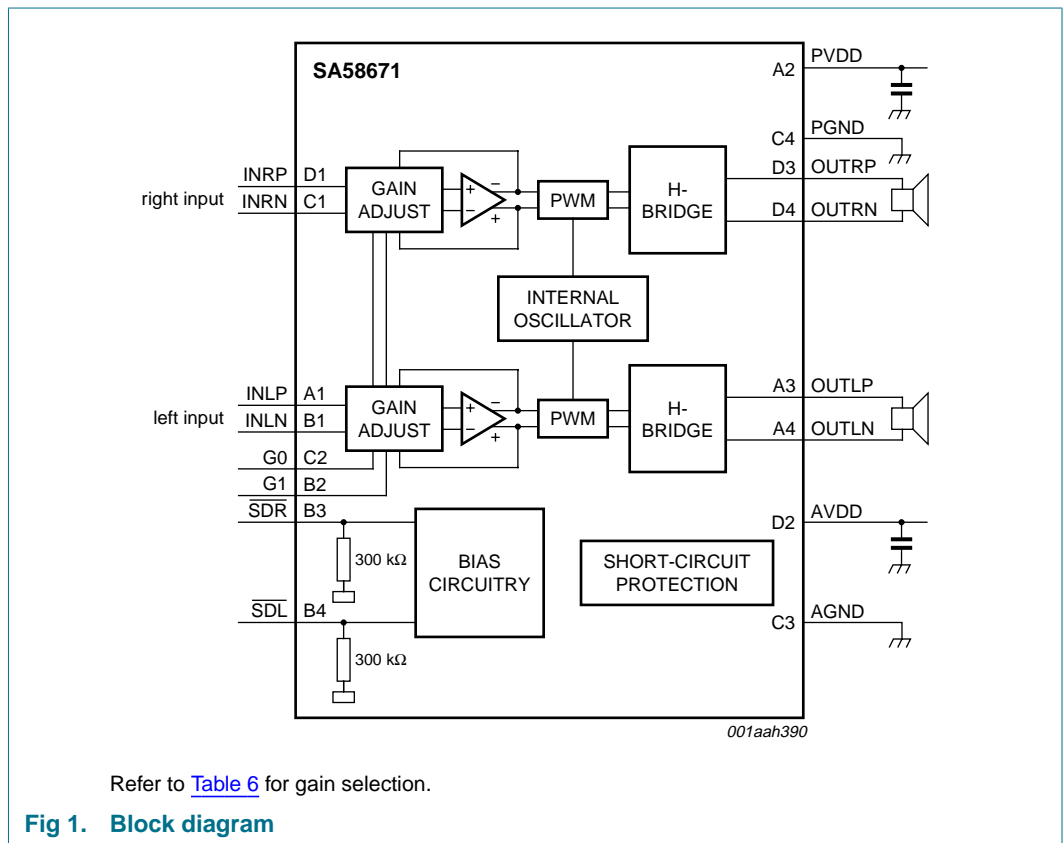
- Portable radio and gaming
- Educational toy

### 4. Ordering information

Table 1. Ordering information

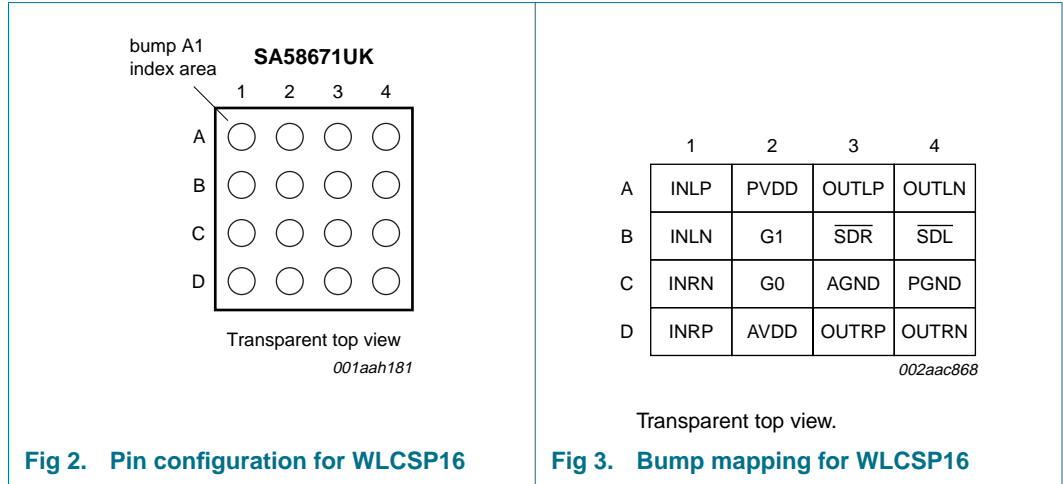
Type number	Package		Version
	Name	Description	
SA58671UK	WLCSP16	wafer level chip-size package; 16 bumps; 2.06 × 2.11 × 0.6 mm	SA58671UK

### 5. Block diagram



## 6. Pinning information

### 6.1 Pinning



### 6.2 Pin description

Table 2. Pin description

Symbol	Pin	Description
INLP	A1	left channel positive input
INLN	B1	left channel negative input
INRN	C1	right channel negative input
INRP	D1	right channel positive input
PVDD	A2	power supply voltage (level same as AVDD)
G1	B2	gain select input 1
G0	C2	gain select input 0
AVDD	D2	analog supply voltage (level same as PVDD)
OUTLP	A3	left channel positive output
SDR	B3	right channel shutdown input (active LOW)
AGND	C3	analog ground
OUTRP	D3	right channel positive output
OUTLN	A4	left channel negative output
SDL	B4	left channel shutdown input (active LOW)
PGND	C4	power ground
OUTRN	D4	right channel negative output

## 7. Limiting values

**Table 3. Limiting values**

*In accordance with the Absolute Maximum Rating System (IEC 60134).*

Symbol	Parameter	Conditions	Min	Max	Unit
V <sub>DD</sub>	supply voltage	active mode	[1] -0.3	+6.0	V
		shutdown mode	-0.3	+7.0	V
V <sub>I</sub>	input voltage		-0.3	V <sub>DD</sub> + 0.3	V
P	power dissipation	derating factor 9.12 mW/K			
		T <sub>amb</sub> = 25 °C	-	1.2	W
		T <sub>amb</sub> = 75 °C	-	690	mW
		T <sub>amb</sub> = 85 °C	-	600	mW
T <sub>amb</sub>	ambient temperature	operating in free air	-40	+85	°C
T <sub>j</sub>	junction temperature	operating	-40	+150	°C
T <sub>stg</sub>	storage temperature		-65	+85	°C

[1] V<sub>DD</sub> is the supply voltage on pin PVDD and pin AVDD.

## 8. Static characteristics

**Table 4. Static characteristics**
 $T_{amb} = 25\text{ }^{\circ}\text{C}$ ; unless otherwise specified.

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
$V_{DD}$	supply voltage	operating	2.5	-	5.5	V
$ V_{O(\text{offset})} $	output offset voltage	measured differentially; inputs AC grounded; $G_{V(\text{cl})} = 6\text{ dB}$ ; $V_{DD} = 2.5\text{ V to }5.5\text{ V}$	-	5	25	mV
PSRR	power supply rejection ratio	$V_{DD} = 2.5\text{ V to }5.5\text{ V}$	-	-75	-55	dB
$V_{i(\text{cm})}$	common-mode input voltage		0.5	-	$V_{DD} - 0.8$	V
CMRR	common mode rejection ratio	inputs are shorted together; $V_{DD} = 2.5\text{ V to }5.5\text{ V}$	-	-69	-50	dB
$V_{IH}$	HIGH-level input voltage	$V_{DD} = 2.5\text{ V to }5.5\text{ V}$ ; pins $\overline{\text{SDL}}$ , $\overline{\text{SDR}}$ , $G_0$ , $G_1$	1.3	-	$V_{DD}$	V
$V_{IL}$	LOW-level input voltage	$V_{DD} = 2.5\text{ V to }5.5\text{ V}$ ; pins $\overline{\text{SDL}}$ , $\overline{\text{SDR}}$ , $G_0$ , $G_1$	0	-	0.35	V
$I_{IH}$	HIGH-level input current	$V_{DD} = 5.5\text{ V}$ ; $V_I = V_{DD}$	-	-	50	$\mu\text{A}$
$I_{IL}$	LOW-level input current	$V_{DD} = 5.5\text{ V}$ ; $V_I = 0\text{ V}$	-	-	5	$\mu\text{A}$
$I_{DD}$	supply current	$V_{DD} = 5.5\text{ V}$ ; no load	-	6	9	mA
		$V_{DD} = 3.6\text{ V}$ ; no load	-	5	7.5	mA
		$V_{DD} = 2.5\text{ V}$ ; no load	-	4	6	mA
$R_{DSon}$	drain-source on-state resistance	$V_{DD} = 5.5\text{ V}$	-	500	-	$\text{m}\Omega$
		$V_{DD} = 3.6\text{ V}$	-	570	-	$\text{m}\Omega$
		$V_{DD} = 2.5\text{ V}$	-	700	-	$\text{m}\Omega$
$Z_{o(\text{sd})}$	shutdown mode output impedance	$V_{SDR} = V_{SDL} = 0.35\text{ V}$	-	2	-	$\text{k}\Omega$
$f_{sw}$	switching frequency	$V_{DD} = 2.5\text{ V to }5.5\text{ V}$	250	300	350	kHz
$G_{V(\text{cl})}$	closed-loop voltage gain	$V_{G0} = V_{G1} = 0.35\text{ V}$	5.5	6	6.5	dB
		$V_{G0} = V_{DD}$ ; $V_{G1} = 0.35\text{ V}$	11.5	12	12.5	dB
		$V_{G0} = 0.35\text{ V}$ ; $V_{G1} = V_{DD}$	17.5	18	18.5	dB
		$V_{G0} = V_{G1} = V_{DD}$	23.5	24	24.5	dB

## 9. Dynamic characteristics

**Table 5. Dynamic characteristics**
 $T_{amb} = 25\text{ }^{\circ}\text{C}$ ;  $R_L = 8\text{ }\Omega$ ; unless otherwise specified.

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
$P_o$	output power	per channel; $f = 1\text{ kHz}$ ; THD+N = 10 %				
		$R_L = 8\text{ }\Omega$ ; $V_{DD} = 5.0\text{ V}$	-	1.3	-	W
		$R_L = 8\text{ }\Omega$ ; $V_{DD} = 3.6\text{ V}$	-	0.72	-	W
		$R_L = 4\text{ }\Omega$ ; $V_{DD} = 5.0\text{ V}$	-	1.2	-	W
THD+N	total harmonic distortion-plus-noise	$V_{DD} = 5.0\text{ V}$ ; $G_{V(cl)} = 6\text{ dB}$ ; $f = 1\text{ kHz}$				
		$P_o = 1\text{ W}$	-	0.14	-	%
		$P_o = 0.5\text{ W}$	-	0.11	-	%
SVRR	supply voltage ripple rejection	$G_{V(cl)} = 6\text{ dB}$ ; $f = 217\text{ Hz}$				
		$V_{DD} = 5.0\text{ V}$	-	-77	-	dB
		$V_{DD} = 3.6\text{ V}$	-	-73	-	dB
CMRR	common mode rejection ratio	$V_{DD} = 5.0\text{ V}$ ; $G_{V(cl)} = 6\text{ dB}$ ; $f = 217\text{ Hz}$	-	-69	-	dB
$Z_i$	input impedance	$G_{V(cl)} = 6\text{ dB}$	-	28.1	-	k $\Omega$
		$G_{V(cl)} = 12\text{ dB}$	-	17.3	-	k $\Omega$
		$G_{V(cl)} = 18\text{ dB}$	-	9.8	-	k $\Omega$
		$G_{V(cl)} = 24\text{ dB}$	-	5.2	-	k $\Omega$
$t_{d(sd-startup)}$	delay time from shutdown to start-up	$V_{DD} = 3.6\text{ V}$	-	3.5	-	ms
$V_{n(o)}$	output noise voltage	$V_{DD} = 3.6\text{ V}$ ; $f = 20\text{ Hz}$ to $20\text{ kHz}$ ; inputs are AC grounded				
		no weighting	-	35	-	$\mu\text{V}$
		A weighting	-	27	-	$\mu\text{V}$

10. Typical performance curves

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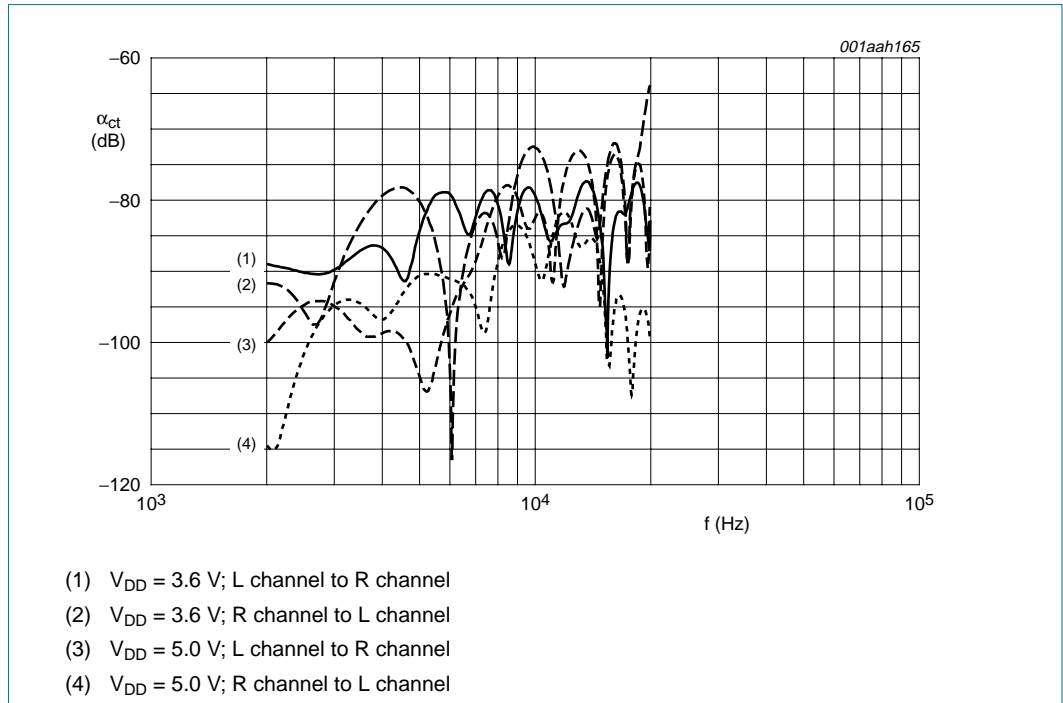


Fig 4. Crosstalk (stepped all-to-one) as a function of frequency

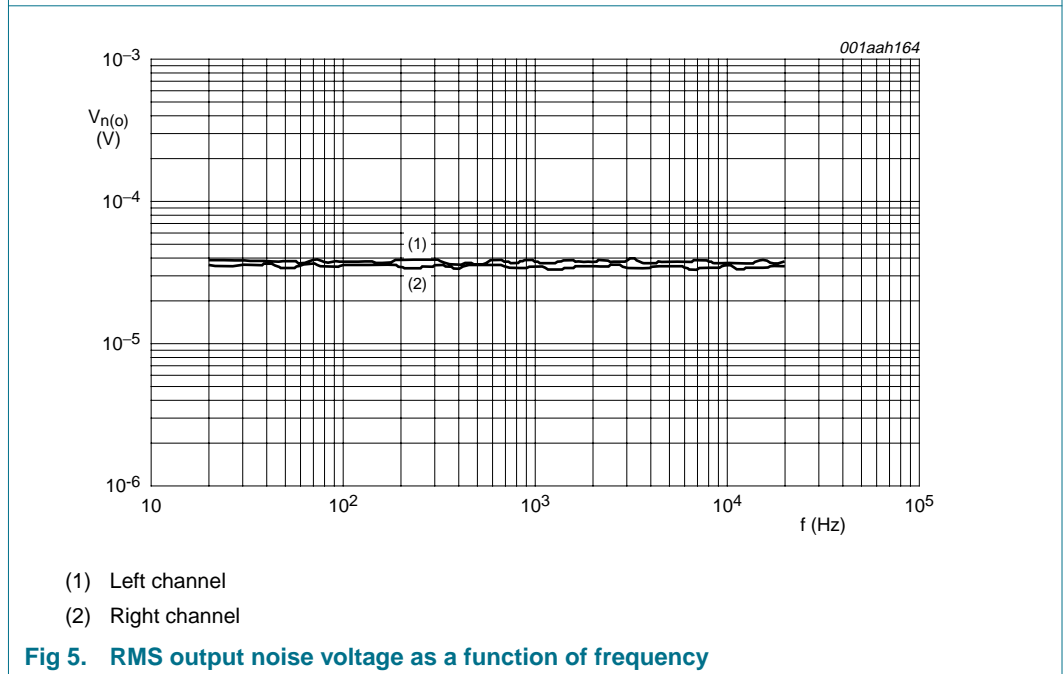
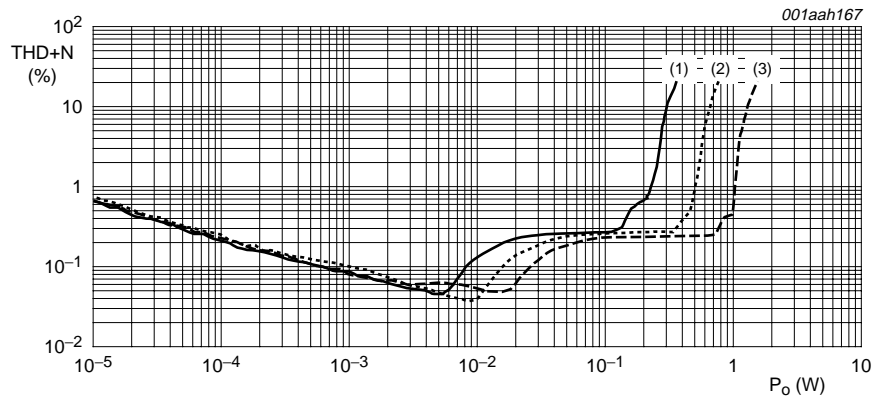
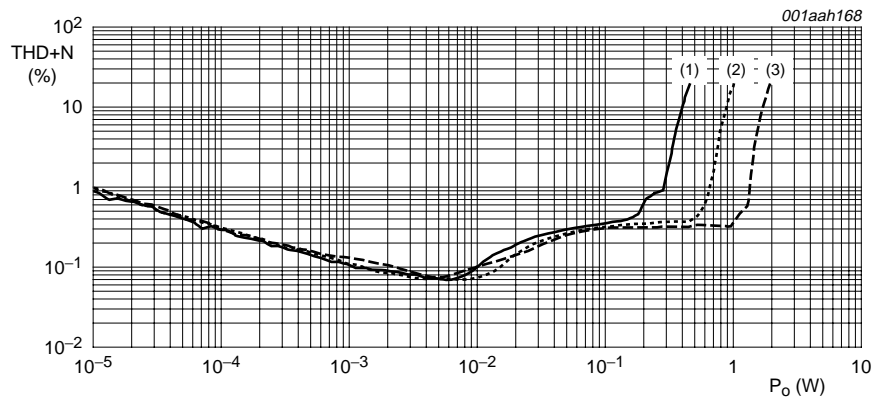


Fig 5. RMS output noise voltage as a function of frequency



a.  $R_L = 8 \Omega$



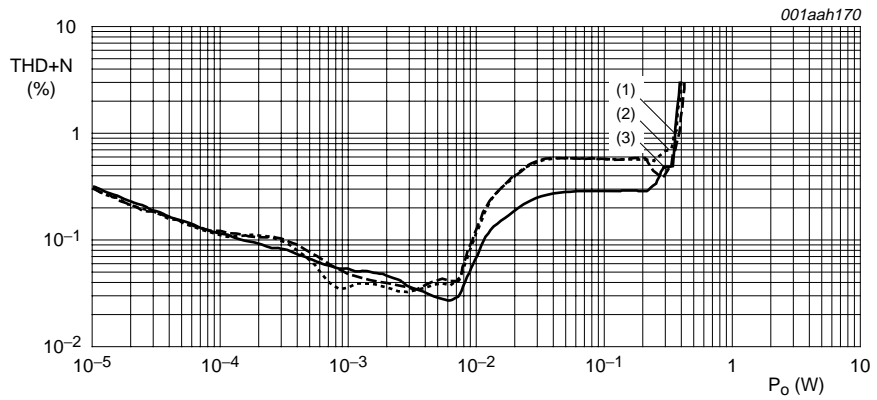
b.  $R_L = 4 \Omega$

- (1)  $V_{DD} = 2.5 \text{ V}$
- (2)  $V_{DD} = 3.6 \text{ V}$
- (3)  $V_{DD} = 5.0 \text{ V}$

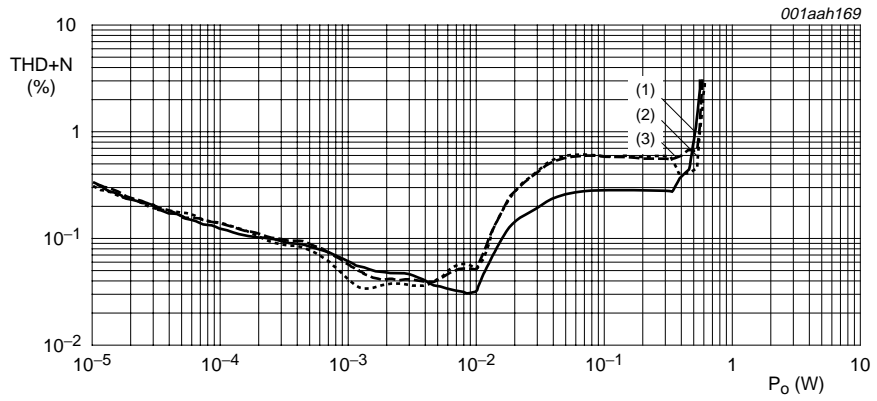
Fig 6. Total harmonic distortion-plus-noise as a function of output power;  $G_{V(cl)} = 6 \text{ dB}$



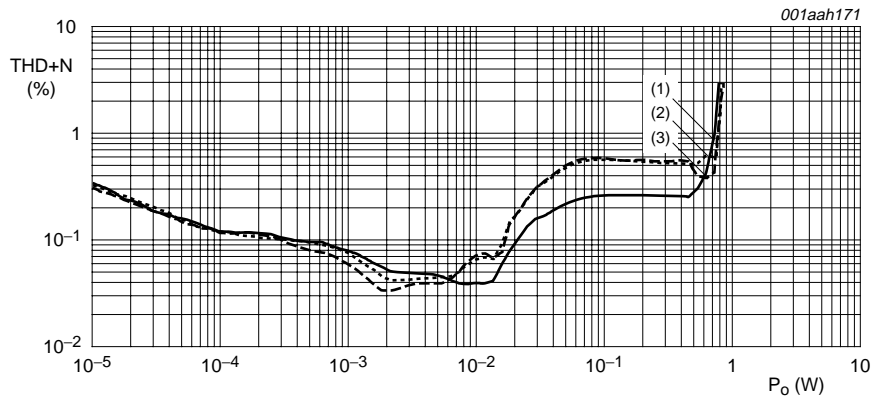
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a.  $V_{DD} = 3.0\text{ V}$



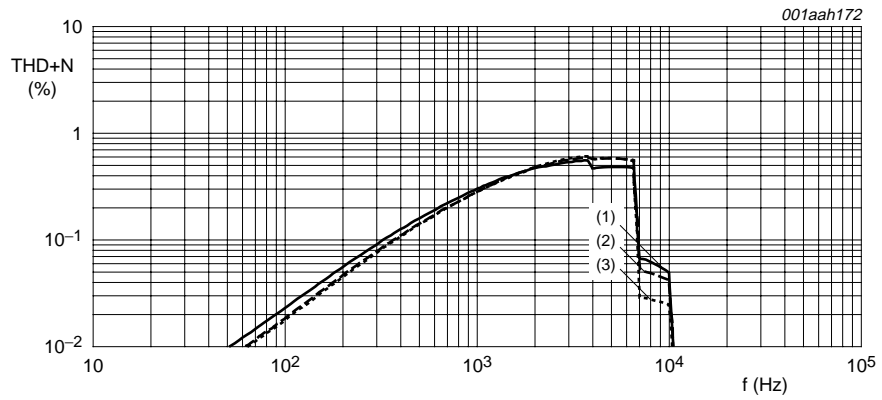
b.  $V_{DD} = 3.6\text{ V}$



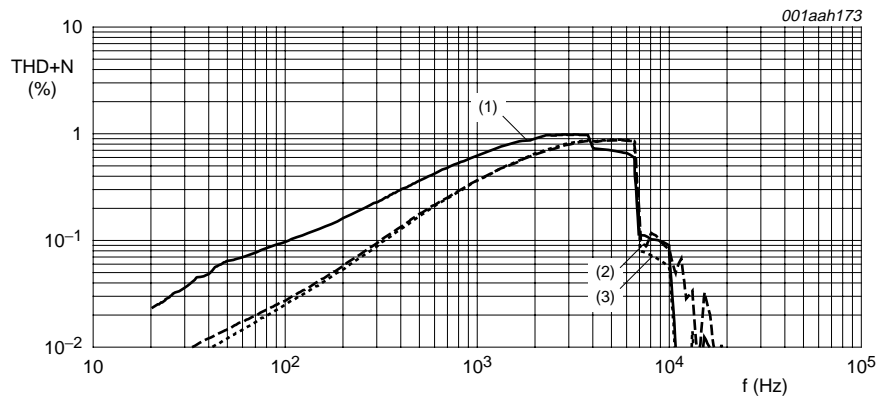
c.  $V_{DD} = 4.2\text{ V}$

- (1)  $f_i = 1\text{ kHz}$
- (2)  $f_i = 3\text{ kHz}$
- (3)  $f_i = 5\text{ kHz}$

**Fig 7. Total harmonic distortion-plus-noise as a function of output power;  $R_L = 8\ \Omega$ ;  $G_{V(cl)} = 6\text{ dB}$**



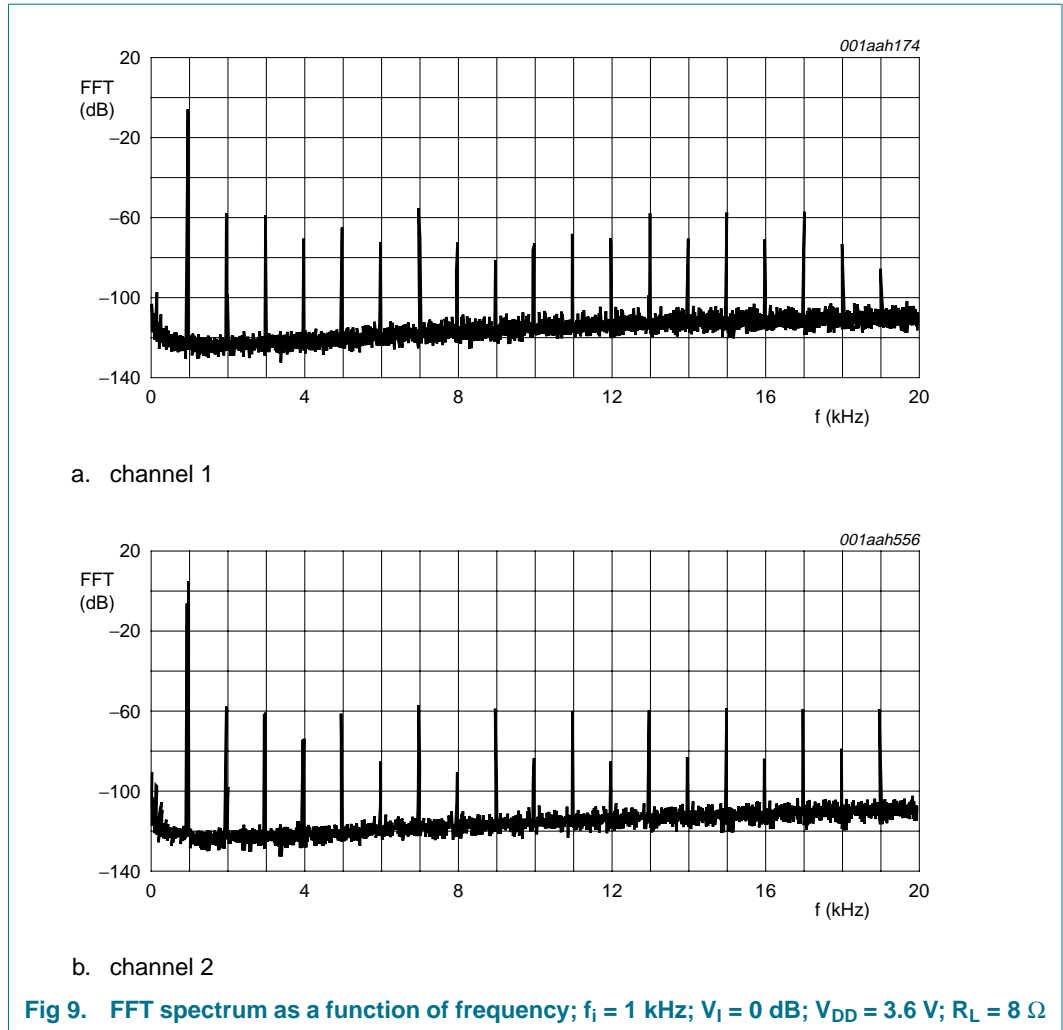
a.  $R_L = 8 \Omega$



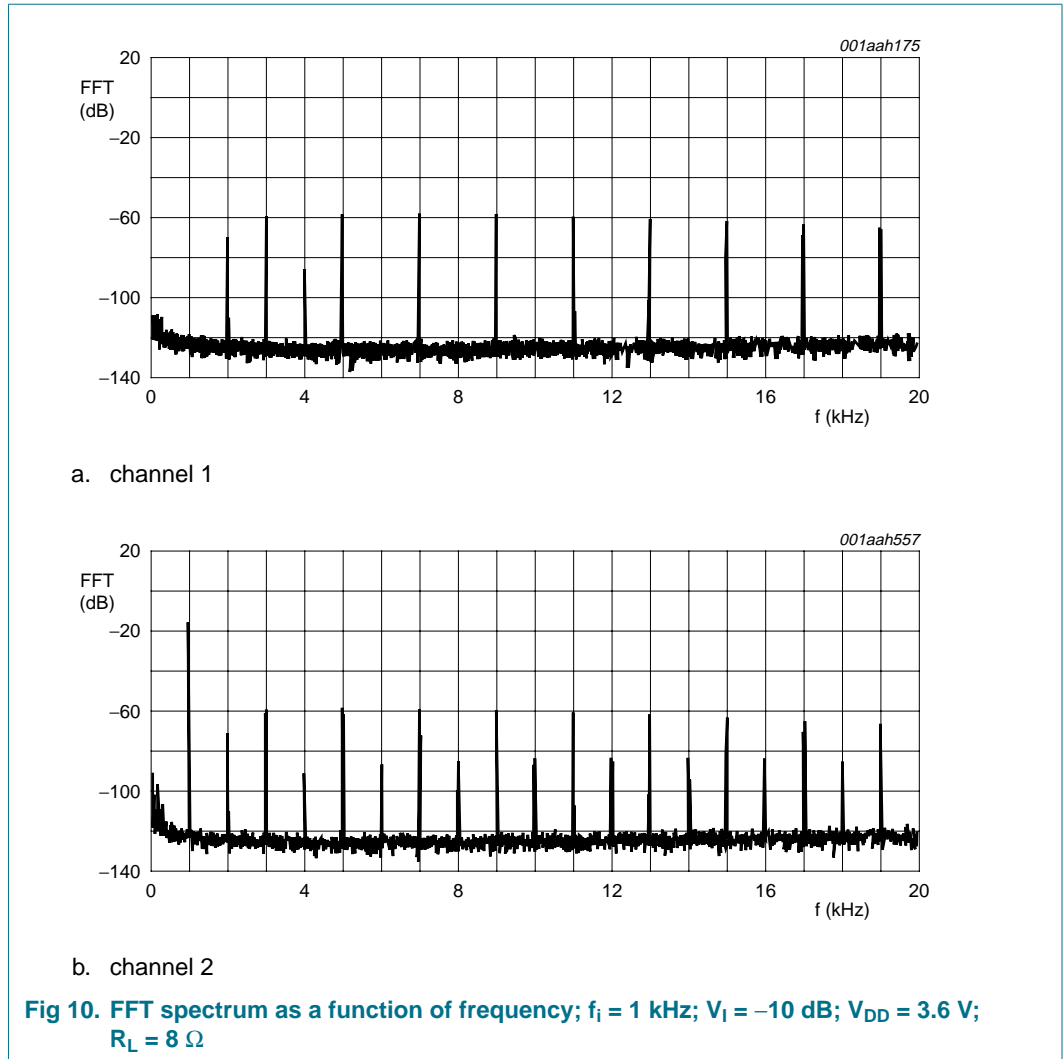
b.  $R_L = 4 \Omega$

- (1)  $V_I = 900 \text{ mV}$
- (2)  $V_I = 725 \text{ mV}$
- (3)  $V_I = 525 \text{ mV}$

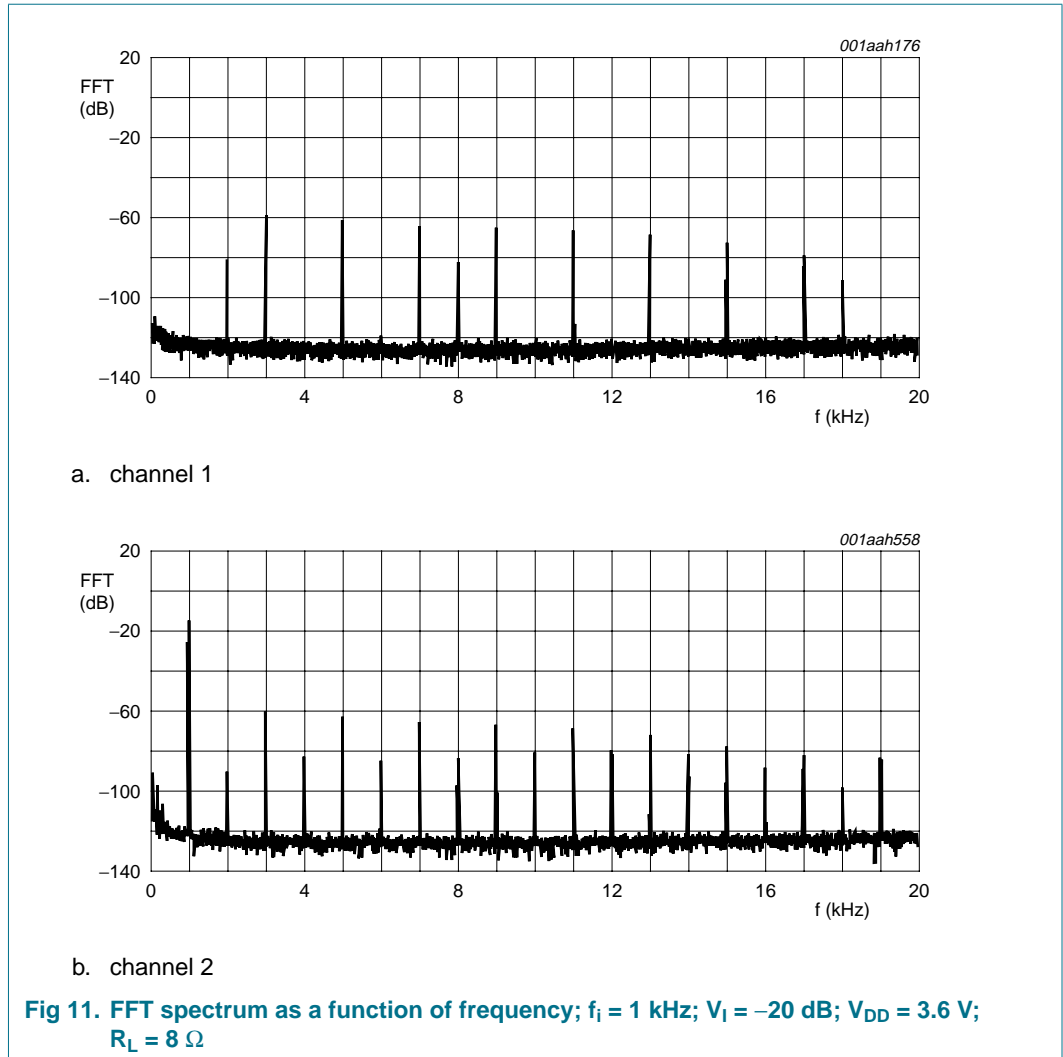
**Fig 8. Total harmonic distortion-plus-noise as a function of frequency;  $V_{DD} = 3.6 \text{ V}$**

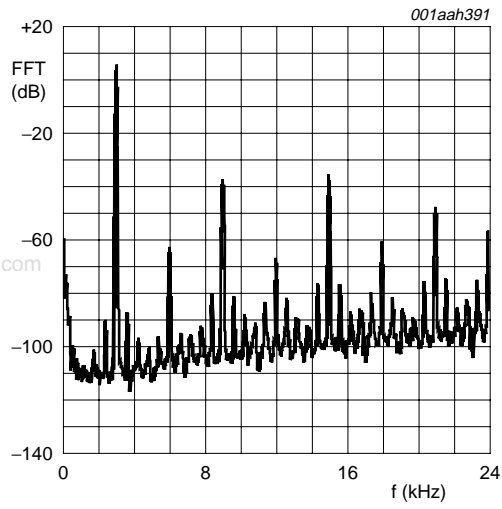


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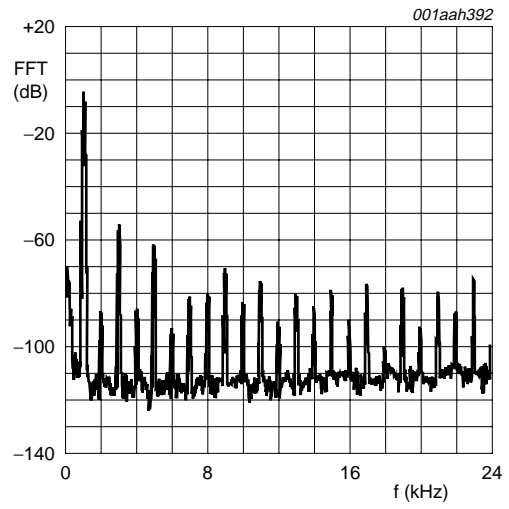


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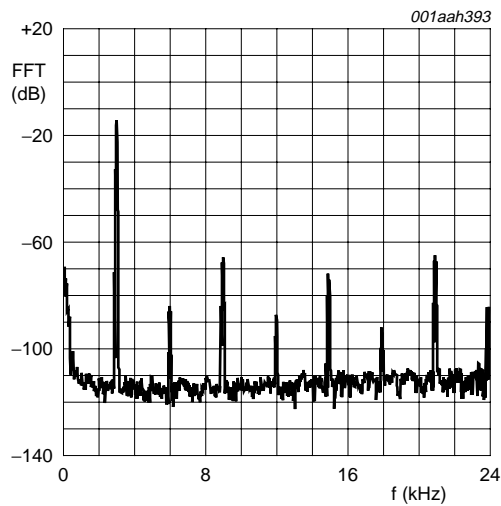




a.  $V_1 = 0 \text{ dB}$

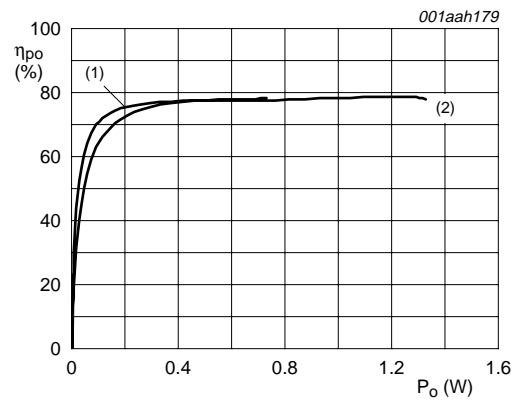
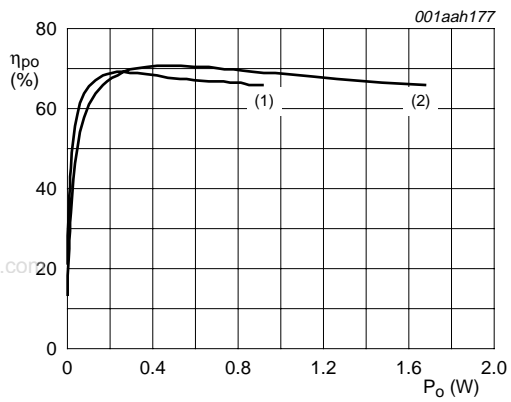


b.  $V_1 = -10 \text{ dB}$



c.  $V_1 = -20 \text{ dB}$

Fig 12. FFT spectrum as a function of frequency;  $f_i = 3 \text{ kHz}$ ;  $V_{DD} = 3.6 \text{ V}$ ;  $R_L = 8 \Omega$



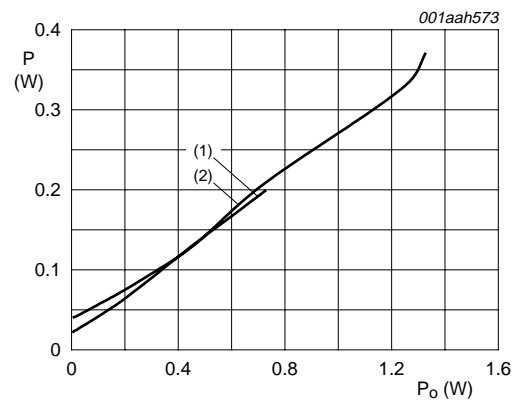
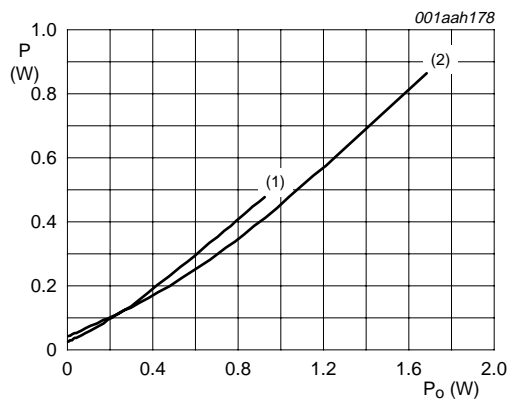
a.  $R_L = 4 \Omega$

(1)  $V_{DD} = 3.6 \text{ V}$

(2)  $V_{DD} = 5.0 \text{ V}$

b.  $R_L = 8 \Omega$

Fig 13. Output power efficiency as a function of output power



a.  $R_L = 4 \Omega$

(1)  $V_{DD} = 3.6 \text{ V}$

(2)  $V_{DD} = 5.0 \text{ V}$

b.  $R_L = 8 \Omega$

Fig 14. Power dissipation as a function of output power

## 11. Application information

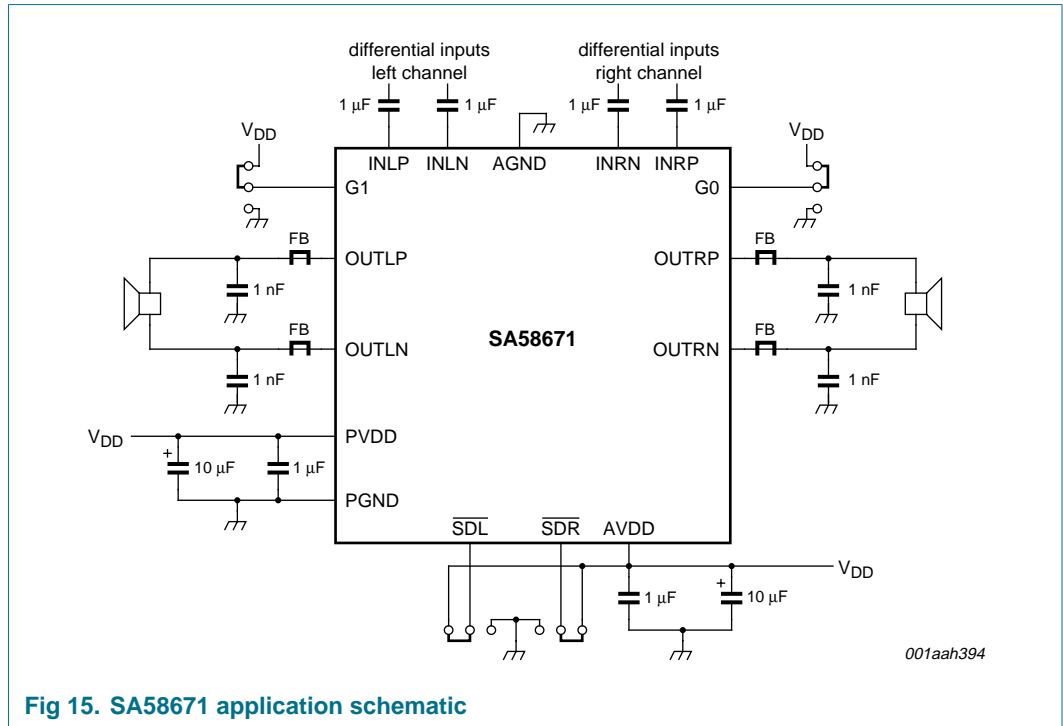


Fig 15. SA58671 application schematic

### 11.1 Power supply decoupling considerations

The SA58671 is a stereo class-D audio amplifier that requires proper power supply decoupling to ensure the rated performance for THD+N and power efficiency. To decouple high frequency transients, power supply spikes and digital noise on the power bus line, a low Equivalent Series Resistance (ESR) capacitor of typically 1 μF is placed as close as possible to the PVDD pins of the device. It is important to place the decoupling capacitor at the power pins of the device because any resistance or inductance in the PCB trace between the device and the capacitor can cause a loss in efficiency. Additional decoupling using a larger capacitor, 4.7 μF or greater, may be done on the power supply connection on the PCB to filter low frequency signals. Usually this is not required due to high PSRR of the device.

### 11.2 Input capacitor selection

The SA58671 does not require input coupling capacitors when used with a differential audio source that is biased from 0.5 V to V<sub>DD</sub> – 0.8 V. In other words, the input signal must be biased within the common-mode input voltage range. If high pass filtering is required or if it is driven using a single-ended source, input coupling capacitors are required.

The 3 dB cut-off frequency created by the input coupling capacitor and the input resistors (see Table 6) is calculated by Equation 1:

$$f_{-3dB} = \frac{1}{2\pi \times R_i \times C_i} \tag{1}$$



**Table 6. Gain selection**

G1	G0	Gain (V/V)	Gain (dB)	Input impedance (kΩ)
LOW	LOW	2	6	28.1
LOW	HIGH	4	12	17.3
HIGH	LOW	8	18	9.8
HIGH	HIGH	16	24	5.2

Since the value of the input decoupling capacitor and the input resistance determined by the gain setting affects the low frequency performance of the audio amplifier, it is important to consider this during the system design. Small speakers in wireless and cellular phones usually do not respond well to low frequency signals, so the 3 dB cut-off frequency may be increased to block the low frequency signals to the speakers. Not using input coupling capacitors may increase the output offset voltage.

[Equation 1](#) is solved for  $C_i$ :

$$C_i = \frac{I}{2\pi \times R_i \times f_{-3dB}} \quad (2)$$

### 11.3 PCB layout considerations

Component location is very important for performance of the SA58671. Place all external components very close to the device. Placing decoupling capacitors directly at the power supply pins increases efficiency because the resistance and inductance in the trace between the device power supply pins and the decoupling capacitor causes a loss in power efficiency.

The trace width and routing are also very important for power output and noise considerations.

For high current terminals (PVDD, PGND and audio output), the trace widths should be maximized to ensure proper performance and output power. Use at least 500 μm wide traces.

For the input pins (INRP, INRN, INLP and INLN), the traces must be symmetrical and run side-by-side to maximize common-mode cancellation.

### 11.4 Filter-free operation and ferrite bead filters

A ferrite bead low-pass filter can be used to reduce radio frequency emissions in applications that have circuits sensitive to frequencies greater than 1 MHz. A ferrite bead low-pass filter functions well for amplifiers that must pass FCC unintentional radiation requirements for frequencies greater than 30 MHz. Choose a bead with high-impedance at high frequencies and very low-impedance at low frequencies. In order to prevent distortion of the output signal, select a ferrite bead with adequate current rating.

For applications in which there are circuits that are EMI sensitive to low frequency (< 1 MHz) and there are long leads from amplifier to speaker, it is necessary to use an LC output filter.

11.5 Efficiency and thermal considerations

The maximum ambient temperature depends on the heat transferring ability of the heat spreader on the PCB layout. In [Table 3 “Limiting values”](#), power dissipation, the power derating factor is given as 9.12 mW/K. The device thermal resistance,  $R_{th(j-a)}$  is the reciprocal of the power derating factor. Convert the power derating factor to  $R_{th(j-a)}$  by [Equation 3](#):

$$R_{th(j-a)} = \frac{1}{\text{derating factor}} = \frac{1}{0.00912} = 110 \text{ K/W} \tag{3}$$

For a maximum allowable junction temperature,  $T_j = 150 \text{ }^\circ\text{C}$  and  $R_{th(j-a)} = 110 \text{ K/W}$  and a maximum device dissipation of 0.6 W (300 mW per channel) and for 1.2 W per channel output power, 4  $\Omega$  load, 5 V supply, the maximum ambient temperature is calculated using [Equation 4](#):

$$T_{amb(max)} = T_{j(max)} - (R_{th(j-a)} \times P_{max}) = 150 - (110 \times 0.60) = 84 \text{ }^\circ\text{C} \tag{4}$$

The maximum ambient temperature is 84  $^\circ\text{C}$  at maximum power dissipation for 5 V supply and 4  $\Omega$  load. If the junction temperature of the SA58671 rises above 150  $^\circ\text{C}$ , the thermal protection circuitry turns the device off; this prevents damage to IC. Using speakers greater than 4  $\Omega$  further enhances thermal performance and battery lifetime by reducing the output load current and increasing amplifier efficiency.

11.6 Additional thermal information

The SA58671 16 bump WLCSP package ground bumps are soldered directly to the PCB heat spreader. By the use of thermal vias, the bumps may be soldered directly to a ground plane or special heat sinking layer designed into the PCB. The thickness and area of the heat spreader may be maximized to optimize heat transfer and achieve lowest package thermal resistance.

12. Test information

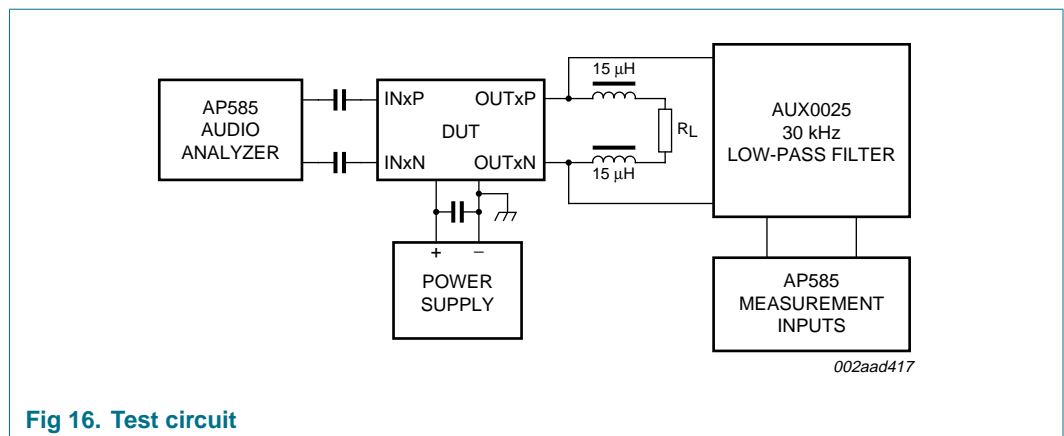


Fig 16. Test circuit

13. Package outline

WLCSP16: wafer level chip-size package; 16 bumps; 2.06 x 2.11 x 0.6 mm

SA58671UK

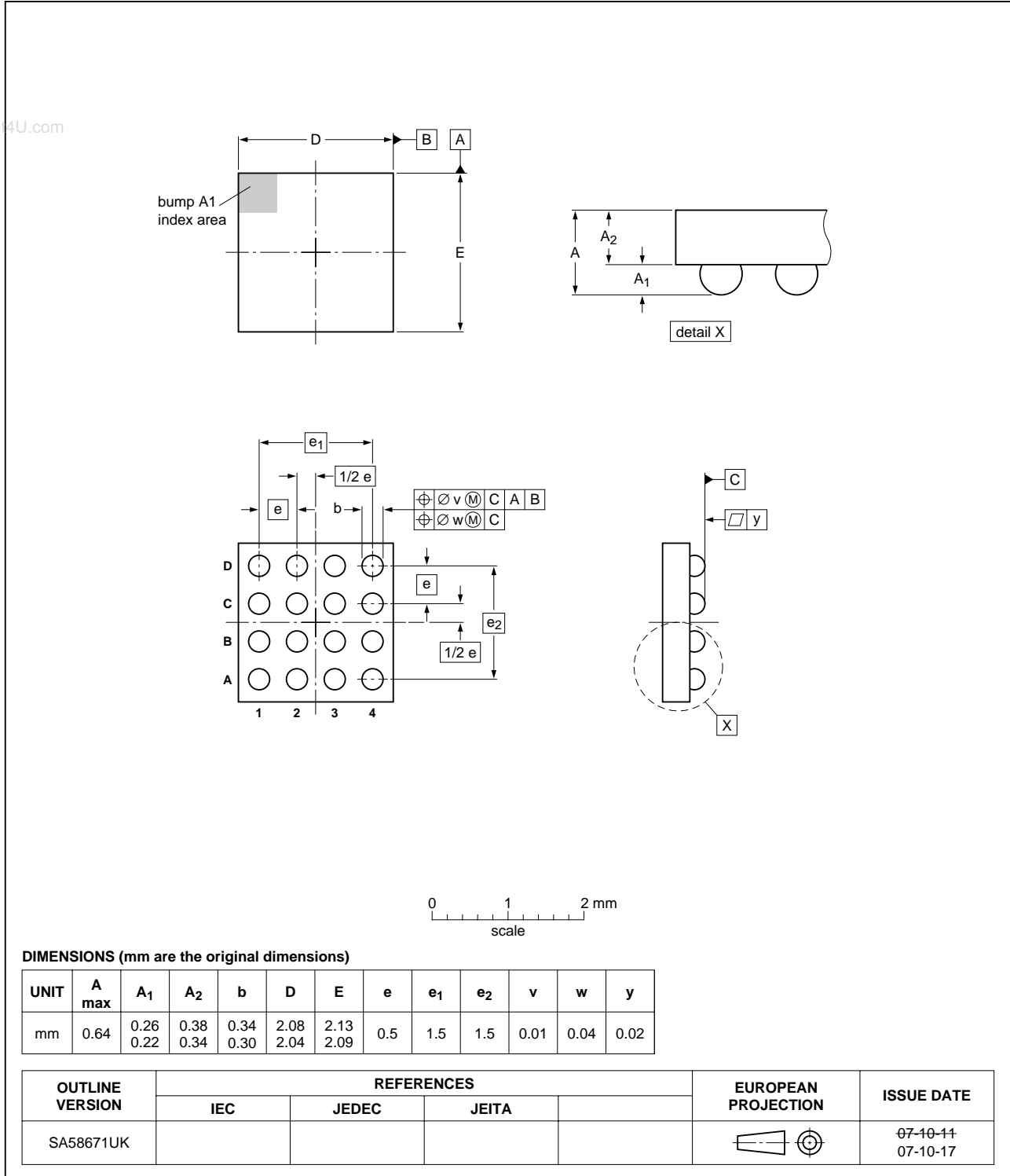


Fig 17. Package outline WLCSP16

## 14. Soldering

This text provides a very brief insight into a complex technology. A more in-depth account of soldering ICs can be found in Application Note *AN10365 "Surface mount reflow soldering description"*.

### 14.1 Introduction to soldering

Soldering is one of the most common methods through which packages are attached to Printed Circuit Boards (PCBs), to form electrical circuits. The soldered joint provides both the mechanical and the electrical connection. There is no single soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and Surface Mount Devices (SMDs) are mixed on one printed wiring board; however, it is not suitable for fine pitch SMDs. Reflow soldering is ideal for the small pitches and high densities that come with increased miniaturization.

### 14.2 Wave and reflow soldering

Wave soldering is a joining technology in which the joints are made by solder coming from a standing wave of liquid solder. The wave soldering process is suitable for the following:

- Through-hole components
- Leaded or leadless SMDs, which are glued to the surface of the printed circuit board

Not all SMDs can be wave soldered. Packages with solder balls, and some leadless packages which have solder lands underneath the body, cannot be wave soldered. Also, leaded SMDs with leads having a pitch smaller than ~0.6 mm cannot be wave soldered, due to an increased probability of bridging.

The reflow soldering process involves applying solder paste to a board, followed by component placement and exposure to a temperature profile. Leaded packages, packages with solder balls, and leadless packages are all reflow solderable.

Key characteristics in both wave and reflow soldering are:

- Board specifications, including the board finish, solder masks and vias
- Package footprints, including solder thieves and orientation
- The moisture sensitivity level of the packages
- Package placement
- Inspection and repair
- Lead-free soldering versus PbSn soldering

### 14.3 Wave soldering

Key characteristics in wave soldering are:

- Process issues, such as application of adhesive and flux, clinching of leads, board transport, the solder wave parameters, and the time during which components are exposed to the wave
- Solder bath specifications, including temperature and impurities

### 14.4 Reflow soldering

Key characteristics in reflow soldering are:

- Lead-free versus SnPb soldering; note that a lead-free reflow process usually leads to higher minimum peak temperatures (see [Figure 18](#)) than a PbSn process, thus reducing the process window
- Solder paste printing issues including smearing, release, and adjusting the process window for a mix of large and small components on one board
- Reflow temperature profile; this profile includes preheat, reflow (in which the board is heated to the peak temperature) and cooling down. It is imperative that the peak temperature is high enough for the solder to make reliable solder joints (a solder paste characteristic). In addition, the peak temperature must be low enough that the packages and/or boards are not damaged. The peak temperature of the package depends on package thickness and volume and is classified in accordance with [Table 7](#) and [8](#)

**Table 7. SnPb eutectic process (from J-STD-020C)**

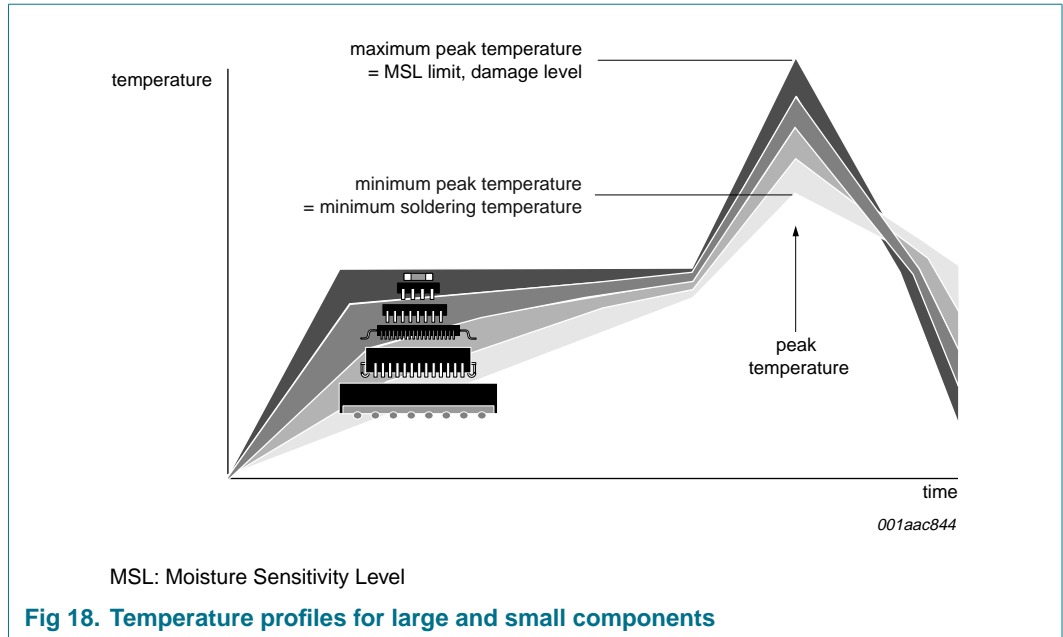
Package thickness (mm)	Package reflow temperature (°C)	
	Volume (mm <sup>3</sup> )	
	< 350	≥ 350
< 2.5	235	220
≥ 2.5	220	220

**Table 8. Lead-free process (from J-STD-020C)**

Package thickness (mm)	Package reflow temperature (°C)		
	Volume (mm <sup>3</sup> )		
	< 350	350 to 2000	> 2000
< 1.6	260	260	260
1.6 to 2.5	260	250	245
> 2.5	250	245	245

Moisture sensitivity precautions, as indicated on the packing, must be respected at all times.

Studies have shown that small packages reach higher temperatures during reflow soldering, see [Figure 18](#).



For further information on temperature profiles, refer to Application Note AN10365 “Surface mount reflow soldering description”.

## 15. Abbreviations

**Table 9. Abbreviations**

Acronym	Description
DUT	Device Under Test
DVD	Digital Video Disc
EMI	ElectroMagnetic Interference
ESR	Equivalent Series Resistance
FFT	Fast Fourier Transform
LC	inductor-capacitor filter
PC	Personal Computer
PCB	Printed-Circuit Board
PDA	Personal Digital Assistant
PSRR	Power Supply Rejection Ratio
PWM	Pulse Width Modulator
USB	Universal Serial Bus
WLCSP	Wafer Level Chip-Size Package

## 16. Revision history

**Table 10. Revision history**

Document ID	Release date	Data sheet status	Change notice	Supersedes
SA58671_1	20071221	Product data sheet	-	-

## 17. Legal information

### 17.1 Data sheet status

Document status <sup>[1][2]</sup>	Product status <sup>[3]</sup>	Definition
Objective [short] data sheet	Development	This document contains data from the objective specification for product development.
Preliminary [short] data sheet	Qualification	This document contains data from the preliminary specification.
Product [short] data sheet	Production	This document contains the product specification.

[1] Please consult the most recently issued document before initiating or completing a design.

[2] The term 'short data sheet' is explained in section "Definitions".

[3] The product status of device(s) described in this document may have changed since this document was published and may differ in case of multiple devices. The latest product status information is available on the Internet at URL <http://www.nxp.com>.

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