

**DATA SHEET** 

# SKY65006-348LF: 2.4–2.5 GHz WLAN/Zigbee® Power Amplifier

#### **Features**

- 2.4-2.5 GHz operation
- WLAN/Zigbee® applications
- · Advanced GaAs HBT process
- Integrated output power detector and F2 filter
- Low voltage positive bias supply (3.3 V)
- Low guiescent current: 50 mA
- 27 dB small signal gain
- 802.11g linear power: 18 dBm (includes integrated filter loss)
- 802.11b mask-compliant power: 21 dBm (includes integrated filter loss)
- 802.15.4 mask-compliant power: 15.4 dBm (includes integrated filter loss)
- Low-cost plastic package QFN 16-pin (3 x 3 x 0.75 mm)
- Lead (Pb)-free, and RoHS-compliant

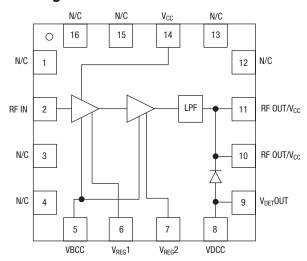
#### **Description**

The SKY65006-348LF is a linear, high-gain two-stage power amplifier with integrated output power detector and second harmonic (F2) filter, designed for low voltage operations. This device is manufactured on an advanced Gallium Arsenide (GaAs), Heterojunction Bipolar Transistor (HBT) process. It is designed for power amplifier applications in WLAN, Zigbee®, and spread spectrum systems from 2.4–2.5 GHz. The amplifier is packaged in a QFN-16, 3 x 3 x 0.75 mm package.

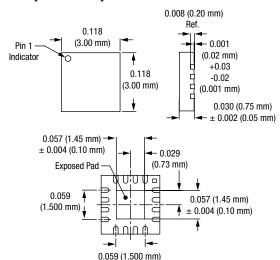


Skyworks offers lead (Pb)-free, RoHS (Restriction of Hazardous Substances)-compliant packaging.

#### **Block Diagram**



#### QFN-16 (3 x 3 mm)



#### **Pin Assignments**

Pin	Symbol	Description					
1, 3, 4, 12, 13, 15, 16	N/C	No connect					
2	RF IN	RF input					
5	VBCC	DC control voltage input that sets bias to the first and second amplifier stages.					
6	V <sub>REG</sub> 1	DC control voltage input to regulate the current to the first amplifier stages.					
7	V <sub>REG</sub> 2	DC control voltage input to regulate the current to the 2nd amplifier stage.					
8	VDCC	Reference voltage input to power detector.					
9	V <sub>DET</sub>	Power detector output voltage.					
10, 11	RF OUT/V <sub>CC</sub>	RF outputs and supply voltage inputs to second amplifier stage. These pins must be connected directly together for current sharing.					
14	V <sub>CC</sub>	DC supply voltage input to the first amplifier stage.					
Center	GND	Equipotential point. Connect package backside center paddle to the printed circuit board common via the lowest possible impedance.					

## **DC Voltage Control Table**

Mode	V <sub>CC</sub>	V <sub>REG</sub> <sup>(1)</sup>	VBCC	VDCC
RF IN-RF OUT	3.3 V	3.0 V	3.3 V	3.0 V

<sup>1.</sup> Voltage applied at evaluation board DC pins.

#### **Absolute Maximum Ratings**

Characteristic	Value		
Supply voltage (V <sub>CC</sub> )	5 V		
Supply current (I <sub>CC</sub> )	500 mA		
Regulator supply voltage (V <sub>REG</sub> 1 & V <sub>REG</sub> 2)	< V <sub>CC</sub> V		
Operating temperature (T <sub>C</sub> )	-40 °C to +85 °C		
Storage temperature (T <sub>ST</sub> )	-55 °C to +125 °C		
RF input power (P <sub>IN</sub> )	10 dBm		
Junction temperature (T <sub>J</sub> )	150 °C		

Performance is guaranteed only under the conditions listed in the specifications table and is not guaranteed under the full range(s) described by the Absolute Maximum specifications. Exceeding any of the absolute maximum/minimum specifications may result in permanent damage to the device and will void the warranty. Each absolute maximum rating listed is an individual parameter. Biasing and driving the amplifier with more than one absolute maximum rating listed may result in permanent damage to the device. Exposure to maximum rating conditions for extended periods may reduce device reliability.

CAUTION: Although this device is designed to be as robust as possible, ESD (Electrostatic Discharge) can damage this device. This device must be protected at all times from ESD. Static charges may easily produce potentials of several kilovolts on the human body or equipment, which can discharge without detection. Industry-standard ESD precautions must be employed at all times.

#### **General RF Transmit Electrical Specifications**

 $T_C = 25$  °C,  $V_{CC} = 3.3$  V,  $V_{REG} = 3$  V, VDCC = 3 V

Parameter	Symbol	Condition	Min.	Тур.	Max.	Unit
Frequency range	F		2400		2500	MHz
Gain	IS <sub>21</sub> I	Small signal	26	27		dB
Gain variation over frequency	I∆S <sub>21</sub> I	Small signal		0.2		dB
Input return loss	IS <sub>11</sub> I	Small signal		27		dB
Output return loss	IS <sub>22</sub> I	Small signal		6.5		dB
Output P <sub>1 dB</sub>	P <sub>1 dB</sub>	CW	23	24		dBm
2nd harmonic	F <sub>2</sub>	CW at P <sub>1 dB</sub>		-35		dBm
3rd harmonic	F <sub>3</sub>	CW at P <sub>1 dB</sub>		-49		dBm
Detector voltage	V <sub>DET</sub>	P <sub>OUT</sub> = 10 dBm, 802.11g modulation		0.4		V
Noise figure	NF	Small signal		6.2	7	dB
PAE @ P <sub>1 dB</sub>	PAE	CW at P <sub>1 dB</sub>	26	29		%
Quiescent current	I <sub>CQ</sub>	(No RF signal )		53		mA
Reference current	I <sub>REF</sub>	(No RF signal)		6		mA
I <sub>CC</sub> @ P <sub>1 dB</sub>	I <sub>CC</sub>	at P <sub>1 dB</sub>		265		mA

#### **802.11g Electrical Specifications**

## OFDM Modulation, 54 Mbps, $T_C$ = 25 °C, $V_{CC}$ = 3.3 V, $V_{REG}$ = 3 V, VDCC = 3 V

Parameter	Symbol	Condition	Min.	Тур.	Max.	Unit
Linear power at 2.442 GHz	P <sub>OUT</sub>	54 Mbps at 3.5% EVM		17		dBm
Current consumption	I <sub>CC</sub>	54 Mbps at linear power		130		mA
Detector voltage	V <sub>DET</sub>	54 Mbps at linear power		1		٧

### **802.11b Electrical Specifications**

#### CCK Modulation, 11 Mbps, $T_C = 25$ °C, $V_{CC} = 3.3$ V, $V_{REG} = 3$ V, VDCC = 3 V

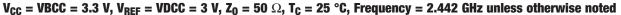
Parameter	Symbol	Condition	Min.	Тур.	Max.	Unit
Compliant power at 2.442 GHz	P <sub>OUT</sub>	11 Mbps		21.5		dBm
Current consumption	I <sub>CC</sub>	11 Mbps at compliant power		190		mA
Detector voltage	V <sub>DET</sub>	11 Mbps at compliant power		1.4		V

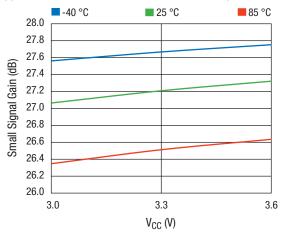
<sup>802.11</sup>b data is taken with a raised cosine filter and an alpha factor of 0.7.

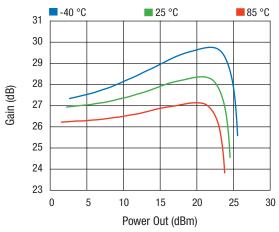
## **802.15.4 Electrical Specifications**

#### Zigbee $^{\circ}$ O-QPSK Modulation, 250 Kb/s, $T_{C}=25$ $^{\circ}$ C, $V_{CC}=3.3$ V, $V_{REG}=3$ V, VDCC = 3 V

Parameter	Symbol	Condition	Min.	Тур.	Max.	Unit
Compliant power at 2.442 GHz	P <sub>OUT</sub>	250 Kb/s @ P <sub>IN</sub> = -12 dBm		15.4		dBm
Power at 2.442 GHz	P <sub>OUT</sub>	250 Kb/s @ P <sub>IN</sub> = -2 dBm		25		dBm

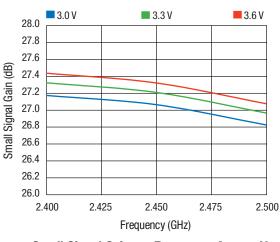


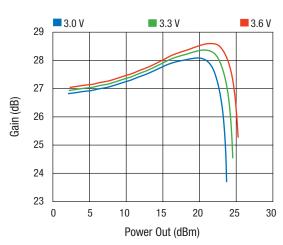




#### Small Signal Gain vs. V<sub>CC</sub> Across Temperature

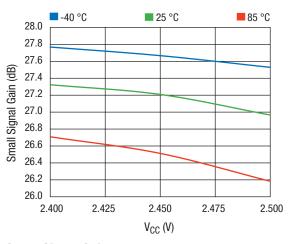
**Gain vs. Power Out Across Temperature** 

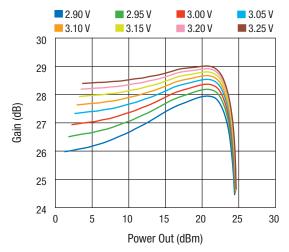




#### Small Signal Gain vs. Frequency Across V<sub>CC</sub>

Gain vs. Power Out Across V<sub>CC</sub>





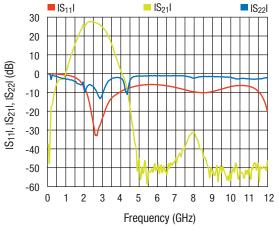
**Small Signal Gain vs. Frequency Across Temperature** 

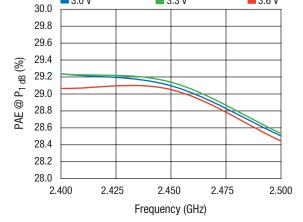
Gain vs. Power Out Across V<sub>RFG</sub>

3.6 V

#### **Typical Performance Data**

## $V_{CC}$ = VBCC = 3.3 V, $V_{REF}$ = VDCC = 3 V, $Z_0$ = 50 $\Omega$ , $T_C$ = 25 °C, Frequency = 2.442 GHz unless otherwise noted



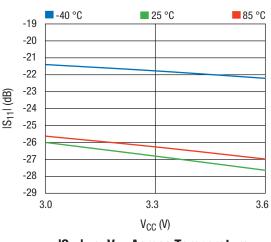


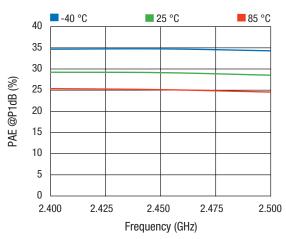
3.3 V

3.0 V

S-Parameters vs. Frequency

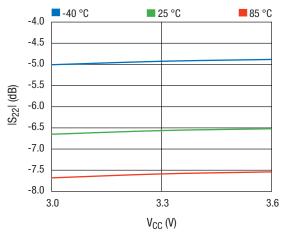
PAE @ P<sub>1 dB</sub> vs. Frequency Across V<sub>CC</sub>

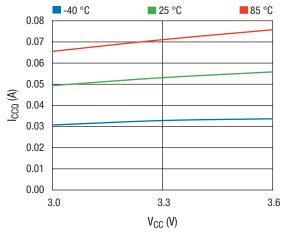




IS<sub>11</sub>I vs. V<sub>CC</sub> Across Temperature

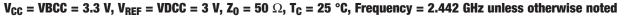
PAE @ P<sub>1 dB</sub> vs. Frequency Across Temperature

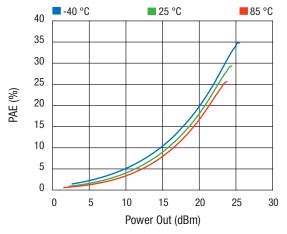




IS<sub>22</sub>I vs. V<sub>CC</sub> Across Temperature

I<sub>CCO</sub> vs. V<sub>CC</sub> Across Temperature





Power Out (dBm)

PAE @ P<sub>1 dB</sub> vs. Power Out Across V<sub>CC</sub>

15

20

3.3 V

■ 3.6 V

30

25

3.0 V

35

30

25

20

15

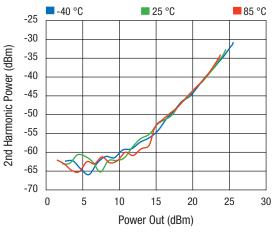
10

5

0

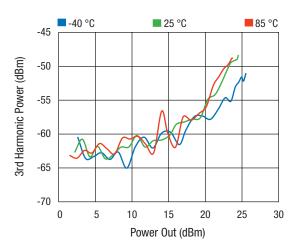
PAE @ P<sub>1 dB</sub> (%)

PAE @ P<sub>1 dB</sub> vs. Power Out Across Temperature

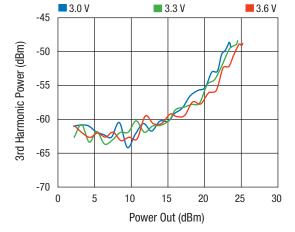


3.0 V 3.3 V 3.6 V -25 -30 2nd Harmonic Power (dBm) -35 -40 -45 -50 -55 -60 -65 -70 5 15 20 30 P<sub>OUT</sub> (dBm)

2nd Harmonic vs. Power Out Across Temperature

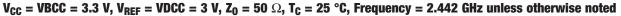


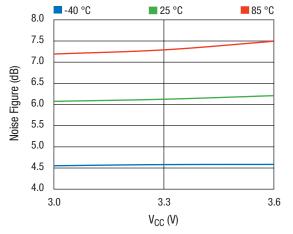
2nd Harmonic vs. Power Out Across V<sub>CC</sub>

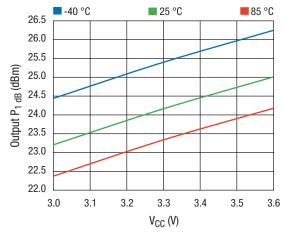


3rd Harmonic vs. Power Out Across Temperature

3rd Harmonic vs. Power Out Across V<sub>CC</sub>

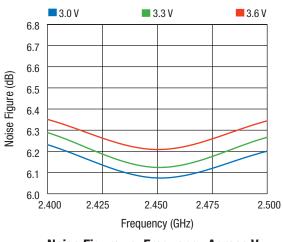


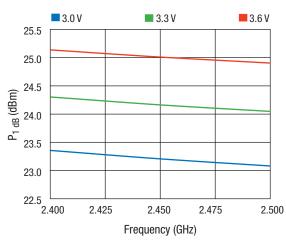




#### Noise Figure vs. V<sub>CC</sub> Across Temperature

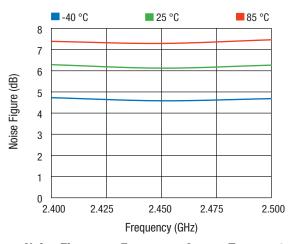
Output P<sub>1 dB</sub> vs. V<sub>CC</sub> Across Temperature

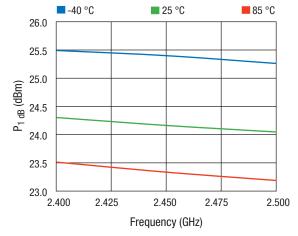




#### Noise Figure vs. Frequency Across V<sub>CC</sub>

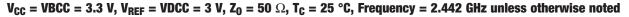
Output P<sub>1 dB</sub> vs. Frequency Across V<sub>CC</sub>

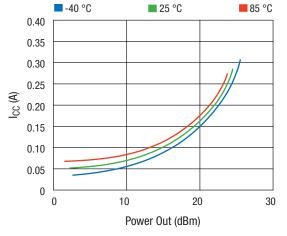




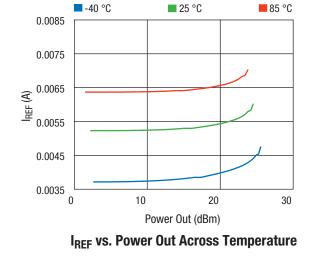
**Noise Figure vs. Frequency Across Temperature** 

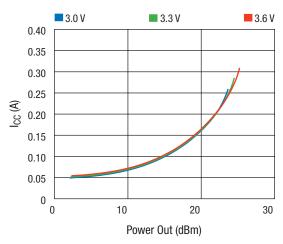
Output P<sub>1 dB</sub> vs. Frequency Across Temperature



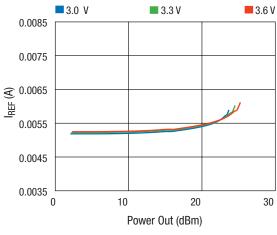


I<sub>CC</sub> vs. Power Out Across Temperature

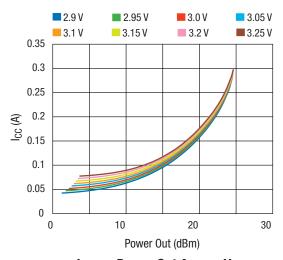




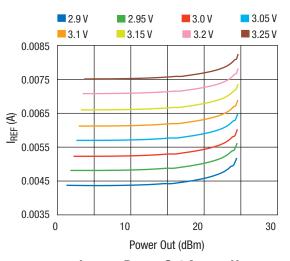
I<sub>CC</sub> vs. Power Out Across V<sub>CC</sub>



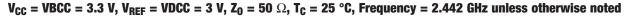
I<sub>REF</sub> vs. Power Out Across V<sub>CC</sub>

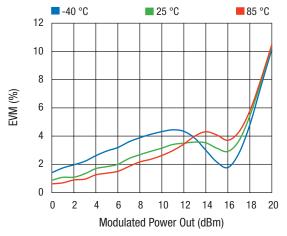


I<sub>CC</sub> vs. Power Out Across V<sub>REG</sub>

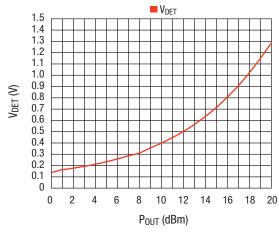


IREE vs. Power Out Across VREG

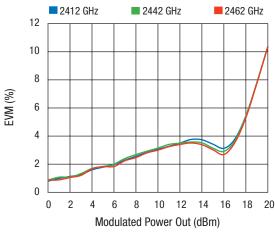




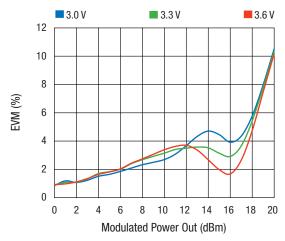
EVM vs. Modulated Power Out Across Temperture 802.11g, 54 Mbps, 64 QAM



Detector Voltage vs. Power Out 802.11g , 54 Mbps, 64 QAM

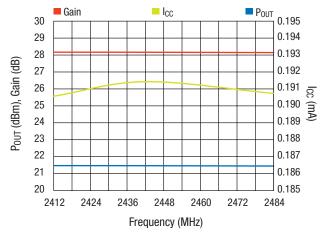


EVM vs. Modulated Power Out Across Frequency 802.11g, 54 Mbps, 64 QAM



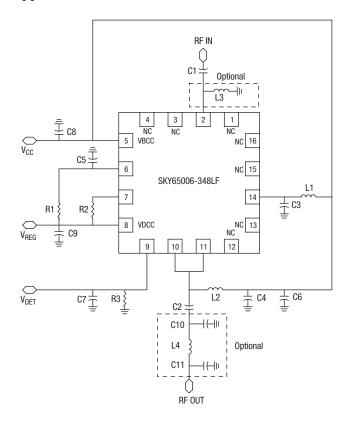
EVM vs. Modulated Power Out Across V<sub>CC</sub> 802.11g, 54 Mbps, 64 QAM

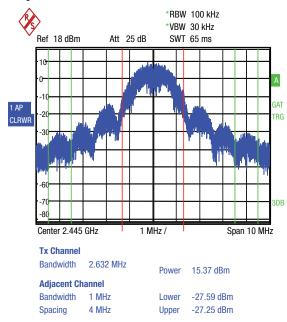
## $V_{CC}$ = VBCC = 3.3 V, $V_{REF}$ = VDCC = 3 V, $Z_0$ = 50 $\Omega$ , $T_C$ = 25 °C, Frequency = 2.442 GHz unless otherwise noted



P<sub>OUT</sub>, Gain, and I<sub>CC</sub> vs. Frequency 802.11b, CCK, 11 Mbps

### **Applications Circuit**

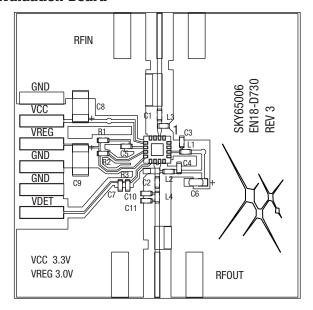




Zigbee® 802.15.4, Spectral Mask, O-QPSK, 250 Kb/s F = 2.445 GHz, Channel Power = 15.4 dBm

Channel Absolute Power Spectral Density at Mask Limit (absolute limit of -30 dBm with |f-fc| > 3.5 MHz with 100 MHz resolution bandwidth).

#### **Evaluation Board**



**Board Layout** 

#### **Bill of Material for Evaluation Board**

Part #	ID	Size	Value	Units	Manufacturer	Product Number
1	C <sub>1</sub>	0402	5.6	pF	Murata	GRM1555C1H5R6CZ01E
2	$C_2$	0402	5.6	pF	Murata	GRM1555C1H5R6CZ01E
3	C <sub>3</sub>	0402	10K	pF	Murata	GRM155R71E103KA01
4	C <sub>4</sub>	0402	10K	pF	Murata	GRM155R71E103KA01
5	C <sub>5</sub>	0402	1.8	pF	Murata	GRM1555C1H1R8CZ01D
6	C <sub>6</sub>	0603	4.7	μF	Panasonic	ECST1AZ475R
7	C <sub>7</sub>	0402	4.7	pF	Murata	GRM1555C1H4R7CZ01E
8	C <sub>8</sub>	1206	10	μF	AVX	TAJA106M006R
9	C <sub>9</sub>	1206	10	μF	AVX	TAJA106M006R
10	C <sub>10</sub>	0402	1	pF	Murata	GRM1555C1H1R0CZ01E
11	C <sub>11</sub>	0402	1	pF	Murata	GRM1555C1H1R0CZ01E
12	L <sub>1</sub>	0402	22	nH	TDK	MLK1005S22NJT000
13	L <sub>2</sub>	0402	22	nH	TDK	MLK1005S22NJT000
14	L <sub>3</sub>	0402	2.2	nH	TDK	MLK1005S2N2ST000
15	L <sub>4</sub>	0402	2.2	nH	TDK	MLK1005S2N2ST000
16	R <sub>1</sub>	0402	180	Ω	Panasonic	ERJ2GEJ181X
17	R <sub>2</sub>	0402	240	Ω	Panasonic	ERJ2GEJ241X
18	R <sub>3</sub>	0402	51K	Ω	Panasonic	ERJ2GEJ513X
19	PCB				Metro circuits	EN18-D730

#### **Test Board Biasing Procedure**

- 1. Connect the RF input and output ports as labeled on the engineering evaluation board.
- 2. Set the input power level from a CW signal generator to approximately -25 dBm.
- 3. Apply ground connection from DC voltage supply to all GND pins before applying any voltage.
- 4. Adjust the power supply to 3.3 V and set the current limit to 400 mA. Apply voltage to the pin labeled V<sub>CC</sub> and note that there is no current draw from the supply. Be sure to apply the voltage to V<sub>CC</sub> before applying any other voltages to the test board.
- 5. Adjust a second power supply output to 3.0 V and set the current limit to 30 mA. Apply voltage to the pin labeled  $V_{REG}$  and VDCC. Note that the current draw for  $V_{REG}$  is approximately 10 mA.
- 6. Observe that the current on the  $V_{CC}$  supply is in the range of the quiescent current specification. The SKY65006 should be approximately 50 mA.
- Observe that the small signal gain is within the range specified. The SKY65006 should be in the range of 27 dB. This should verify the proper working conditions for this device, and further testing can proceed.
- 8. To observe the detector voltage output, connect a voltmeter or oscilloscope to the  $V_{DET}$  pin on the evaluation test board. Set the signal source to CW mode and increase power until the output voltage begins to increase. The nominal offset voltage with low or no signal inputs should be approximately 50–200 mV and should increase monotonically to approximately 700–1000 mV, when driven at an output level of approximately 18 dBm. The evaluation circuit contains an external 51K  $\Omega$  resistor and an equivalent capacitance of 10 pF to ground.
- 9. Bias the unit off by first removing the  $V_{REG}$  power supply and finally remove the connection to the  $V_{CC}$  power supply.

#### **Application Information**

The Skyworks SKY65006 is a high-performance 2-stage InGaP power amplifier designed for 2.4-2.5 GHz ISM, IEEE802.11b, 802.11g WLAN and Zigbee® band applications. The SKY65006 is a high-efficiency linear amplifier designed for single 3.3 V supply operation, requiring no input and output matching components for 50  $\Omega$  operation. This device also includes an internal power detector and integrated harmonic filter for reduced PC board component count. The integrated low pass filter is also highly effective in reducing harmonics at their source by localizing harmonic rejection to a tiny portion of the PA chip. This significantly reduces the risk of radiation from a high order filter design external to the amplifier. Filtering of harmonics in this way may eliminate the need for an external shield over the PA, and reduces overall cost. If additional suppression of harmonics is required, an external low pass filter can be added to the output of the amplifier. Optional shunt inductor, L3, is included on the applications board at the input of the amplifier to improve the return loss. The typical performance data shown includes these optional components.

The SKY65006 requires a nominal V<sub>CC</sub> supply voltage of 3.3 V and a positive control voltage V<sub>RFG</sub>1, 2 providing bias for the first and second stage amplifiers. Nominal control voltage, V<sub>REG</sub>, is 2.5-2.6 V resulting from the stack of two emitter-base junctions of about 1.3 V each for typical GaAs HBT device. To insure proper reference currents into V<sub>REG</sub>1, 2, for normal operation of the RF stages, drop-in resistors could be used between V<sub>REG</sub>1, 2 and a V<sub>REG</sub> supply. Bias control would then be set in the range of 2.7–3.5 V allowing added flexibility for both the control voltage value and desired RF stage currents. If additional output power is required, V<sub>CC</sub> can also be increased 4.0 V. Biasing of each stage consists of an external resistor of 180  $\Omega$  (R<sub>1</sub>) and 240  $\Omega$  (R<sub>2</sub>) for the recommended typical bias currents of 15 mA and 35 mA for stage 1 and 2 respectively. In most applications one end of each of the bias resistors is tied to the V<sub>RFG</sub> supply, so both amplifier stages are biased with a single common voltage. Capacitor C<sub>5</sub>, 1.8 pF, bypasses the V<sub>RFG</sub> stage 1 control bias pin and is used to improve RF rejection of the bias control lines.

Although there is no need for external matching when operating in a 50  $\Omega$  system, an input and output 6 pF decoupling capacitor is shown on the evaluation circuit. This capacitor is only mandatory on the RF output side of the device. The RF input is DC isolated and could be connected to driver circuits directly without the need for additional blocking capacitors. Capacitors of 5.6 pF were chosen because their self-resonant frequency would not add any unwanted disturbances in the 50  $\Omega$  transmission line path. The SKY65006 is unconditionally stable at any frequency and voltage setting as long as it is grounded correctly. It is extremely important to pay special attention to the RF grounding pad under the device. Ground pad vias and solder mask patterns are designed in such a way to ensure minimum parasitic inductance to the underlying ground and at each RF bypassing component. To ensure reliable soldering of the device paddle, it is highly recommended that filled vias with a minimal reliable diameter and filling the entire pattern be used. The filled-via technique would remove the possibility of solder migration down via holes, which can cause a large increase in inductance and possible instabilities.

Each amplifier stage is biased through a series choke and shunt capacitor combination which is completely integrated on chip to provide maximum RF isolation and harmonic radiation immunity. To avoid interferences from the low-frequency gain of the amplifier and to insure stability at low out of band frequencies, stage 1 amplifier is biased through inductor L<sub>1</sub>. It is also then shunted by a large value capacitance to ensure proper low-frequency bypassing of the amplifier. To avoid a shunting effect on the 50  $\Omega$  line, a high-impedance, self-resonating choke L<sub>2</sub> (in the range of 22-33 nH depending on vendor and size) and a large value bypass capacitor are used for biasing the output stage. Capacitor  $C_6$ , 4.7  $\mu F$ , on the  $V_{CC}$  line should be placed as close as possible to the biasing network supplying stage 2 or the output stage of the amplifier. Applications with the DC bias being generated strictly from a battery as the voltage source may not require this capacitor, or as large a value as specified in the applications circuit. However, in that case, a smaller ceramic capacitor of at least 0.1 µF should be used and also placed as close as possible to the biasing network supplying stage 2. Capicator C<sub>9</sub> affects amplifier turn-on time. Reduce the value of C9 to decrease turn-on time as long as bias stability is not compromised.

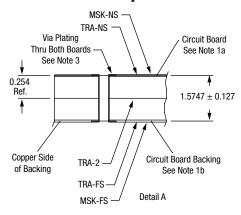
Note: Normal operation requires that  $V_{CC}$  including VBCC be applied before the application of the  $V_{REG}$  voltages biasing stage 1 and 2 bias currents. If  $V_{CC}$  and VBCC are not applied prior to the application of the  $V_{REG}$  biasing, voltage damage could occur from excessive base current draw through the collector junction of the bias transistor.

The SKY65006 also includes an on-board, compensated power detector providing a single-ended output voltage for measuring power over a wide dynamic range. The detector load and settling time constant are set external to the device. Nominal detector load is 51K  $\Omega$  and 5 pF, yielding a settling time of approximately 500 ns. Note that there is an internal 5 pF on-chip capacitance, so the net capacitance value is approximately 10 pF. Lower resistor values may be used if necessary with the net impact being a lower output detector voltage over its useful dynamic range. For proper detector operation, a reference voltage must be applied to the V\_DET line. Any voltage between 2 and 4 V is acceptable for the reference voltage, but it is recommended to supply V\_DET from the V\_REG power supply. The benefit in doing

this is that the approximate 2 mA of current that the reference circuit consumes will not be wasted with the PA in the "Off" state. There is also the option of not biasing the detector reference if the current consumption is of prime importance, but the detector will then act as a normal unbiased detector, and sensitivity and accuracy will be degraded.

The evaluation circuit board is constructed as a four-layer FR4 stack with an overall thickness of 0.062 inches (1.57 mm). Top layer dielectric is 0.01-inch thick with 50  $\Omega$  transmission line widths of 0.0195 inches. The printed circuit board is constructed using a symmetrical 0.01-inch stack on the top and bottom layers and with a 0.032-inch thick pre-preg core. All components are 0402 in size with the exception of the 4.7 uF and 10 uF tantalum capacitors. Please note the 10 uF capacitors are installed to provide low frequency filtering for lab testing. Actual values, if necessary, will be dependent upon layout and circuit environment. All ground vias used are 0.012 inches in diameter and placed as close to the ground ends of by-passing components as possible. Four vias are used under the device to create a low inductance path to ground. If a smaller diameter is to be used, or if the substrate thickness is greater than 0.01 inches, additional vias must be placed under the device to reduce the potential risk of parasitic oscillation.

#### **Evaluation Board Stack-Up**



#### Notes:

Units = mm.

- 1. Material:
- Circuit board: FR4, 0.254 mm thick, 1 oz finished copper TRA-NS layer, 1/2 oz finished copper TRA-2 layer.
- 1b. Circuit board backing: FR4 prepreg, 1 oz copper one side.
- 1c. Laminate the unmetalized side of backing to bottom of circuit board for a total thickness of 1.5747  $\pm$  0.127 mm. (See Detail A)
- 2. Plating: 200 microinches of nickel, and 50-100 microinches of soft gold.
- 3. Via plating: Cu plate 0.001 to 0.0015 thru both boards.
- RF lines marked with \* to be finished width of 0.50 mm measured at bottom of trace (trace to board interface).

All line width tolerances  $\pm$  0.025 mm.

All rubout tolerances ± 0.025 mm.

- 5. Silk-screen reference designators approximately as shown.
- 6. Separate boards with router.

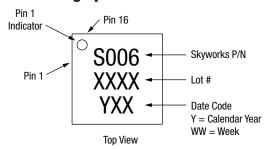
#### **Recommended Solder Reflow Profiles**

Refer to the "<u>Recommended Solder Reflow Profile</u>" Application Note.

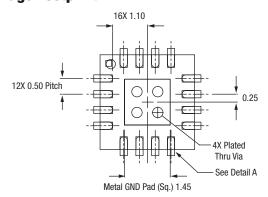
#### **Tape and Reel Information**

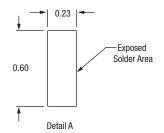
Refer to the "<u>Discrete Devices and IC Switch/Attenuators</u> Tape and Reel Package Orientation" Application Note.

#### **Device Branding Specifications**



#### **Package Footprint**





Units = mm

#### **Ordering Information**

Model Name	Manufacturing Part Number	<b>Evaluation Kit Part Number</b>	
SKY65006-348LF: 2.4–2.5 GHz WLAN/Zigbee® Power Amplifier	SKY65006-348LF (Pb-free package)	TW17-D620-001	

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