

Description

The SARS⁽¹⁾ is an auxiliary switch diode especially designed for snubber circuits, which are used in the primary sides of flyback switched-mode power supplies.

Being capable of reducing the ringing voltage generated at power MOSFET turn-off, the SARS-incorporated snubber circuits allow better cross regulation of multiple outputs.

The SARS can also improve power supply efficiency by partially transferring such ringing voltage into the secondary side of a power supply unit.

Features

- Improves Cross Regulation
- Reduces Noise
- Improves Efficiency

Applications

For switched-mode power supplies (SMPS) with flyback topology such as:

- White Goods
- Adaptor
- Industrial Equipment

Typical Application



Package

SARS01 (Axial φ 2.7 / φ 0.60)



Not to scale

Selection Guide

R _{S2}	Part Number	I _{F(AV)}	V _F (max.)	Power Supply Output Power, Po*
External Resistor	SARS01	1.2 A	0.92 V	up to 50 W
	SARS02	1.5 A	0.92 V	up to 100 W
	SARS05	1 A	1.05 V	up to 50 W
Built-in 22 Ω	SARS10	0.3 A	13 V	up to 300 W

 \ast $P_{\rm O}$ represents a reference value for product selection. When using the product, you should monitor temperature rises during actual operation.

⁽¹⁾ The "SARS" represents any one of the SARSxx devices listed in this document.

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Absolute Maximum Ratings

22 22/3

Parameter	Symbol	Conditions	Rating	Unit	Remarks
Transient Peak Reverse Voltage	V _{RSM}		800	V	
Peak Repetitive Reverse Voltage	V _{RM}		800	V	
			1.2	A	SARS01
Average Forward Current ⁽²⁾	T		1.2		SARS02
Average Forward Current	$\mathbf{I}_{\mathrm{F}(\mathrm{AV})}$		1.0		SARS05
			0.3		SARS10
	I _{FSM}	Half cycle sine wave, positive side, 10 ms, 1 shot	110	A	SARS01
			100		SARS02
Surge Forward Current			30		SARS05
		1 ms, square pulse, 1 shot	1.5		SARS10
	I ² t	$1 \text{ ms} \le t \le 10 \text{ ms}$	60.5	A ² s	SARS01
I ² t Limiting Value			50		SARS02
			4.5		SARS05
					SARS10
Innation Tommenoture	TJ	ξO'	-40 to 150	°C	SARS01/02/05
Junction Temperature			-20 to 125	C	SARS10
Storogo Tommorotomo	T		-40 to 150	°C	SARS01/02/05
Storage Temperature	I STG	0	-20 to 125		SARS10
Power Dissipation	Р		3.0	W	SARS10

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⁽²⁾ See the derating curves of each product.

Electrical Characteristics

Parameter	Symbol	Conditions	Min.	Тур.	Max.	Unit	Remarks
	V _F	$I_F = 1.2 A$	—		0.92		SARS01
Forward Voltage Drop		$I_{\rm F} = 1.5 ~{\rm A}$	—		0.92	V	SARS02
		$I_{\rm F} = 1.0 \ {\rm A}$	—		- 1.05 V	SARS05	
		$I_F\!=0.5~A$			13		SARS10
					10		SARS01
	I _R	$V_R = V_{RM}$	—	_	10	μA	SARS02
Reverse Leakage Current			—	_	5		SARS05
			_		10		SARS10
Reverse Leakage Current under High Temperature	H·I _R	$V_{R} = V_{RM},$ $T_{J} = 100 \ ^{\circ}C$			50	μA	SARS01/02/05
		$V_R = V_{RM},$ $T_J = 125 \ ^{\circ}C$		_	100		SARS10
			2		18		SARS01
Reverse Recovery Time	t _{rr}	$I_F = I_{RP} = 100 \text{ mA},$ $T_J = 25 \text{ °C},$ 90% recovery point	2		18	μs	SARS02
			2		19		SARS05
			1		9		SARS10
			_	_	20		SARS01
Thormal Desistance	R _{th(J-L)}	(3)	_		15	°C/W	SARS02
Thermal Resistance			—	_	20		SARS05
	R _{th(J-C)}	(4)			15	°C/W	SARS10

Unless otherwise specified, $T_A = 25$ °C, only the SARS10 incorporates a resistor (22 Ω).



 $^{^{(3)}}$ $R_{th(J\text{-}L)}$ is thermal resistance between junction and lead. $^{(4)}$ $R_{th(J\text{-}c)}$ is thermal resistance between junction and case.







 $(V_R = 0 V, T_J = 150 °C)$





 $(T_{\rm J} = 150 \ ^{\circ}{\rm C})$



Figure 11. V_F vs. I_F Typical Characteristics

Figure 12. V_R vs. I_R Typical Characteristics

SARS05 Rating and Characteristic Curves



Figure 13. $I_{F(AV)}$ vs. P_F Power Dissipation Curves $(T_J = 150 \text{ °C})$







Figure 14. V_R vs. P_R Power Dissipation Curves (T_J = 150 °C)







Figure 17. V_F vs. I_F Typical Characteristics



vs. I_R Typical Characteristics Figure 1



Figure 19. I_{F(AV)} vs. P_F Power Dissipation Curves $(T_J = 125 \ ^{\circ}C)$





SARS10 Rating and Characteristic Curves



Figure 23. V_R vs. I_R Typical Characteristics

Physical Dimensions and Marking Diagrams

• SARS01

Axial (φ 2.7 / φ 0.6)



NOTES:

- Dimensions in millimeters
- Bare lead: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time, within the following limits: Flow: $260 \pm 5 \text{ °C} / 10 \pm 1 \text{ s}, 2 \text{ times}$
 - Soldering Iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)

• SARS02

Axial ($\phi 4 / \phi 0.78$)



NOTES:

- Dimensions in millimeters
- Bare lead: Pb-free (RoHS compliant)

- When soldering the products, be sure to minimize the working time within the following limits: Flow: $260 \pm 5 \text{ °C} / 10 \pm 1 \text{ s}, 2 \text{ times}$ Soldering iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)

• SARS05



- Dimensions in millimeters
- Bare lead frame: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time, within the following limits: Flow: $260 \pm 5 \text{ °C} / 10 \pm 1 \text{ s}, 2 \text{ times}$ Soldering Iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)
- The recommended screw torque for TO220F: 0.490 N·m to 0.686 N·m (5 kgf·cm to 7 kgf·cm)

Operational Comparison of Clamp Snubber Circuits

Figure 24 shows a general clamp snubber circuit. In the circuit, the surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop, and is consumed by R_{S1} through the energy discharge loop. All the consumed energy becomes loss in R_{S1} . In addition, the ringing of surge voltage results in poor cross regulation of multi-outputs.



Figure 24. General Clamp Snubber Circuit



Figure 25. Waveforms of General Clamp Snubber Circuit



Figure 26. Enlarged View of Figure 25

Figure 27 shows the clamp snubber circuit using the SARS. The surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop. Since the reverse recovery time, trr, of the SARS is a relatively long period, the energy charged to C_S is discharged to the reverse direction of the surge absorb loop until C_S voltage is equal to the flyback voltage. Some discharged energy is transferred to secondary side. Thus, the power supply efficiency improves.

In addition, the power supply using the SARS reduces the ringing voltage. Thus, the cross regulation of multi-outputs can be improved.





Figure 29. Enlarged View of Figure 28

Power Dissipation and Junction Temperature Calculation

Figure 30 shows a typical application using the SARS. Figure 31 shows the operating waveforms of the SARS.

The power dissipation of the SARS is calculated as follows:

- 1) The waveforms of the SARS voltage, V_{SARS} , and the SARS current, I_{SARS} , are measured in actual application operation. $V_{SARS} \times I_{SARS}$ is calculated by the math function of oscilloscope. (Since the SARS10 incorporates a resistor, $V_{SARS(10)}$ is measured.)
- 2) The each average energy $(P_1, P_2 \cdots P_k)$ is measured at period of each polarity of $V_{SARS} \times I_{SARS} (t_1, t_2, \cdots t_k)$ as shown in Figure 30 by the automatic measurement function of the oscilloscope.
- 3) The power dissipation of the SARS, P_{SARS}, is calucultated by Equation (1):

$$P_{SARS} = \frac{1}{T} (|P_1 \times t_1| + |P_2 \times t_2| + \dots |P_k \times t_k|)$$
 (1)

where:

 P_{SARS} is power dissipation of the SARS, T is switching cycle of power MOSFET (s), and P_k is average energy of period t_k (W).

A differential probe is recommended to use for the measurement of V_{SARS} . Please conform to the oscilloscope manual about power dissipation measurement including the delay compensation of probe.



Figure 30. Typical Application



In addition, by using the temperature of the SARS in actual application operation, the estimated junction temperature of the SARS is calculated by Equation (2) and Equation (3). It should be enough lower than T_J of the absolute maximum rating.

• SARS01/02/05

$$T_{J(SARS)} = T_{L} + \theta_{J-L} \times P_{SARS} (^{\circ}C)$$
(2)

where:

 $T_{J(SARS)}$ is junction temperature of the SARS, T_L is lead temperature of the SARS, and θ_{J-L} is thermal resistance between junction to lead.

• SARS10

$$T_{J(SARS)} = T_{C} + \theta_{J-C} \times P_{SARS} (^{\circ}C)$$
(3)

Where:

 $T_{J(SARS)}$ is junction temperature of the SARS, T_C is case temperature of the SARS, and θ_{J-C} is thermal resistance between junction to case.

Parameter Setting of Snubber Circuit using SARS

The temperature of the SARS and peripheral components should be measured in actual application operation.

The reference values of snubber circuit using the SARS are as follows:

• C_s

680 pF to 0.01 µF.

The voltage rating is selected according to the voltage subtraced the input voltage from the peak of V_{DS} .

• **R**_{S1}

 R_{S1} is the bias resistance to turn off the SARS, and is 100 k Ω to 1 $M\Omega.$

Since a high voltage is applied to R_{S1} that has high resistance, the following should be considered according to the requirement of the application:

- Select a resistor designed for electromigration, or
- Connect more resistors in series so that the applied voltages of individual resistors can be reduced.

The power rating of resistor should be selected from the measurement of the effective current of R_{S1} based on actual operation in the application.

• **R**_{S2}

 R_{s2} is the limited resistance in the energy discharging. The value of 22 Ω to 220 Ω is connected to the SARS in series (the SARS10 incorporates R_{s2}).

The power rating of resistor should be selected from the measurement of the effective current of R_{S2} based on actual operation in the application.

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Reference Design of Power Supply

This section provides the information on a reference design, including power supply specifications, a circuit diagram, the bill of materials, and transformer specifications.

• Power Supply Specifications

Item	Specification
Input Voltage	85 VAC to 265 VAC
Output Power	34.8 W (40.4 W peak)
Output 1	8 V / 0.5 A
Output 2	14 V / 2.2 A (2.6 A peak)

• Circuit Schematic



• Bill of Materials

Symbol	Ratings ⁽¹⁾	Recommended Part No.	Symbol	Ratings ⁽¹⁾	Recommended Part No.
C1 ⁽²⁾	Film, 0.1 µF, 275 V		D52	Schottky, 100 V, 10 A	FMEN-210A
C2 ⁽²⁾	Electrolytic, 150 µF, 400 V		F1	Fuse, 250 V AC, 3 A	
C3	Ceramic, 1000 pF, 1 kV	7	L1 ⁽²⁾	CM inductor, 3.3 mH	
C4	Ceramic, 0.01 µF		PC1	Optocoupler, PC123 or equiv.	
C5	Electrolytic, 22 µF, 50 V		R1 ⁽³⁾	Metal oxide, 330 kΩ, 1 W	
C6 ⁽²⁾	Ceramic, 15 pF/2 kV		R2	47 Ω, 1 W	
C7 ⁽²⁾	Ceramic, 2200 pF, 250 V		R3	10 Ω	
C51 ⁽²⁾	Electrolytic, 680 µF, 25 V		R4 ⁽²⁾	0.47 Ω, 1/2 W	
C52	Electrolytic, 680 µF, 25 V		R51	1 kΩ	
C53	Electrolytic, 470 µF, 16 V		R52	1.5 kΩ	
C54 ⁽²⁾	Ceramic, 0.1 µF, 50 V		R53 ⁽²⁾	100 kΩ	
D1	600 V, 1 A	EM01A	R54 ⁽²⁾	6.8 kΩ	
D2	600 V, 1 A	EM01A	R55	± 1%, 39 kΩ	
D3	600 V, 1 A	EM01A	R56	\pm 1%, 10 k Ω	
D4	600 V, 1 A	EM01A	T1	See the Transformer Specification	
D5	800 V, 1.2 A	SARS01	U1	IC,	STR3A453D
D6	Fast recovery, 200 V, 1 A	AL01Z	U51	Shunt regulator, $V_{REF} = 2.5 V$	(TL431 or equiv.)
D51	Schottky, 60 V, 1.5 A	EK16			

 $^{(1)}$ Unless otherwise specified, the voltage rating of capacitor is 50 V or less and the power rating of resistor is 1/8 W or less.

⁽²⁾ Refers to a part that requires adjustment based on operation performance in an actual application.

(3) High voltage is applied to this resistor that has high resistance. To meet your application requirements, it is required to select resistors designed for electromigration, or to connect more resistors in series so that the applied voltages of individual resistors can be reduced.

• Transformer Specifications

Item	Specification
Primary Inductance, L _P	518 µН
Core Size	EER-28
AL Value	245 nH/N ² (with a center gap of about 0.56 mm)
Winding Specification	See Table 1
Winding Structure	See Figure 32

Table 1. Winding Specification

Winding	Symbol	Number of Turns (turns)	Wire Diameter (mm)	Structure
Primary Winding	P1	18	$\phi \ 0.23 \times 2$	Single-layer, solenoid winding
Primary Winding	P2	28	φ 0.30	Single-layer, solenoid winding
Auxiliary Winding	D	12	$\phi \ 0.30 \times 2$	Solenoid winding
Output 1 Winding	S1-1	6	φ 0.4 × 2	Solenoid winding
Output 1 Winding	S1-2	6	φ 0.4 × 2	Solenoid winding
Output 2 Winding	S2-1	4	$\phi 0.4 \times 2$	Solenoid winding
Output 2 Winding	S2-2	4	φ 0.4 × 2	Solenoid winding



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