

# μA783

## 9 WATT AUDIO POWER AMPLIFIER

FAIRCHILD LINEAR INTEGRATED CIRCUIT

**GENERAL DESCRIPTION** — The μA783 is high-voltage monolithic integrated circuit in a 12-pin power package. It is constructed using the Fairchild Planar\* epitaxial process. It is designed for use as a low frequency Class B power amplifier and is intended primarily for 8 Ω and 16 Ω applications. It typically provides 9 W into 8 ohms and 5 W into 16 ohms from a 24 V supply.

The μA783 is provided with two pin configurations (P3 and P4). Both devices are identical electrically.

The μA783 is pin for pin compatible with the TBA810S and TCA940.

- THERMAL SHUTDOWN
- WIDE SUPPLY VOLTAGE RANGE (4 V to 30 V)
- HIGH CURRENT CAPABILITY (2.5 A)
- 12-PIN POWER PACKAGE

### ABSOLUTE MAXIMUM RATINGS

Supply Voltage	30 V
Output Peak Current (Non-Repetitive)	3.5 A
Output Current (Repetitive)	2.5 A
Input Voltage	220 mVrms
Power Dissipation: at $T_A = 70^\circ\text{C}$	1.0 W
at $T_C = 90^\circ\text{C}$	6.0 W
Storage and Junction Temperature	-40 to 150°C
Pin Temperature - Soldering, 10 s	260C

\*Planar is a patented Fairchild process.

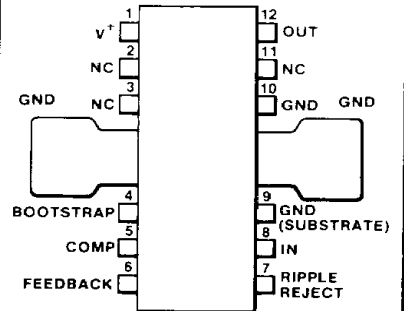
### CONNECTION DIAGRAM

#### 12-PIN POWER PACKAGE

(TOP VIEW)

PACKAGE OUTLINE 9W

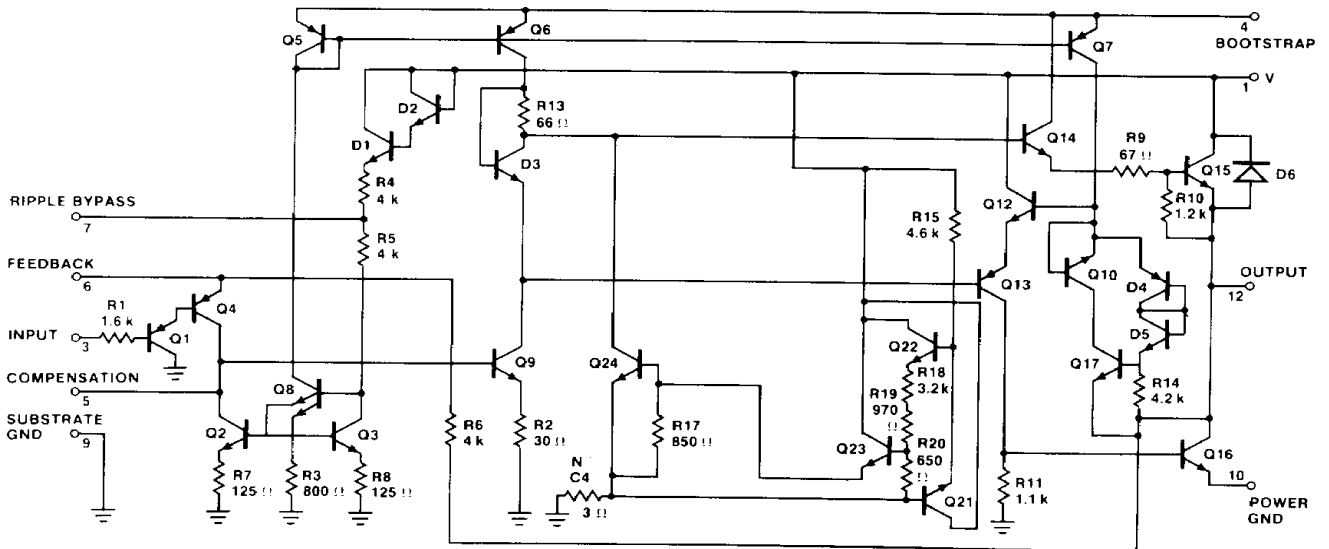
PACKAGE CODES P3, P4



### ORDER INFORMATION

TYPE	PART NO.
μA783C	μA783P3C
μA783C	μA783P4C

### EQUIVALENT CIRCUIT



**ELECTRICAL CHARACTERISTICS:** Refer to the test circuit:  $T_A = 25^\circ\text{C}$

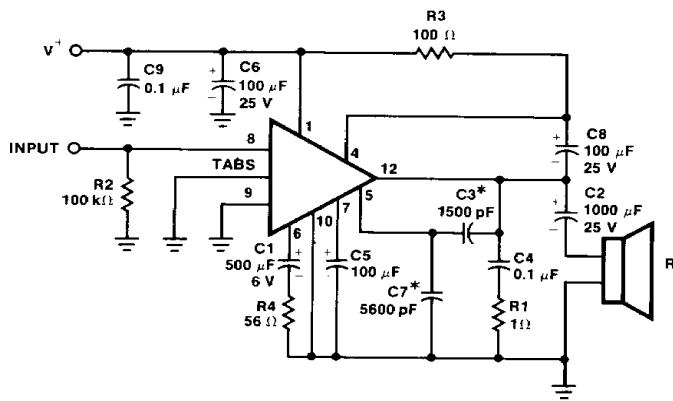
CHARACTERISTICS	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Quiescent Output Voltage (Pin 12)	$V^+ = 24.0\text{ V}$	11.2	12.0	12.8	V
Quiescent Drain Current (Pin 1)			20.0	30.0	mA
Bias Current (Pin 8)				0.4	$\mu$ A
Power Output	THD = 10% $f = 1.0\text{ kHz}$	8.0	5.0		W
	$V^+ = 24.0\text{ V}, R_L = 16\ \Omega$		9.0		W
	$V^+ = 24.0\text{ V}, R_L = 8\ \Omega$		5.2		W
	$V^+ = 14.4\text{ V}, R_L = 4\ \Omega$		0.9		W
Input Sensitivity	$P_{OUT} = 9\text{ W}, V^+ = 24.0\text{ V}$ $R_L = 8.0\ \Omega, f = 1.0\text{ kHz}$		147.0	200.0	mV
			60.0		mV
Input Resistance (Pin 8)			5.0		M $\Omega$
Frequency Response (-3.0 dB)	$V^+ = 24.0\text{ V}, R_L = 8.0\ \Omega$ $C_3 = 820\text{ pF}$ $C_3 = 1500\text{ pF}$		20-30000		Hz
			20-20000		Hz
Total Harmonic Distortion	$P_{OUT} = 50\text{ mW to } 5\text{ W},$ $V^+ = 24.0\text{ V}$ $R_L = 8.0\ \Omega, f = 1.0\text{ kHz}$		0.3		%
Voltage Gain (Open Loop)	$V^+ = 24.0\text{ V}, R_L = 8.0\ \Omega, f = 1.0\text{ kHz}$		70.0		dB
Voltage Gain (Closed Loop)	$V^+ = 24.0\text{ V}, R_L = 8.0\ \Omega, f = 1.0\text{ kHz}$	34.0	36.0	40.0	dB
Input Noise Voltage	$V^+ = 24.0\text{ V}, R_g = 0,$ BW (-3.0 dB) = 20 Hz to 20,000 Hz		3.0		$\mu$ V
Input Noise Current	$V^+ = 24.0\text{ V},$ BW (-3.0 dB) = 20 Hz to 20,000 Hz		0.15		nA
Efficiency	$P_{OUT} = 9\text{ W}, V^+ = 24.0\text{ V},$ $R_L = 8.0\ \Omega, f = 1.0\text{ kHz}$		70.0		%
Supply Voltage Rejection	$V^+ = 24.0\text{ V}, R_L = 8.0\ \Omega$ $f_{ripple} = 100\text{ Hz}$		45.0		dB

**THERMAL DATA**

$\theta_{JC}$	Thermal Resistance Junction to Case (tab)	MAX	$\mu$ A783P3 12° C/W	$\mu$ A783P4 10° C/W
$\theta_{JA}$	Thermal Resistance Junction to Ambient	MAX	70° C/W**	80° C/W

\*\*Obtained with tabs soldered to print circuit with minimized copper area.

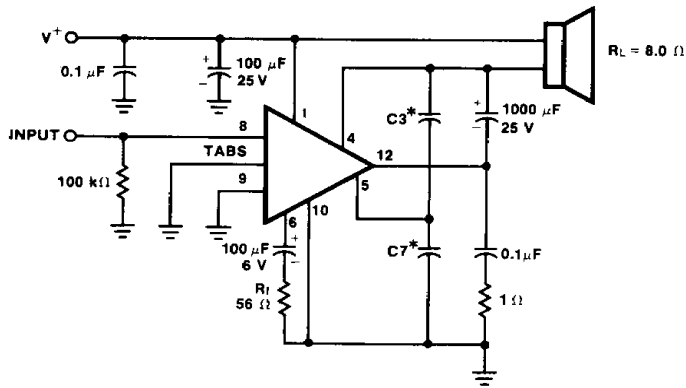
**TEST AND APPLICATION CIRCUIT**



\*C3 and C7 See Figure 3

Figure 1

TYPICAL CIRCUIT WITH LOAD CONNECTED TO THE SUPPLY VOLTAGE



\*C3 and C7 See Figure 3

Figure 2

TYPICAL VALUE OF C3 AS A FUNCTION OF Rf FOR VARIOUS VALUES OF BANDWIDTH

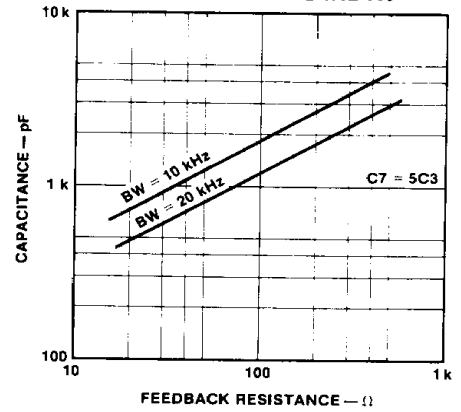


Figure 3

POWER OUTPUT AS A FUNCTION OF SUPPLY VOLTAGE

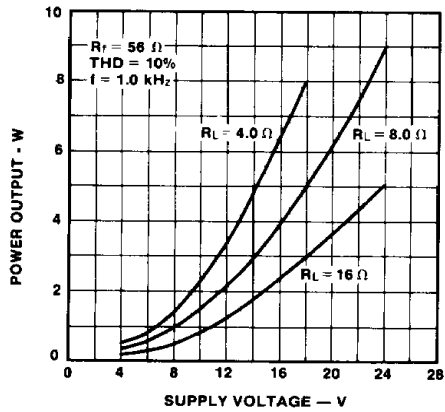


Figure 4

MAXIMUM POWER DISSIPATION AS A FUNCTION OF SUPPLY VOLTAGE (SINE WAVE OPERATION)

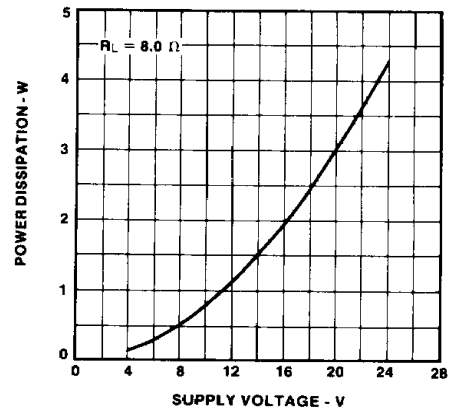


Figure 5

TOTAL HARMONIC DISTORTION AS A FUNCTION OF POWER OUTPUT

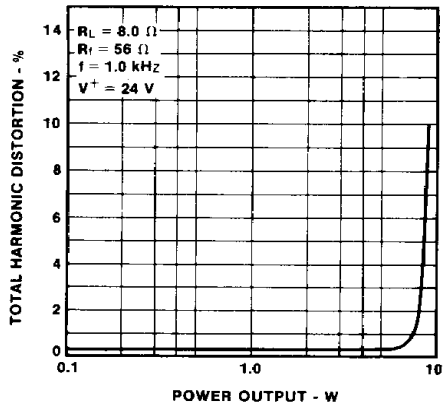


Figure 6

TOTAL HARMONIC DISTORTION AS A FUNCTION OF FREQUENCY

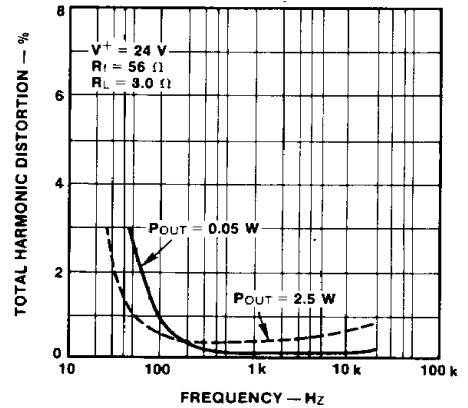


Figure 7

**INPUT VOLTAGE AND VOLTAGE GAIN (CLOSED LOOP) AS A FUNCTION OF FEEDBACK RESISTANCE**

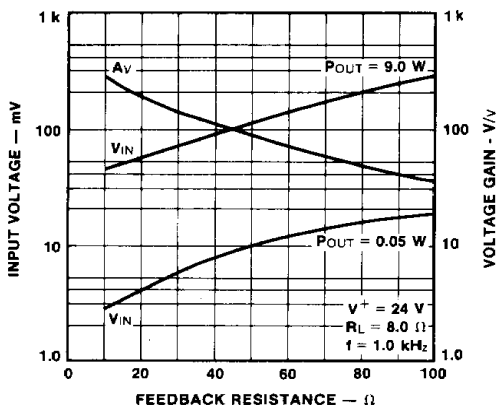


Figure 8

**POWER DISSIPATION AND EFFICIENCY AS A FUNCTION OF POWER OUTPUT**

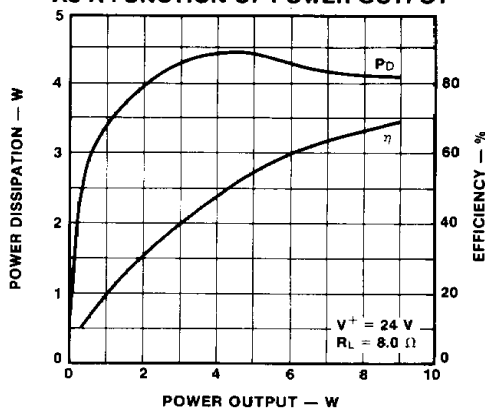


Figure 9

**OUTPUT VOLTAGE AS A FUNCTION OF SUPPLY VOLTAGE**

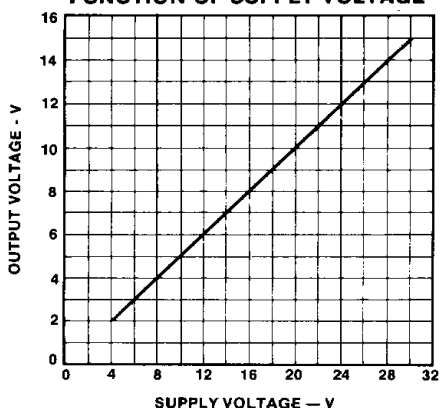


Figure 10

**QUIESCENT CURRENT AS A FUNCTION OF SUPPLY VOLTAGE**

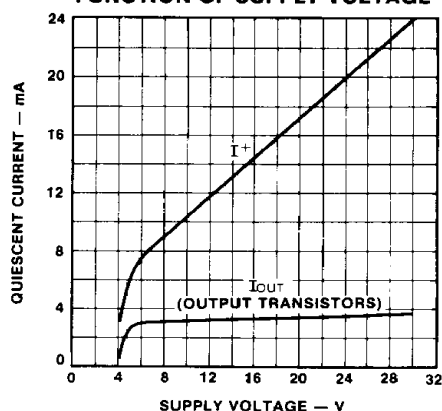


Figure 11

**SUPPLY VOLTAGE REJECTION AS A FUNCTION OF FEEDBACK RESISTANCE**

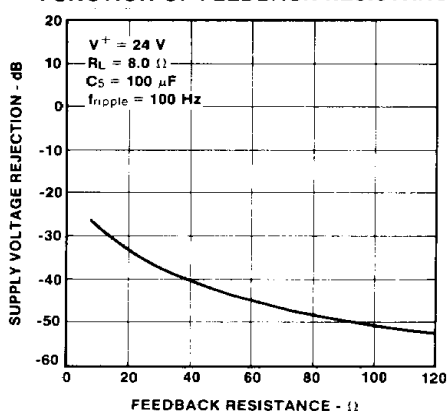


Figure 12

**SUPPLY VOLTAGE REJECTION AS A FUNCTION OF FEEDBACK RESISTANCE IN CIRCUIT OF FIGURE 2**

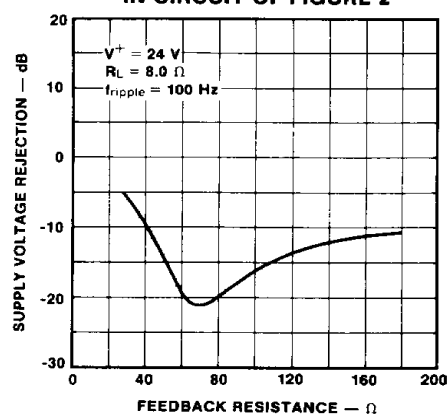


Figure 13

**MOUNTING INSTRUCTIONS**

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heat sink ( $\mu$ A783P4C, Figure 14) or by soldering them to an area of copper on the printed circuit. ( $\mu$ A783P3C, Figure 15). During soldering, the tabs temperature must not exceed 230°C and the soldering time must not be longer than 12 seconds. Figures 16a and 16b show two ways that can be used for mounting the device.

**MAXIMUM POWER DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE ( $\mu$ A783P4C)**

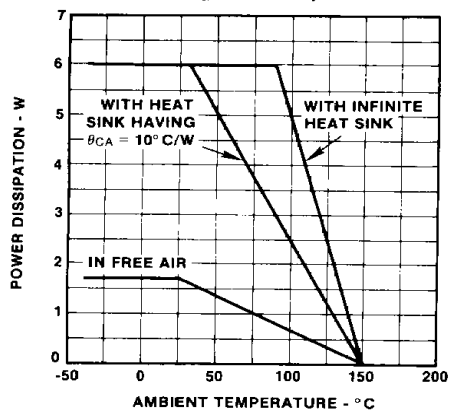


Figure 14

**MAXIMUM POWER DISSIPATION AND TOTAL THERMAL RESISTANCE AS A FUNCTION OF COPPER AREA OF PC BOARD ( $\mu$ A783P3C)**

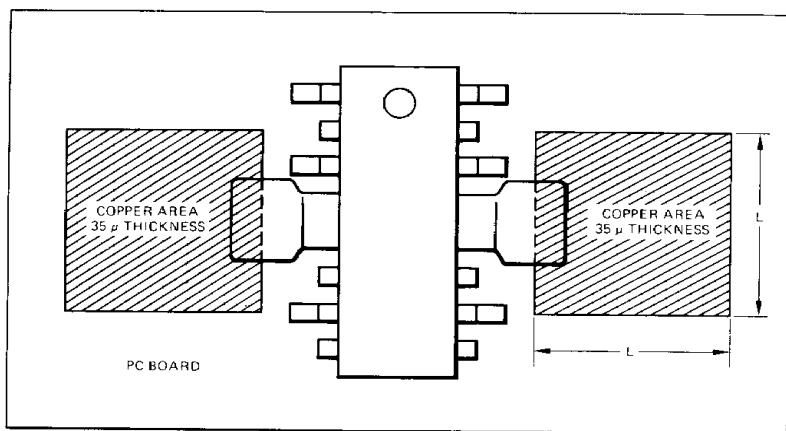


Figure 15

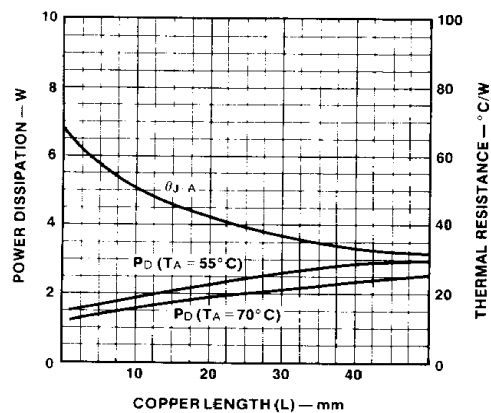


Figure 16a shows a method of mounting the  $\mu$ A783P3C that is satisfactory both from the point of view of heat dissipation and from mechanical considerations. For the  $\mu$ A783P4C, the desired thermal resistance is obtained attaching the hardware shown in Figure 16b, to a bracket with proper dimensions. This bracket can also act as a support for the whole printed circuit board.

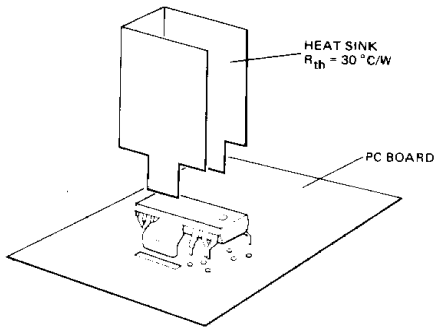


FIGURE 16a

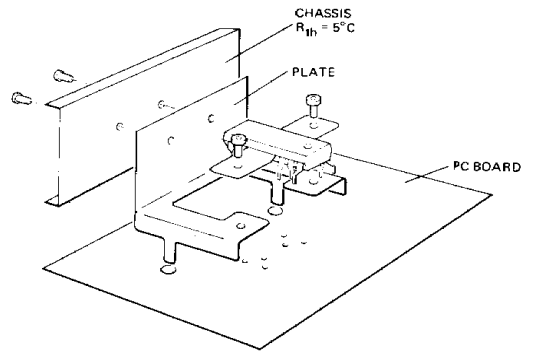


Figure 16b

**THERMAL SHUTDOWN**

The on chip design of the thermal limiting circuit offers the following advantages:

1. An overload on the output (even if permanent) or an above-limit ambient temperature can be easily handled.
2. The heat sink can have a smaller factor of safety compared with that of a conventional circuit. In case of too high a junction temperature, power output, power dissipation and the supply current decrease (Figure 17) thus protecting the device.

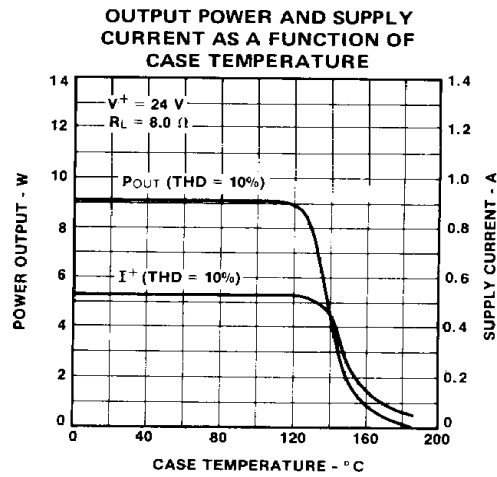


Figure 17